

International Association of Wildland Fire

BARA: cellular automata simulation of multidimensional smouldering in peat with horizontally varying moisture contents

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ABSTRACT

Background. Smouldering peatland wildfires can last for months and create a positive feedback for climate change. These flameless, slow-burning fires spread horizontally and vertically and are strongly influenced by peat moisture content. Most models neglect the non-uniform nature of peat moisture. Aims. We conducted a computational study into the spread behaviour of smouldering peat with horizontally varying moisture contents. **Methods.** We developed a discrete cellular automaton model called BARA, and calibrated it against laboratory experiments. **Key results.** BARA demonstrated high accuracy in predicting fire spread under non-uniform moisture conditions, with >80% similarity between observed and predicted shapes, and captured complex phenomena. BARA simulated I h of peat smouldering in 3 min, showing its potential for field-scale modelling. **Conclusion.** Our findings demonstrate: (i) the critical role of moisture distribution in determining smouldering behaviour; (ii) incorporating peat moisture distribution into BARA's simple rules achieved reliable predictions of smouldering spread; (iii) given its high accuracy and low computational requirement, BARA can be upscaled to field applications. **Implications.** BARA could form part of an early fire warning system for peatland.

Keywords: cellular automata, climate change, fire, hydrology, modelling, peat moisture, peatlands, wildfires.

Introduction

Smouldering is a flameless and slow-burning fire that spreads both horizontally and vertically and occurs at a lower temperature than flaming combustion (Rein 2013). Owing to these differences, smouldering peatland wildfires produce haze that spreads to inhabited regions and affects people's health (Rein 2013; Huang *et al.* 2015; Hu *et al.* 2018). These wildfires create positive feedbacks to climate change by releasing carbon that is naturally stored in peat and cannot be reabsorbed by the ecosystem (Johnston *et al.* 2012; Rein 2013; Turetsky *et al.* 2015).

Peat moisture content (MC) is widely recognised as the primary factor influencing smouldering peatland wildfires (Rein 2013; Mezbahuddin *et al.* 2023), as it affects ignition limits and spread rates (Frandsen 1987; Huang *et al.* 2015; Christensen *et al.* 2020). In peatlands, the peat MC varies both spatially (horizontally and vertically) and temporally (Meingast *et al.* 2014; Prat-Guitart *et al.* 2016, 2017). These MC variations are influenced by topography, surface vegetation, hydrological processes and weather conditions (Prat-Guitart *et al.* 2016, 2017; Bechtold *et al.* 2020). Vertically, peat is wetter at deeper points owing to their proximity to the groundwater table (GWT) (Fig. 1*a*). Horizontally, variations in peat MC are more intricate (Fig. 1*b*) and influenced by factors such as topography and surface vegetation (Prat-Guitart *et al.* 2017).

The complex interplay of MC variations has hindered the development of modelling studies focusing on smouldering peat with spatially varying MCs. To date, studies involving spatially varying MCs in smouldering peat models have been constrained by the complexities associated with multi-dimensional spread (Huang and Rein 2015; Prat-Guitart *et al.* 2016). However, given the significant influence of peat MC on smouldering

Received: 27 March 2023 Accepted: 6 November 2023 Published: 23 January 2024

Cite this: Purnomo DMJ et al. (2024) International Journal of Wildland Fire 33, WF23042. doi:10.1071/WF23042

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Fig. 1. (*a*) Peat MC measured at three different depths, 5, 10 and 30 cm, within a 30-day period in a peatland in New Zealand. This MC profile was extracted from the work of Campbell *et al.* (2002). (*b*) Horizontal MC variations (top view) observed in a peatland in Ireland. This MC profile was extracted from the work of Prat-Guitart *et al.* (2017).

behaviour, there is a need to overcome these challenges and advance our understanding of the phenomenon.

