

Supplementary material

**Quantification of kinetic rate law parameters of uranium release from sodium autunite as a function of aqueous bicarbonate concentrations**

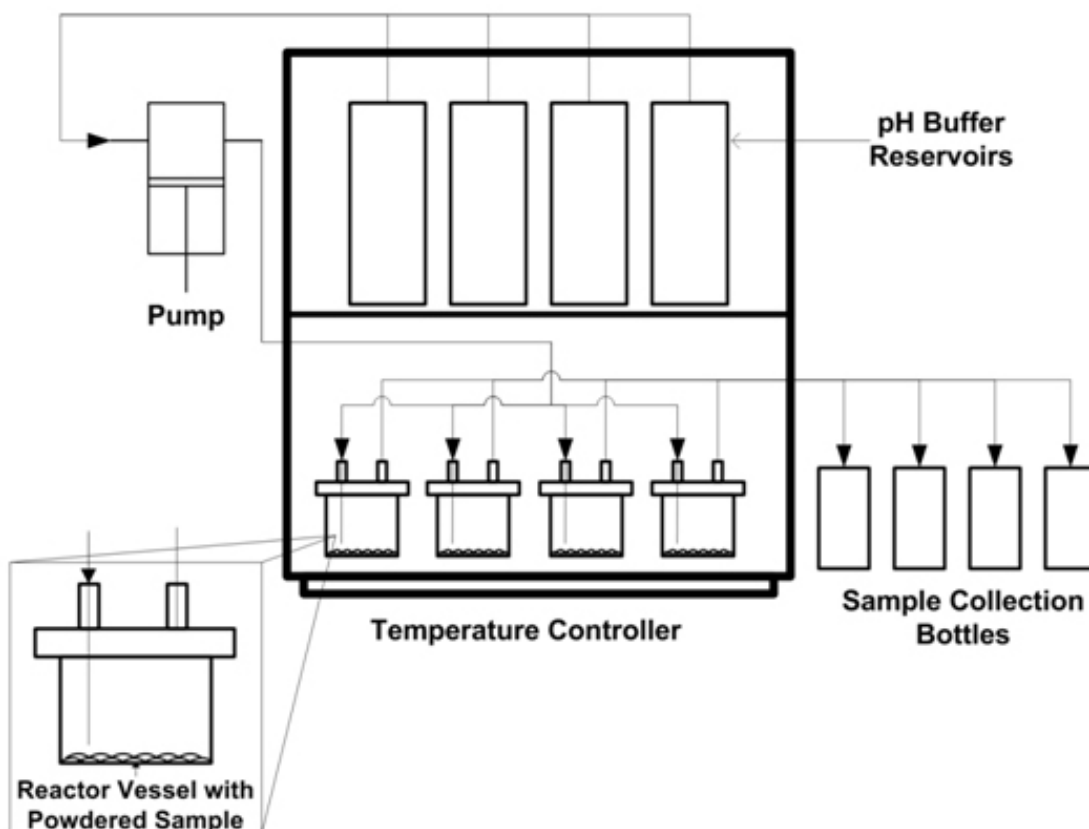
Ravi Gudavalli<sup>A,B</sup>, Yelena Katsenovich<sup>A,D</sup>, Dawn Wellman<sup>C</sup>, Leonel Lagos<sup>A</sup> and Berrin Tansel<sup>B</sup>

<sup>A</sup>Applied Research Center, Florida International University, 10555 W Flagler St, Suite 2100, Miami, FL 33174, USA.

