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data_global

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_audit_creation_method      'SHELXL-97 plus manual editing'

_publ_contact_author_name   'Andrew D.Bond'
_publ_contact_author_address
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Department of Chemistry
University of Cambridge
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CB2 1EW
UK
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_publ_contact_author_email   adb29@cam.ac.uk
_publ_contact_author_fax     '(01223) 336362'
_publ_contact_author_phone   '(01223) 336352'
_publ_requested_journal      'Aust. J. Chem.'
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'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
'H' 'H' 0.0000 0.0000
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
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'-x, -y, -z'
'x, -y-1/2, z'
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Grown in-situ at 268K in a 0.3 mm Lindemann capillary tube.
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HKL Denzo and Scalepack (Otwinowski & Minor 1997)
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Refinement of F2 against ALL reflections. The weighted R-factor wR and
goodness of fit S are based on F2, conventional R-factors R are based
on F, with F set to zero for negative F2. The threshold expression of
F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
on F2 are statistically about twice as large as those based on F, and R-
factors based on ALL data will be even larger.
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_refine_ls_weighting_details
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_atom_sites_solution_secondary    difmap
_atom_sites_solution_hydrogens    geom
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'Fc2=kFc[1+0.001xFc2\l3/sin(2\q)]-1/4'
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_atom_site_symmetry_multiplicity
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_atom_site_refinement_flags
_atom_site_disorder_assembly
_atom_site_disorder_group
C1 C 0.3909(4) 0.2500 1.0137(3) 0.0482(6) Uani 1 2 d S . .
C2 C 0.2421(3) 0.36495(16) 1.0071(2) 0.0639(6) Uani 1 1 d . . .
H2A H 0.3347 0.4393 1.0100 0.091(4) Uiso 1 1 calc R . .
H2B H 0.1939 0.3663 1.1127 0.091(4) Uiso 1 1 calc R . .

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C3 C 0.0248(3) 0.36431(17) 0.8343(3) 0.0673(6) Uani 1 1 d . . .
H3A H 0.0204 0.4396 0.7646 0.082(4) Uiso 1 1 calc R . .
H3B H -0.1172 0.3613 0.8649 0.082(4) Uiso 1 1 calc R . .
C4 C 0.0375(4) 0.2500 0.7229(3) 0.0594(7) Uani 1 2 d S . .
H4 H -0.0967 0.2500 0.6077 0.073(7) Uiso 1 2 calc SR . .
C7 C 0.6189(5) 0.2500 1.1743(4) 0.0790(9) Uani 1 2 d S . .
H7A H 0.715(4) 0.1741(19) 1.169(3) 0.099(5) Uiso 1 1 d . . .
H7C H 0.592(5) 0.2500 1.288(4) 0.099(5) Uiso 1 2 d S . .
C8 C 0.2693(3) 0.2500 0.6844(3) 0.0517(6) Uani 1 2 d S . .
C9 C 0.2983(3) 0.1350(2) 0.5818(2) 0.0801(7) Uani 1 1 d . . .
H9A H 0.2939 0.0617 0.6510 0.108(4) Uiso 1 1 calc R . .
H9B H 0.4469 0.1388 0.5635 0.108(4) Uiso 1 1 calc R . .
H9C H 0.1724 0.1315 0.4659 0.108(4) Uiso 1 1 calc R . .
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C2 0.0736(11) 0.0552(11) 0.0685(12) -0.0096(9) 0.0319(10) 0.0001(8)
C3 0.0594(9) 0.0686(12) 0.0799(13) 0.0097(10) 0.0321(9) 0.0159(8)
C4 0.0420(11) 0.0758(17) 0.0531(14) 0.000 0.0078(10) 0.000
C7 0.0718(17) 0.112(3) 0.0424(15) 0.000 0.0071(14) 0.000
C8 0.0476(11) 0.0698(15) 0.0337(12) 0.000 0.0092(9) 0.000
C9 0.0841(13) 0.1007(16) 0.0573(12) -0.0200(11) 0.0269(10) -0.0013(11)
O11 0.0396(8) 0.0924(13) 0.0382(9) 0.000 0.0141(6) 0.000