Considering these complexities at a large scale, computational studies of smouldering using physics-based models such as computational fluid dynamics are too expensive (Purnomo 2022; Yuan *et al.* 2023). Therefore, in the present work, we explored cellular automata (CA). CA are discrete models that use simple rules and limit the interactions of entities within a domain (von Neumann 1967; Wolfram 1984). Unlike physicsbased models that use fundamental principles for their rules, CA can use a number of approaches, such as empirical and statistical, as the governing rules.

CA consider a grid of cells, each of which has a certain state (e.g. peat, smouldering, or burnt) that is updated over discrete time steps. Each cell in CA affects only a few neighbouring cells, whereas in physics-based models, each cell could affect all the cells in the grid; thus, the number of computations in CA can be minimal. By using simple rules and limiting the reach of interactions between cells, CA provide a computationally efficient way to simulate complex phenomena; they require fewer resources but can achieve equivalent results.

CA have been extensively used to model wildfires, and many aspects and phenomena (e.g. crown fire, firebrands) have been successfully simulated by implementing different rules (Clarke *et al.* 1994; Karafyllidis and Thanailakis 1997; Malamud *et al.* 1998; Alexandridis *et al.* 2011; Collin *et al.* 2011; Trunfio *et al.* 2011; Ntinas *et al.* 2017). Unlike flaming fires, smouldering fires have been the focus of few studies involving the application of CA (Belcher *et al.* 2010; Fernandez-Anez *et al.* 2017, 2019; Purnomo *et al.* 2021, 2023; Widyastuti *et al.* 2021).

Among these works, only heat accumulation and bond percolation approaches (see details in Purnomo 2022) have been used for the rules in CA. In heat accumulation CA, each cell has an intrinsic value on which its state is based. A cell changes state when its intrinsic value exceeds a threshold (Purnomo 2022). The intrinsic value of each cell is updated

depending on the intrinsic values of neighbouring cells. In bond percolation CA, a cell changes state probabilistically when conditions are met (e.g. making contact with a cell with a different state; Purnomo 2022).

The model in Belcher *et al.* (2010) used bond percolation CA to simulate smouldering peat with uniform and constant MC. This model took into account the probability of ignition and extinction, which were dependent on the oxygen concentration. It was designed to explore fire activity over millennia, based on variations in Earth's oxygen concentration.

The model in Fernandez-Anez *et al.* (2017, 2019) used heat accumulation CA and considered drying, pyrolysis and oxidation thresholds, mimicking the physical phenomena of smouldering. This model focused on uniformly moist peat and investigated smouldering behaviour under different conditions, including downwind, upwind and limited oxygen concentrations.

The model in Widyastuti *et al.* (2021) used an agentbased method that is similar to bond percolation CA to simulate peatland wildfires at the field scale, encompassing both flaming and smouldering. This model considered peat MC and GWT to determine the associated probabilities. However, it only examined the effects of uniform and constant peat MC and GWT, without considering their spatial and temporal variations.

The model in Purnomo *et al.* (2021) also used bond percolation CA to simulate field-scale peatland wildfires that considered both flaming and smouldering. The probabilities involved in the model were calibrated against a semi-physical model and experiments. The model also investigated the impact of peat MC on smouldering severity, but did not account for variations in MC.

Building on their earlier work, Purnomo *et al.* (2023) advanced the model in Purnomo *et al.* (2021) by incorporating temporal variations in peat MC. This updated model explored the effects of such variations on smouldering severity over extended periods. However, the spatial variations in peat MC were not considered in this particular model.

Existing literature on CA models for smouldering predominantly focuses on uniform MC. Furthermore, these models solely address the horizontal spread of smouldering, neglecting its vertical spread. The current paper presents a novel approach by utilising CA to simulate smouldering peat with horizontally varying MCs, while also incorporating its multidimensional spread. This is the first study to consider both the spatial variability in MC and the comprehensive spread of smouldering within a CA framework.