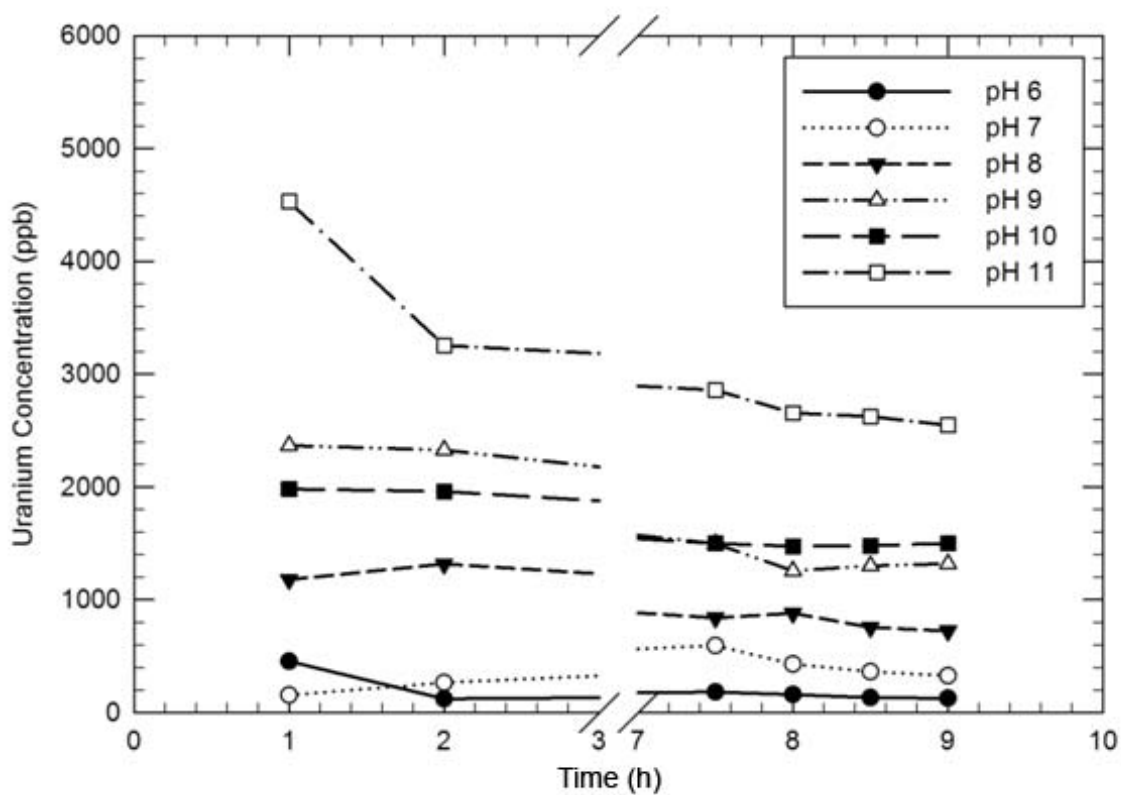
<sup>B</sup>Department of Civil and Environmental Engineering, Florida International University, 10555 W Flagler Street, Suite 3680, Miami, FL 33174, USA.

<sup>C</sup>Pacific Northwest National Laboratory, PO Box 999, K3-62, Richland, WA 99352, USA.