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;
All esds (except the esd in the dihedral angle between two l.s. planes)
are estimated using the full covariance matrix. The cell esds are taken
into account individually in the estimation of esds in distances, angles
and torsion angles; correlations between esds in cell parameters are only
used when they are defined by crystal symmetry. An approximate (isotropic)
treatment of cell esds is used for estimating esds involving l.s. planes.
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C1 C2 1.516(2) 4_565 N
C1 C2 1.516(2) . N
C2 C3 1.521(3) . N
C2 H2A 0.9700 . N
C2 H2B 0.9700 . N
C3 C4 1.522(2) . N
C3 H3A 0.9700 . N
C3 H3B 0.9700 . N
C4 C3 1.522(2) 4_565 N
C4 C8 1.534(3) . N
C4 H4 0.9800 . N

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C7 H7A 1.01(2) . N
C7 H7C 0.97(3) . N
C8 O11 1.444(2) . N
C8 C9 1.516(2) . N
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C9 H9A 0.9600 . N
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O11 C1 C7 104.73(18) . . N
O11 C1 C2 108.84(12) . 4_565 N
C7 C1 C2 112.76(13) . 4_565 N
O11 C1 C2 108.84(12) . . N
C7 C1 C2 112.76(13) . . N
C2 C1 C2 108.72(18) 4_565 . N
C1 C2 C3 110.10(15) . . N
C1 C2 H2A 109.6 . . N
C3 C2 H2A 109.6 . . N
C1 C2 H2B 109.6 . . N
C3 C2 H2B 109.6 . . N
H2A C2 H2B 108.2 . . N
C2 C3 C4 108.26(14) . . N
C2 C3 H3A 110.0 . . N
C4 C3 H3A 110.0 . . N
C2 C3 H3B 110.0 . . N
C4 C3 H3B 110.0 . . N
H3A C3 H3B 108.4 . . N
C3 C4 C8 107.2(2) . 4_565 N
C3 C4 C8 110.28(12) . . N
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C3 C4 H4 109.7 . . N
C3 C4 H4 109.7 4_565 . N
C8 C4 H4 109.7 . . N
C1 C7 H7A 109.6(12) . . N
C1 C7 H7C 111.8(19) . . N
H7A C7 H7C 109.3(17) . . N
O11 C8 C9 107.02(12) . . N
O11 C8 C9 107.02(12) . 4_565 N
C9 C8 C9 108.8(2) . 4_565 N
O11 C8 C4 107.87(17) . . N
C9 C8 C4 112.87(12) . . N
C9 C8 C4 112.87(12) 4_565 . N
C8 C9 H9A 109.5 . . N
C8 C9 H9B 109.5 . . N
H9A C9 H9B 109.5 . . N
C8 C9 H9C 109.5 . . N
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C2 C1 C2 C3 -58.8(2) 4_565 . . . . N
C1 C2 C3 C4 -2.4(2) . . . . N
C2 C3 C4 C3 63.9(2) . . . 4_565 N
C2 C3 C4 C8 -56.1(2) . . . . N
C3 C4 C8 O11 59.08(13) . . . . N
C3 C4 C8 O11 -59.08(13) 4_565 . . . . N
C3 C4 C8 C9 177.11(15) . . . . N
C3 C4 C8 C9 58.9(2) 4_565 . . . . N
C3 C4 C8 C9 -58.9(2) . . . 4_565 N
C3 C4 C8 C9 -177.11(15) 4_565 . . 4_565 N
C7 C1 O11 C8 180.000(1) . . . . N
C2 C1 O11 C8 59.18(12) 4_565 . . . . N
C2 C1 O11 C8 -59.18(12) . . . . N
C9 C8 O11 C1 -121.72(12) . . . . N
C9 C8 O11 C1 121.72(12) 4_565 . . . . N
C4 C8 O11 C1 0.0 . . . . N

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