Methods

The cellular automata model

In this work, we developed a CA model to simulate the multidimensional spread of smouldering peat (not a 3D



Fig. 2. (a) Schematic of the rules in BARA. Subscript (n) represents the neighbour's position relative to the centre cell (i), i.e. north (N), south (S), east (E) and west (W). Straight arrows represent the heat transfer to neighbours. Curvy arrows represent the heat loss to the surroundings. (b) Schematic of the state change in BARA from *peat* (P) to smouldering (S) to burnt out (B). The state change from *peat* to smouldering occurs when H exceeds Θ with a probability of P_s . Smouldering cells remain in that state for a time period t_s after which they become burnt out.

model in its full essence to minimise computational cost) with horizontally varying MCs. From here on, we refer to the model in this work as BARA, which originates from the term for 'smouldering' in Indonesian. BARA integrates a heat accumulation approach to model heat transfer (mimicking heat transfer from burning fuel to unburnt fuel) and a bond percolation approach to introduce uncertainty (related to the variability in nature, e.g. caused by landscape heterogeneity), adapted from Fernandez-Anez et al. (2019); thus, BARA is a stochastic model. In BARA, the intrinsic values of cells were updated every time step based on the intrinsic values of their neighbours, and the states of cells were updated probabilistically when their intrinsic values exceeded predetermined thresholds. We used the von Neumann neighbourhood (simplest neighbourhood to minimise computational cost), which includes the four cells adjacent to the centre cell: north (N), south (S), west (W) and east (E) as shown in Fig. 2a (see Table 1 for the information of variables in the figure).

States and rules of BARA

BARA considers three states: *peat* (*P*), *smouldering* (*S*) and *burnt out* (*B*). These states represent simplified stages of smouldering fire. In physical terms, the *peat* state represents undisturbed peat that can transition to the *smouldering* state when it is burning. Once the full depth of peat is consumed, *smouldering* cells are extinguished, and cells change to the *burnt out* state. Each cell in BARA has an intrinsic value (*H*) at any given time, which in this work is referred to as a heat value, analogous to temperature in physical terms. Information on the states and heat values of cells is stored in two different computational layers, the fuel and heat layers, adapted from Fernandez-Anez *et al.* (2019). This multi-layer approach enables BARA to imitate the physics of combustion. The fuel layer mimics the evolution of fuel during the combustion (e.g. unburnt fuel, oxidation), and

 Table I.
 The list of variables and parameters used in BARA with their units.

Variable and parameters	Symbol	Unit
Smouldering time in BARA	t _s	s
Heat release rate in BARA	Q _R	Non-dimensional
Heat transfer coefficient in BARA	φ	Non-dimensional
Burning threshold in BARA	Θ	Non-dimensional
Heat loss coefficient in BARA	μ	Non-dimensional
Smouldering probability in BARA	Ps	Non-dimensional
Time step	Δt	s
Cell size	Δx	mm
Horizontal spread rate	S _H	mm/min
Vertical spread rate	S _d	mm/min
Smouldering width	Ws	mm/min
Moisture content	MC	Non-dimensional
Inorganic content	IC	Non-dimensional
Reactor thickness	d	mm
Bulk density	$ ho_{ m b}$	kg/m ³
Organic density	ρο	kg/m ³
Specific heat	с	kJ/kg K
Thermal conductivity	k	W/m K

the heat layer mimics the heat transfer in fires based on the temperature distribution.

The state change from *peat* to *smouldering* depends on the H values of cells: when the H values exceed the burning threshold (Θ), the *peat* cells change to *smouldering* with a probability of P_s (smouldering probability). The H values of cells are affected by the sum of H received from or given to neighbouring cells (H_t) . If H_t is greater than zero, then heat is given to the neighbours (n); otherwise, heat is received from the neighbours to the centre cell (i). The value of H_t depends on the difference in H between the cell and its neighbouring cells, the number of cells separating the two cells (Δl) and the heat transfer coefficient (φ), as shown in Eqn 1 (see further details in Supplementary Appendix B). However, because we used the von Neumann neighbourhood, the value of Δl_{in} in Eqn 1 was set to 1. φ determines the fraction of ΔH transferred to neighbouring cells, which mimics heat transfer coefficients in physical terms. This heat transfer depends on the neighbouring cells involved in the process; therefore, in spatially non-uniform cases, different neighbouring cells have different ΔH and φ .