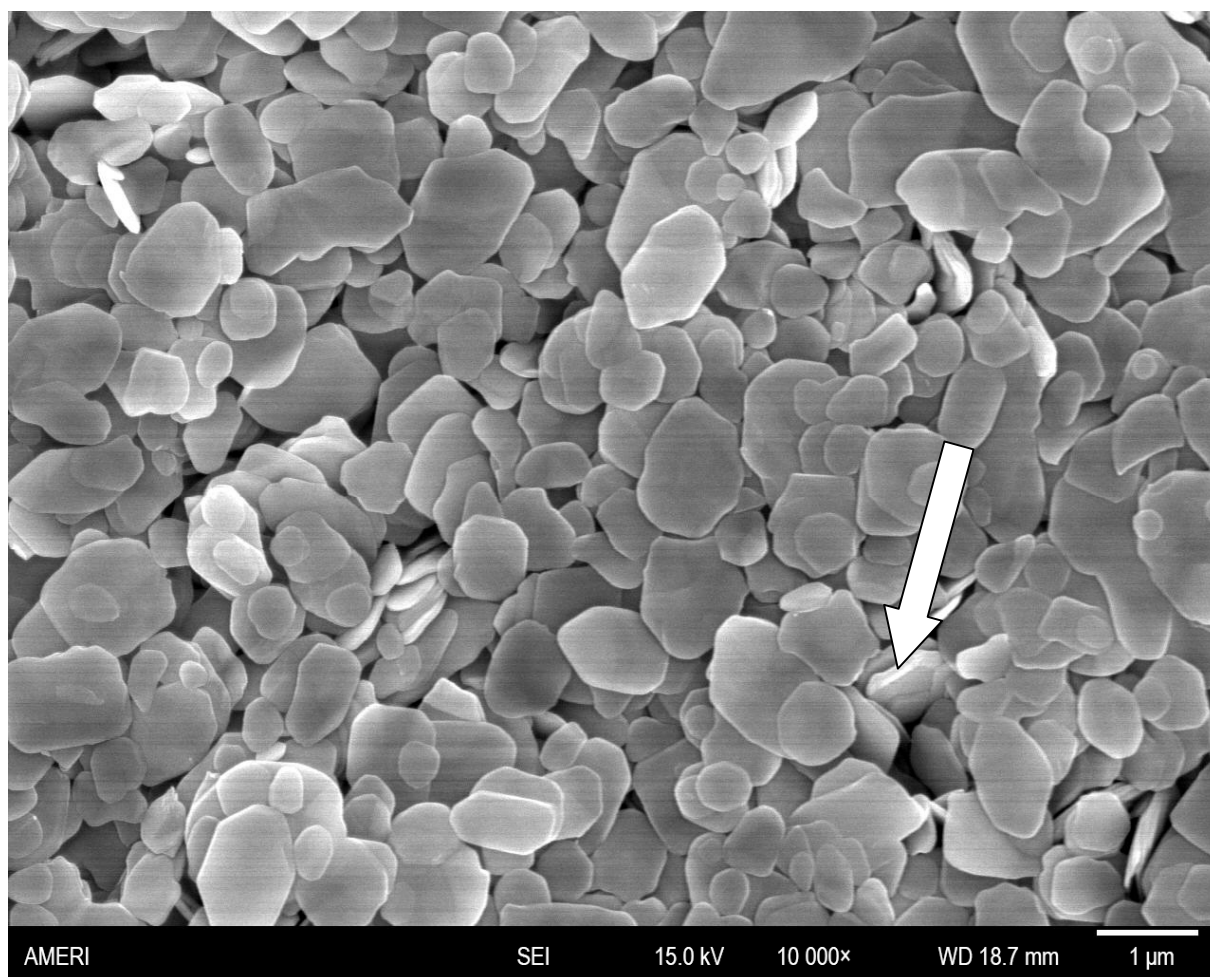
<sup>D</sup>Corresponding author. Email address: katsenov@fiu.edu



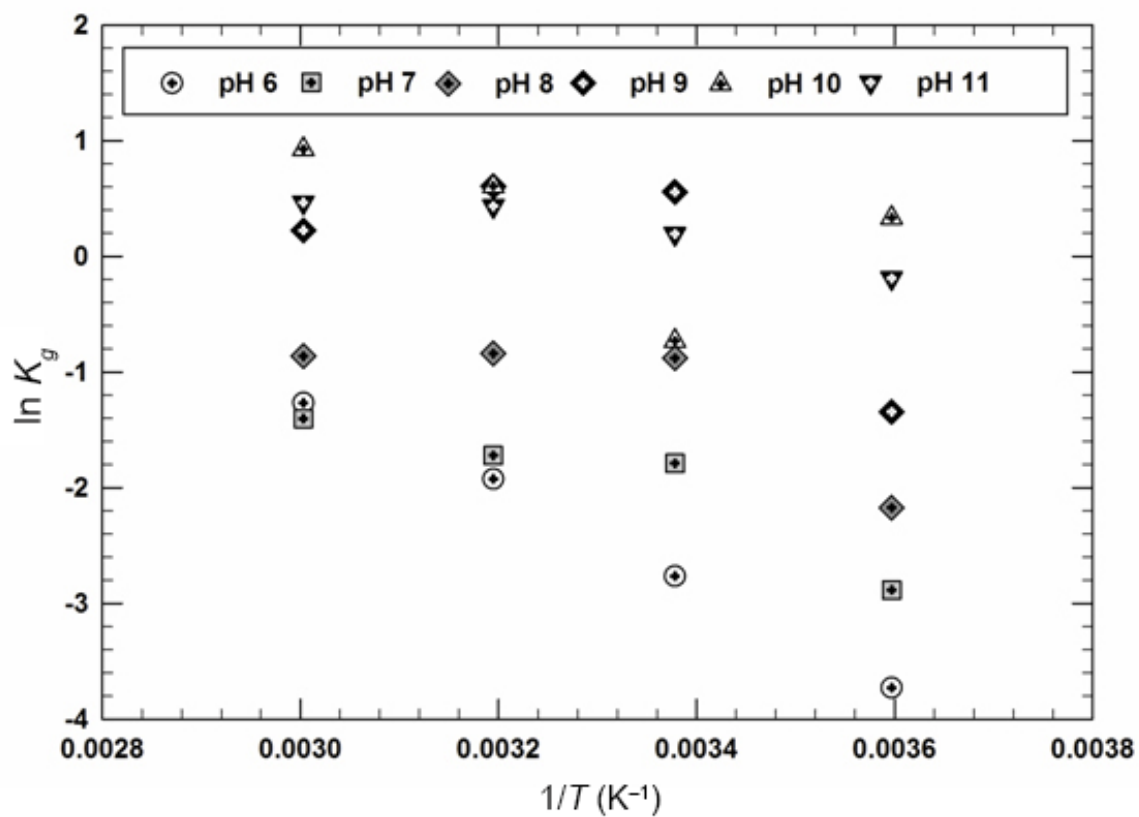
**Fig. S1.** Schematic of single-pass flow-through experimental setup showing syringe pump, reactor vessels, temperature chamber, buffer reservoirs and sample collection bottles.