$$H_{\rm t} = \varphi_n \times \frac{\Delta H_{in}}{\Delta l_{in}} \tag{1}$$

Heat loss to the surroundings is also considered in BARA and depends on the difference between the H values of cells and



Fig. 3. The components present in any one cell in BARA: each cell in the model contains organic and inorganic matter, water and air. In every time step in smouldering cells, peat with a thickness δ is consumed by the fire.

the *H* value of the ambient environment (H_o), and the heat loss coefficient (μ). H_o is held constant at zero for simplification purposes, but in nature, ambient conditions are not constant. At every time step, an amount of heat (μ *H*) is lost from each cell to the surroundings, representing the heat loss due to convection and radiation. In general, μ depends on wind and surface shape, but it was set constant for simplicity. These heat transfer rules are summarised in Fig. 2*a*.

We implemented a novel method to introduce the vertical spread in BARA in addition to the 2D horizontal spread of Fernandez-Anez et al. (2019). The thickness of peat in a cell (d) decreases with time while burning owing to the vertical spread that consumes it vertically (Fig. 2a). A peat cell contains inorganic and organic matter, water and air (see Fig. 3), where organic matter is the only combustible component. A peat cell contains water and inorganic matter because peat in nature is wet and has impurities from mineral content. As peat is a porous medium, air occupies its pores; thus, the *peat* cell has an air component. Every time step while a cell smoulders, its organic fraction is consumed by a thickness δ . The fire completely consumes one cell of *peat* when the product of the number of time step and δ is equal to d. This is implemented by using a smouldering time variable (t_s) . Once *peat* cells become *smouldering* cells, they continue to burn for a time t_s . Smouldering cells become burnt out after t_s is reached (Fig. 2b). During t_s , a smouldering cell generates an amount of heat Q_R in every time step, increasing H; this process reproduces the heat generation of fire. However, for simplicity, $Q_{\rm R}$ was set to depend only on the organic faction. Table 1 summarises variables and parameters used in BARA.

Sensitivity analysis

The variables used in BARA were selected based on calibration against laboratory experiments. However, prior to this calibration, we performed a sensitivity analysis to determine the importance of each variable and the range of variable values that enable the predictions to fit experimental results. Both sensitivity analysis and calibration were undertaken in a 400×400 cell grid, where the cell size (Δx) was 1 mm and *d* was 1.6 cm (see Fig. 2*a*).



Fig. 4. Sensitivity analysis of BARA for different cell sizes. BARA was run using different cell sizes, and the predicted horizontal spread rates (S_H) of each scenario (one scenario means one cell size) were compared against the prediction when using a cell size of 0.4 mm (highest resolution tested). The variation in S_H is within 5% when the cell size is smaller than 2 mm. From this analysis, a cell size (Δx) of I mm was selected for BARA.

This domain simulated the experiments used for calibration ($40 \times 40 \times 1.6$ cm) in Christensen *et al.* (2020). The cell size selected was the coarsest size that has a small difference (less than 10%) in predictions against the predictions by using the tested finest cell size (0.4 mm, see Fig. 4). One time step (Δt) in BARA represents 20 s in real time, which was selected to satisfy the stability criteria given the spatial resolution (Δx).

The six variables in BARA (P_s , φ , Q_R , t_s , Θ and μ) were arranged into four groups of three variables. For the sake of efficiency and simplicity, the sensitivity analysis was performed by exploring combinations of three variables (instead of six), setting the other three as constants, and was performed four times. The variables were grouped as follows: Group 1 (P_s , φ and Θ); Group 2 (Q_R , φ and Θ); Group 3 (t_s , φ and Θ), and Group 4 (μ , φ , and Θ). These groups were considered because P_s , Q_R , t_s and μ have independent effects on predictions (the change in one variable cannot be compensated for by a change of the other variable to obtain an equal prediction), whereas the effects of φ and Θ on predictions are dependent on one another (the change of one variable can be compensated for by a change of the other variable to obtain an equal prediction).