**Fig. S2.** Change in uranium concentration over time for SPTF experiments for Na-autunite at 23 °C, 0.0005 M  $\text{HCO}_3^-$  and pH range 6–11



**Fig. S3.** Image of post-reacted Na-autunite minerals at 10 000 magnification showing no formation of secondary mineral phases and minor formation of cleavage planes (black arrow) occurred during the dissolution process.



**Fig. S4.** Normal logarithm of pseudo equilibrium constant as a function of inverse temperature. The resulting regression lines yield the values of enthalpy ( $\Delta H$ )

**Table S1. Composition of Tris-buffered bicarbonate solutions used in synthetic Na-autunite dissolution studies**

Solution	Composition	pH @ 23°C
1	0.01 M Tris + 0.0005 M HCO <sub>3</sub> <sup>-</sup> + 0.01096 M HCl	5.96
2	0.01 M Tris + 0.0005 M HCO <sub>3</sub> <sup>-</sup> + 0.0103 M HCl	7.00
3	0.01 M Tris + 0.0005 M HCO <sub>3</sub> <sup>-</sup> + 0.00779 M HCl	8.01
4	0.01 M Tris + 0.0005 M HCO <sub>3</sub> <sup>-</sup> + 0.00256 M HCl	9.01
5	0.01 M Tris + 0.0005 M HCO <sub>3</sub> <sup>-</sup> + 0.000147 M HCl	10.02
6	0.01 M Tris + 0.0005 M HCO <sub>3</sub> <sup>-</sup> + 0.00083 M KOH	11.00
7	0.01 M Tris + 0.001 M HCO <sub>3</sub> <sup>-</sup> + 0.0112 M HCl	6.01
8	0.01 M Tris + 0.001 M HCO <sub>3</sub> <sup>-</sup> + 0.0103 M HCl	7.02
9	0.01 M Tris + 0.001 M HCO <sub>3</sub> <sup>-</sup> + 0.00654 M HCl	8.00
10	0.01 M Tris + 0.001 M HCO <sub>3</sub> <sup>-</sup> + 0.00265 M HCl	9.01
11	0.01 M Tris + 0.001 M HCO <sub>3</sub> <sup>-</sup> + 0.000147 M HCl	10.00
12	0.01 M Tris + 0.001 M HCO <sub>3</sub> <sup>-</sup> + 0.00116 M KOH	11.00
13	0.01 M Tris + 0.002 M HCO <sub>3</sub> <sup>-</sup> + 0.0118 M HCl	6.01
14	0.01 M Tris + 0.002 M HCO <sub>3</sub> <sup>-</sup> + 0.0108 M HCl	6.99
15	0.01 M Tris + 0.002 M HCO <sub>3</sub> <sup>-</sup> + 0.00798 M HCl	7.99
16	0.01 M Tris + 0.002 M HCO <sub>3</sub> <sup>-</sup> + 0.00267 M HCl	9.01
17	0.01 M Tris + 0.002 M HCO <sub>3</sub> <sup>-</sup> + 0.00006 M KOH	10.00
18	0.01 M Tris + 0.002 M HCO <sub>3</sub> <sup>-</sup> + 0.00192 M KOH	11.00
19	0.01 M Tris + 0.003 M HCO <sub>3</sub> <sup>-</sup> + 0.0125 M HCl	6.01
20	0.01 M Tris + 0.003 M HCO <sub>3</sub> <sup>-</sup> + 0.01077 M HCl	7.01
21	0.01 M Tris + 0.003 M HCO <sub>3</sub> <sup>-</sup> + 0.00784 M HCl	8.01
22	0.01 M Tris + 0.003 M HCO <sub>3</sub> <sup>-</sup> + 0.00240 M HCl	9.01
23	0.01 M Tris + 0.003 M HCO <sub>3</sub> <sup>-</sup> + 0.000379 M KOH	9.99
24	0.01 M Tris + 0.003 M HCO <sub>3</sub> <sup>-</sup> + 0.002747 M KOH	11.00