The sensitivity analysis is based on smouldering spread rate and smouldering width. Thus, the set of values of the variables that enable BARA to give spread rate and smouldering width similar to the experiments of Christensen *et al.* (2020) were explored. Smouldering width is the distance between unburnt and burnt lines that comprise the smouldering perimeter. This is an important parameter because



Fig. 5. Results from BARA simulation of smouldering peat, with 20% MC and 20% IC, both the expected circular ring result (left) and the unexpected non-circular result (right). *P* is *peat*, *S* is *smouldering* and *B* is *burnt out*.

it represents the vertical spread rate of smouldering (Christensen *et al.* 2020).

Results

The sensitivity analysis of Group 1 (see Supplementary Fig. A1) shows that high P_s values made BARA predict noncircular spread (see Fig. 5), whereas low P_s values made BARA predict no ignition; the range of usable P_s values is narrow (0.08–0.15). P_s was then set to 0.1, at the centre of this narrow range.

Fig. 6 shows the sensitivity analysis of Groups 2 and 3 on horizontal spread rate and smouldering width compared with the values measured in Christensen et al. (2020). In this figure, black regions represents non-circular spread. From the sensitivity analysis of Group 2 (see Fig. 6a), the range of φ values that enables BARA to predict correctly is from 0.05 to 0.2; lower values caused no ignition, whereas higher values cause the shape to be non-circular. This reasoning was also adopted to determine the valid range for Θ , which was found to be 0.01–0.2. An increase in $Q_{\rm R}$ increases the horizontal spread rate $(S_{\rm H})$. The minimum value of $Q_{\rm R}$ was set to 1 (corresponding to the ranges of φ and Θ values), whereas its upper limit was not found. Of the circular pattern predictions, a wide range of spread rates can be predicted by BARA by using different values of $Q_{\rm B}$, φ and Θ . However, none of the combinations of variables in Group 2 can simulate all the smouldering widths (W_s) measured in Christensen *et al.* (2020) (see Fig. 6b), but t_s , which belongs to Group 3, enabled the prediction of all the smouldering widths measured in Christensen et al. (2020) (see Fig. 6c).

The sensitivity analysis of Group 4 shows that μ does not affect the horizontal spread rate or the smouldering width significantly (within 20% uncertainty compared with above 100% uncertainty for different φ , Θ , or $Q_{\rm R}$), but μ determines the ignitability of peat in the model. With a very high μ , smouldering was not initiated; with $\mu = 0$, there was no significant change in the BARA predictions compared with the predictions with a higher μ . Therefore, the range of μ was set from 0 to 0.9. The upper limit was the maximum μ value at which smouldering was initiated, with a minimum Θ value and a maximum φ value. According to the sensitivity analysis, the order of importance of the variables in BARA is φ and Θ have the same importance, $Q_{\rm R}$ and $t_{\rm s}$ have the same importance, then $P_{\rm s}$ and lastly μ .

The six variables in BARA were calibrated against a set of three laboratory experiments (Frandsen 1987, 1997; Christensen *et al.* 2020). Of these variables, P_s is constant ($P_s = 0.1$); φ , Q_R and t_s are variables that were set to depend on peat properties because they have similar meaning to the physical variables; and Θ and μ are independent variables, which were explored within their valid ranges.