**Table S2. Aqueous speciation reactions used in modelling**

Speciation reaction	log K	Source
$\text{UO}_2^{2+} + 3\text{CO}_3^{-2} = \text{UO}_2(\text{CO}_3)_2^{-2}$	16.61	[1]
$\text{UO}_2^{2+} + 3\text{CO}_3^{-2} = \text{UO}_2(\text{CO}_3)_3^{-4}$	21.84	[1]
$\text{UO}_2^{2+} + \text{H}_2\text{O} = \text{UO}_2(\text{OH})^+ + \text{H}^+$	-5.25	[1]
$\text{UO}_2^{2+} + 2\text{H}_2\text{O} = \text{UO}_2(\text{OH})_2(\text{aq}) + 2\text{H}^+$	-12.15	[1]
$\text{UO}_2^{2+} + 3\text{H}_2\text{O} = \text{UO}_2(\text{OH})_3^- + 3\text{H}^+$	-20.25	[1]
$\text{UO}_2^{2+} + 4\text{H}_2\text{O} = \text{UO}_2(\text{OH})_4^{-2} + 4\text{H}^+$	-32.4	[1]
$2\text{UO}_2^{2+} + \text{H}_2\text{O} = (\text{UO}_2)_2(\text{OH})^{3+} + \text{H}^+$	-2.7	[1]
$2\text{UO}_2^{2+} + 2\text{H}_2\text{O} = (\text{UO}_2)_2(\text{OH})_2^{2+} + 2\text{H}^+$	-5.62	[1]
$3\text{UO}_2^{2+} + 4\text{H}_2\text{O} = (\text{UO}_2)_3(\text{OH})_4^{2+} + 4\text{H}^+$	-11.9	[1]
$3\text{UO}_2^{2+} + 5\text{H}_2\text{O} = (\text{UO}_2)_3(\text{OH})_5^+ + 5\text{H}^+$	-15.55	[1]
$3\text{UO}_2^{2+} + 6\text{CO}_3^{-2} = (\text{UO}_2)_3(\text{CO}_3)_6^{-6}$	54.0	[1]
$3\text{UO}_2^{2+} + 7\text{H}_2\text{O} = (\text{UO}_2)_3(\text{OH})_7^- + 7\text{H}^+$	-32.2	[1]
$4\text{UO}_2^{2+} + 7\text{H}_2\text{O} = (\text{UO}_2)_4(\text{OH})_7^+ + 7\text{H}^+$	-21.9	[1]
$\text{H}_2\text{CO}_3 = \text{H}^+ + \text{HCO}_3^-$	-6.35	[1]
$\text{H}_2\text{CO}_3 = 2\text{H}^+ + \text{CO}_3^{-2}$	-16.68	[1]
$\text{H}^+ + \text{PO}_4^{-3} = \text{HPO}_4^{-2}$	12.375	[2]
$\text{K}^+ + \text{H}^+ + \text{PO}_4^{-3} = \text{KHPO}_4^-$	13.25	[2]
$2\text{K}^+ + \text{H}^+ + \text{PO}_4^{-3} = \text{K}_2\text{HPO}_4(\text{aq})$	13.5	[2]
$\text{UO}_2^{2+} + \text{PO}_4^{-3} = \text{UO}_2\text{PO}_4^-$	13.23	[2]
$\text{UO}_2^{2+} + \text{PO}_4^{-3} + \text{H}^+ = \text{UO}_2\text{HPO}_4(\text{aq})$	19.61	[2]
$\text{UO}_2^{2+} + \text{PO}_4^{-3} + 2\text{H}^+ = \text{UO}_2\text{H}_2\text{PO}_4^+$	20.69	[2]
$\text{UO}_2^{2+} + \text{PO}_4^{-3} + 3\text{H}^+ = \text{UO}_2\text{H}_3\text{PO}_4^{2+}$	22.48	[2]

**Table S3. Single-Pass flow-through experimental conditions and dissolution rates of synthetic sodium autunite**

Sample ID	Surface area (m <sup>2</sup> )	Temperature (°C)	pH (23 °C)	Flow rate (mL day <sup>-1</sup> )	U (µg L <sup>-1</sup> )	U rate (mol m <sup>-2</sup> s <sup>-1</sup> )	
0.0005 M HCO <sub>3</sub> <sup>-</sup>							
SAUT-01	1.07	5	6	1014	24.3	$2.74 \times 10^{-12}$	$(5.31 \times 10^{-13})$
SAUT-02	1.09	5	7	1021	41.2	$3.600 \times 10^{-12}$	$(6.98 \times 10^{-13})$
SAUT-03	1.03	5	8	1022	79.5	$7.02 \times 10^{-12}$	$(1.36 \times 10^{-12})$
SAUT-04	0.97	5	9	976	404.8	$3.66 \times 10^{-11}$	$(7.10 \times 10^{-12})$
SAUT-05	0.65	5	10	1020	2057.8	$2.94 \times 10^{-10}$	$(4.09 \times 10^{-11})$
SAUT-06	0.59	5	11	1003	414.7	$6.30 \times 10^{-11}$	$(1.22 \times 10^{-11})$
SAUT-07	1.59	23	6	1016	245.9	$1.9 \times 10^{-12}$	$(3.69 \times 10^{-13})$
SAUT-08	1.18	23	7	976	279.4	$2.084 \times 10^{-11}$	$(4.036 \times 10^{-12})$
SAUT-09	1.59	23	8	952	1025.2	$2.54 \times 10^{-11}$	$(1.45 \times 10^{-11})$
SAUT-10	1.18	23	9	1030	1075.8	$8.55 \times 10^{-11}$	$(2.46 \times 10^{-11})$
SAUT-11	1.60	23	10	822	2070.4	$7.83 \times 10^{-11}$	$(8.77 \times 10^{-12})$
SAUT-12	1.59	23	11	997	2799.0	$1.12 \times 10^{-10}$	$(2.17 \times 10^{-11})$
SAUT-13	0.89	40	6	1483	85.6	$1.28 \times 10^{-11}$	$(2.49 \times 10^{-12})$
SAUT-14	0.89	40	7	1500	177.7	$2.685 \times 10^{-11}$	$(5.19 \times 10^{-12})$
SAUT-15	1.63	40	8	1474	496.0	$4.06 \times 10^{-11}$	$(1.43 \times 10^{-11})$
SAUT-16	0.88	40	9	1513	706.7	$1.10 \times 10^{-10}$	$(2.12 \times 10^{-11})$
SAUT-17	1.58	40	10	1512	1652.9	$1.43 \times 10^{-10}$	$(3.84 \times 10^{-11})$
SAUT-18	1.12	40	11	1508	1161.0	$1.33 \times 10^{-10}$	$(2.58 \times 10^{-11})$
SAUT-19	0.88	60	6	1910	68.6	$1.32 \times 10^{-11}$	$(2.55 \times 10^{-12})$
SAUT-20	1.61	60	7	2429	214.9	$2.94 \times 10^{-11}$	$(7.92 \times 10^{-12})$
SAUT-21	1.14	60	8	2448	640.7	$1.24 \times 10^{-11}$	$(2.41 \times 10^{-12})$
SAUT-22	0.89	60	9	2425	1766.7	$4.35 \times 10^{-11}$	$(6.46 \times 10^{-11})$
SAUT-23	1.16	60	10	2442	1816.2	$3.52 \times 10^{-10}$	$(6.81 \times 10^{-11})$
SAUT-24	0.89	60	11	2435	681.9	$1.90 \times 10^{-10}$	$(3.68 \times 10^{-11})$
0.001 M HCO <sub>3</sub> <sup>-</sup>							
SAUT-25	0.46	5	6	990	9.573	$1.94 \times 10^{-12}$	$(1.98 \times 10^{-13})$
SAUT-26	0.77	5	7	989	32.123	$3.70 \times 10^{-12}$	$(7.16 \times 10^{-13})$
SAUT-27	0.77	5	8	1003	99.458	$1.18 \times 10^{-11}$	$(2.28 \times 10^{-12})$
SAUT-28	0.76	5	9	1021	414.558	$5.04 \times 10^{-11}$	$(9.76 \times 10^{-12})$
SAUT-29	0.69	5	10	1002	2131.330	$2.79 \times 10^{-10}$	$(3.88 \times 10^{-11})$
SAUT-30	0.55	5	11	986	683.31	$1.10 \times 10^{-10}$	$(2.12 \times 10^{-11})$
SAUT-31	1.17	23	6	976	14.4	$1.4 \times 10^{-12}$	$(2.1 \times 10^{-13})$
SAUT-32	0.88	23	7	973	48.5	$2.47 \times 10^{-11}$	$(6.99 \times 10^{-13})$