In a cell, t_s is the time required to consume the peat vertically, at a vertical spread rate of S_d , throughout its thickness (*d*); t_s was formulated as shown in Eqn 2. The vertical spread rate (S_d) was formulated as shown in Eqn 3, adapted from Christensen (2020). In Eqn 3, ρ_o is the organic density, and a_1 (-0.31 mm/min) and a_2 (110.7 kg mm/m³ min) are calibration constants from Christensen (2020).

$$t_{\rm s} = \frac{d}{S_{\rm d}} \tag{2}$$

$$S_{\rm d} = a_1 + \frac{a_2}{\rho_{\rm o}} \tag{3}$$

The formulation of $Q_{\rm R}$ was derived based on the heat generated by the combustion of peat in one time step with a constant heat generation per unit volume (see Supplementary Appendix B for derivation). $Q_{\rm R}$ depends on $\rho_{\rm o}$ and $S_{\rm d}$, as shown in Eqn 4, and is non-dimensionalised by a constant ($a_3 = 0.39 \,\mathrm{m}^2 \,\mathrm{s/kg}$), which makes the minimum value of $Q_{\rm R}$ equal to one (see the sensitivity analysis section).

$$Q_{\rm R} = a_3 \times \rho_{\rm o} \times S_{\rm d} \tag{4}$$

The formulation of φ (Eqn 5) was derived based on 1D transient heat transfer via conduction, which considers the effective thermal conductivity (k_e), which includes radiative heat transfer across pores (see Supplementary Appendix B for derivation). φ depends on ρ_b and the effective specific heat (c) of the inorganic content (IC), MC and organic content. c is the sum of the individual specific heat values multiplied by the mass fraction. φ was normalised within the range of 0.05–0.2 by using constants ($a_4 = 0.05$ and $a_5 = 78\,912$ K/m³ J).

$$\varphi = a_4 + a_5/c\rho_b \tag{5}$$

 Θ was calibrated between 0.01 and 0.2 against the experiments of Christensen (2020) under different MC, IC and bulk density (ρ_b) conditions. Meanwhile, μ was calibrated between 0 and 0.9 against the experiments of Frandsen (1987, 1997). BARA requires only the peat properties MC, IC and ρ_b as inputs, and thus can be used to simulate the spread of smouldering under any peat conditions.



Fig. 6. Sensitivity analysis of Q_R for different Θ and ϕ values based on (*a*) horizontal spread rate, and (*b*) smouldering width. Regions shaded in black represent simulations with a non-circular shape (unexpected results). (*c*) Sensitivity analysis of t_s for different Θ and ϕ values based on smouldering width. Regions shaded in black represent simulations with a non-circular shape (unexpected results).

BARA accurately simulated the experiments of Christensen *et al.* (2020) under all MC, IC and ρ_b conditions (some comparisons shown in Fig. 7); the differences between the BARA predictions and experiments based on horizontal spread rates and smouldering widths are within

10% (see Fig. 8). In Fig. 8, each blue dot represents the comparison between the prediction and the experiment under one set of MC, IC and $\rho_{\rm b}$, whereas the black line represents the experiments. When the BARA predictions are equal to the values in the experiments, the blue dots overlap the



Fig. 7. Comparison examples between the BARA predictions and the infrared images from experiments of Christensen *et al.* (2020) in the calibration process under two different conditions: (*a*) 2.5% IC and 110% MC; (*b*) 20% IC and 0% MC. *P* is *peat*, S is *smouldering* and *B* is *burnt out*. The heat value (H) was normalised within a range of 0-100 for simplicity.



Fig. 8. Calibration results of Θ in BARA against the experiments of Christensen *et al.* (2020) for horizontal spread rate (S_H) and smouldering width (W_S). The solid black line represents the target, where the predictions perfectly match the experimental results. Blue circles are the simulation results from BARA with their stochastic uncertainty after 10 repetitions. Dashed lines indicate regions within ±10% error from the experiments.

black line. The error bars represent the uncertainty in the experiments after two repetitions (*x*-axis error bar; Christensen *et al.* 2020) and the predictions (P_s makes BARA stochastic) after 10 repetitions (*y*-axis error bar); we found that the prediction uncertainty is not significant (see Fig. 8).