Sample ID	Surface area (m <sup>2</sup> )	Temperature (°C)	pH (23 °C)	Flow rate (mL day <sup>-1</sup> )	U (µg L <sup>-1</sup> )	U rate (mol m <sup>-2</sup> s <sup>-1</sup> )	
SAUT-33	1.18	23	8	980	654.0	$3.58 \times 10^{-11}$	$(5.98 \times 10^{-12})$
SAUT-34	1.18	23	9	971	1605.6	$1.27 \times 10^{-10}$	$(2.46 \times 10^{-11})$
SAUT-35	0.88	23	10	1001	799.9	$8.23 \times 10^{-11}$	$(8.77 \times 10^{-12})$
SAUT-36	1.14	23	11	1000	1303.3	$1.00 \times 10^{-10}$	$(1.94 \times 10^{-11})$
SAUT-37	0.88	40	6	1509	102.6	$1.59 \times 10^{-11}$	$(3.09 \times 10^{-12})$
SAUT-38	0.88	40	7	1514	191.4	$2.99 \times 10^{-11}$	$(5.80 \times 10^{-12})$
SAUT-39	0.88	40	8	1518	315.4	$5.36 \times 10^{-11}$	$(9.54 \times 10^{-12})$
SAUT-40	0.89	40	9	1528	832.0	$1.09 \times 10^{-10}$	$(2.12 \times 10^{-11})$
SAUT-41	1.59	40	10	1495	1589.8	$1.88 \times 10^{-10}$	$(2.61 \times 10^{-11})$
SAUT-42	1.13	40	11	1507	1548.1	$1.92 \times 10^{-10}$	$(3.71 \times 10^{-11})$
SAUT-43	0.89	60	6	2430	21.2	$7.15 \times 10^{-12}$	$(1.35 \times 10^{-12})$
SAUT-44	0.87	60	7	2443	64.9	$3.64 \times 10^{-11}$	$(2.44 \times 10^{-12})$
SAUT-45	1.12	60	8	2412	194.3	$3.78 \times 10^{-11}$	$(7.33 \times 10^{-12})$
SAUT-46	1.16	60	9	2452	615.2	$1.17 \times 10^{-10}$	$(2.26 \times 10^{-11})$
SAUT-47	1.13	60	10	2442	2433.2	$4.60 \times 10^{-10}$	$(9.21 \times 10^{-11})$
SAUT-48	1.55	60	11	2447	1757.6	$2.50 \times 10^{-10}$	$(4.85 \times 10^{-11})$
0.002 M HCO <sub>3</sub> <sup>-</sup>							
SAUT-49	0.61	5	6	977	20.3	$2.95 \times 10^{-12}$	$(4.11 \times 10^{-13})$
SAUT-50	0.84	5	7	1037	68.2	$7.65 \times 10^{-12}$	$(1.48 \times 10^{-12})$
SAUT-51	1.03	5	8	1019	152.6	$1.37 \times 10^{-11}$	$(2.65 \times 10^{-12})$
SAUT-52	0.82	5	9	976	551.1	$5.90 \times 10^{-11}$	$(1.14 \times 10^{-11})$
SAUT-53	0.59	5	10	1003	2060	$3.13 \times 10^{-10}$	$(4.36 \times 10^{-11})$
SAUT-54	0.59	5	11	1004	946.1	$1.49 \times 10^{-10}$	$(2.89 \times 10^{-11})$
SAUT-55	0.88	23	6	994	13.9	$1.73 \times 10^{-12}$	$(2.08 \times 10^{-13})$
SAUT-56	1.18	23	7	961	388.2	$2.86 \times 10^{-11}$	$(5.54 \times 10^{-12})$
SAUT-57	1.18	23	8	966	393.1	$3.59 \times 10^{-11}$	$(6.34 \times 10^{-12})$
SAUT-58	1.59	23	9	955	3851.3	$2.12 \times 10^{-10}$	$(5.57 \times 10^{-11})$
SAUT-59	1.12	23	10	976	1727.2	$1.35 \times 10^{-10}$	$(1.88 \times 10^{-11})$
SAUT-60	0.89	23	11	978	1154.2	$1.16 \times 10^{-10}$	$(2.21 \times 10^{-11})$
SAUT-61	0.88	40	6	1492	191.4	$2.70 \times 10^{-11}$	$(5.23 \times 10^{-12})$
SAUT-62	0.86	40	7	1504	265.5	$4.17 \times 10^{-11}$	$(8.09 \times 10^{-12})$
SAUT-63	0.86	40	8	1506	460.3	$7.26 \times 10^{-11}$	$(1.40 \times 10^{-11})$
SAUT-64	0.87	40	9	1517	1576.9	$2.49 \times 10^{-10}$	$(4.83 \times 10^{-11})$
SAUT-65	1.63	40	10	1512	3386.3	$2.77 \times 10^{-10}$	$(5.40 \times 10^{-11})$
SAUT-66	1.14	40	11	1502	2196.0	$2.62 \times 10^{-10}$	$(5.07 \times 10^{-11})$