Fig. 9. Correlation between Θ in BARA and thermal inertia (ρkc). Black circles are predictions. Solid red line represents the best linear regression.



Fig. 10. Calibration of μ in BARA against experiments of Frandsen (1987, 1997) for the critical conditions for ignition. The region at the top right has ignition, whereas in the bottom left, there is no ignition.

From the calibration, we found that Θ exhibits a strong logarithmic correlation (R = 0.91) with thermal inertia ($k\rho_b c$), as shown in Fig. 9. We formulated Θ as shown in Eqn 6 with $a_5 = -1.194$ and $a_6 = 16.599$. Fig. 10 shows the critical IC and MC of BARA for different μ compared with experiments. For low μ values, the critical IC and MC of BARA are significantly higher than those of the experiments. For high μ values, the critical IC and MC of BARA are significantly lower than those of the experiments. When $\mu = 0.1$, the critical IC and MC of BARA show good agreement with the experiments; thus, μ was set to this value.

$$\Theta = \exp(a_5 \ln(k\rho_b c) - a_6) \tag{6}$$

After calibration, we used BARA to generate blind predictions of laboratory experiments on smouldering peat under variable dry (0% MC) and wet (60% MC) peat conditions. We studied three different spatial distributions of MC: halftone, stripes and checkerboard, shown in Fig. 11, adapted



Fig. 11. Top view of configuration of the MC distribution of laboratory-controlled experiments of Hadden and Rein (2009). Reg. in the figure represents region. The wet peat has 60% MC, whereas the dry peat has 0% MC. The experiments were conducted in a $20 \times 20 \times 6$ cm reactor with line ignition at the bottom edge of the pictures and smouldering spreading horizontally. In each configuration, there are edge regions (red dashed line), regions near the reactor sides; a middle part (blue solid line), regions relatively distant from the reactor sides; and the MC boundary (yellow solid line), locations at which peat with high MC and low MC meet.

from Hadden and Rein (2009). The BARA predictions provide good agreement against the experiments on shape similarity for the halftone, stripes and checkerboard configurations as shown in Fig. 12.

We quantified the error of the BARA predictions against the experiments based on the unburnt and burnt areas at different times, shown in Fig. 13. These areas were selected because the use of smouldering area can cause a compensation effect; the predictions and the experiments have similar areas but with significantly different shapes. The error presented in Fig. 13 is the error in unburnt and burnt areas at 10-min intervals. We found that the BARA predictions had average errors of less than 20% for halftone, stripes and checkerboard configurations in both unburnt and burnt areas.

Discussion

Fig. 12*a* compares the BARA prediction against the experiment for the halftone configuration. The smouldering front and area in the BARA prediction agree well with that of the experiment. The slower spread in wet peat and faster spread in dry peat are present in both the BARA prediction and the experiment. The shape of the edge in the BARA prediction matches the shape in the experiment, which indicates the retardation of the spread on the edge as ignition is not across the whole width (see Fig. 11).

For the stripes configuration, there are three complex phenomena in the experiment that were accurately predicted by BARA: arc creation, arc stretch and flattening (see Fig. 12b). The cause for arc creation is the same as in the halftone configuration (ignition protocol). At 1 h after ignition, this arc was stretched when the smouldering front in the middle burnt the dry peat and accelerated, whereas on the edge, the smouldering front was still burning wet peat. When the smouldering front reached the subsequent section of wet peat 3 h after ignition, it decelerated and was overtaken by the front on the edge, exhibiting a flattening phenomenon.

In the checkerboard configuration, BARA accurately predicted changes of spread direction of the smouldering front that caused several complex phenomena (see Fig. 12c). At 2h after ignition, because there is a change from wet-dry-wet to dry-wet-dry configuration, the smouldering front in the middle changes direction to spread diagonally to the dry peat; this spread creates ear-like shapes of the smouldering front. During this diagonal spread, the smouldering front on the edge encircled wet peat near the ignition, which caused the smouldering front on the edge to flatten owing to the merging of forward and backward spreads of the smouldering front on edge. The diagonal spread was observed again 4 h after ignition, but towards the middle; this spread caused another wet peat encirclement in the middle, which led to the creation of a step profile.

We found that the errors in burnt area are $\sim 10\%$ higher than the errors in unburnt area for the three configurations (see Fig. 13). These findings indicate that the rules for extinction (corresponding to t_s) can still be improved. For example, the extinction rules can be improved by calibrating BARA against the data of 2D vertical spread when available.

These results show the good ability of BARA to simulate both the horizontal and vertical spread of smouldering in peat with horizontally varying MCs (a realistic condition), in which a sequence of complex phenomena is involved. BARA has a high accuracy (above 80%) in the three MC configurations. To simulate 1 h of peat smouldering, BARA requires only an average of 3 min of computational time (with a 2.7 GHz CPU), which is 240 times faster than using physics-based models (Yuan *et al.* 2023). Therefore, BARA is a powerful and computationally efficient model to simulate multidimensional spread of smouldering in peat with horizontally varying MCs and can be used to predict its progression with faster-than-real-time simulations for mitigation purposes.

Smouldering wildfires are field-scale phenomena; thus, field-scale modelling is of utmost importance (Santoso *et al.* 2022; Robb *et al.* 2023). As BARA considers the three most important factors that affect smouldering (MC, IC and bulk density) and mainly uses non-dimensional parameters (see Table 1), it can potentially be applied to field conditions (considering the spatial and temporal variations in peat conditions) and across scales. This can be done, for instance, by scaling its non-dimensional parameters (Richter 2019; Purnomo 2022), which is a fairly simple task. Therefore, BARA has the potential to simulate smouldering wildfires at their actual scale. BARA's accuracy and scalability make it a potential component of an operational fire early warning system, a crucial tool that is currently lacking.



Recent research has laid the groundwork for such a system (Nikonovas *et al.* 2020, 2022; Wang *et al.* 2022; Mezbahuddin *et al.* 2023), and BARA's capabilities position it as a valuable addition to advance fire prevention and mitigation efforts.

Conclusion

We used CA to simulate multidimensional spread of smouldering peat with horizontally varying MCs for the first time. The model, BARA, was calibrated against laboratory experiments in homogeneous MC of Christensen *et al.* (2020). BARA was applied to generate blind predictions of the laboratory experiments with non-uniform MCs of Hadden and Rein (2009) and accurately reproduced various



phenomena observed in the experiments, such as diagonal spread and wet peat encirclement, which shows the importance of the MC spatial distribution for smouldering behaviours. These predictions agreed well with the experiments of Hadden and Rein (2009) with above 80% accuracy in smouldering area. BARA only requires 3 min to simulate 1 h of peat smouldering, highlighting its potential for fieldscale applications (Purnomo 2022). Our modelling work improves and integrates our current understanding of the multidimensional spread of smouldering fires in peats with non-uniform MCs. As it is accurate and scalable, BARA can potentially form a key part of an operational fire early warning system, which is currently lacking, although recent research has laid the foundations for such a system (Nikonovas et al. 2020, 2022; Wang et al. 2022; Mezbahuddin et al. 2023).



Fig. 13. Quantitative comparisons of burnt and unburnt areas between the BARA predictions and the experiments of smouldering peat with non-uniform MCs in (a) halftone, (b) stripes, and (c) checkerboard configurations. The errors presented here are the errors every 10 min. (d) Illustration of the burnt and unburnt areas for the comparisons.

Supplementary material

Supplementary material is available online.

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Data availability. The data that support this study are available on request.

Conflicts of interest. The authors declare no conflicts of interest.

Declaration of funding. This research was partly sponsored by European Research Council (ERC) Consolidator Grant HAZE (682587) and Indonesian Endowment Fund for Education (LPDP).

Acknowledgements. We would like to thank Rory Hadden from the University of Edinburgh for providing videos of the 2010 experiments.

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