Sample ID	Surface area (m <sup>2</sup> )	Temperature (°C)	pH (23 °C)	Flow rate (mL day <sup>-1</sup> )	U (µg L <sup>-1</sup> )	U rate (mol m <sup>-2</sup> s <sup>-1</sup> )	
SAUT-67	0.86	60	6	2432	55.7	$1.86 \times 10^{-11}$	$(2.11 \times 10^{-12})$
SAUT-68	1.15	60	7	2450	241.3	$4.65 \times 10^{-11}$	$(9.01 \times 10^{-12})$
SAUT-69	1.14	60	8	2455	203.4	$4.64 \times 10^{-11}$	$(7.65 \times 10^{-12})$
SAUT-70	0.89	60	9	2440	633.5	$1.75 \times 10^{-10}$	$(2.33 \times 10^{-11})$
SAUT-71	0.88	60	10	2445	1833.1	$4.70 \times 10^{-10}$	$(6.78 \times 10^{-11})$
SAUT-72	1.17	60	11	2430	1723.1	$3.23 \times 10^{-10}$	$(6.26 \times 10^{-11})$
0.003 M HCO <sub>3</sub> <sup>-</sup>							
SAUT-73	0.60	5	6	1016	34.7	$5.41 \times 10^{-12}$	$(7.52 \times 10^{-13})$
SAUT-74	0.83	5	7	990	92.8	$9.85 \times 10^{-12}$	$(1.91 \times 10^{-12})$
SAUT-75	0.82	5	8	994	204.2	$2.22 \times 10^{-11}$	$(4.31 \times 10^{-12})$
SAUT-76	0.88	5	9	973	709.5	$7.08 \times 10^{-11}$	$(1.37 \times 10^{-11})$
SAUT-77	0.64	5	10	973	3380.0	$4.64 \times 10^{-10}$	$(6.45 \times 10^{-11})$
SAUT-78	0.65	5	11	995	1218.6	$1.69 \times 10^{-10}$	$(3.28 \times 10^{-11})$
SAUT-79	1.19	23	6	986	150.8	$9.88 \times 10^{-12}$	$(2.18 \times 10^{-12})$
SAUT-80	1.19	23	7	995	427.9	$4.23 \times 10^{-11}$	$(6.25 \times 10^{-12})$
SAUT-81	0.88	23	8	1001	798.8	$8.13 \times 10^{-11}$	$(1.21 \times 10^{-11})$
SAUT-82	0.89	23	9	982	1329.5	$1.55 \times 10^{-10}$	$(2.57 \times 10^{-11})$
SAUT-83	1.12	23	10	982	1487.4	$1.17 \times 10^{-10}$	$(1.63 \times 10^{-11})$
SAUT-84	0.89	23	11	978	2670.8	$2.64 \times 10^{-10}$	$(3.92 \times 10^{-11})$
SAUT-85	0.87	40	6	1501	188.1	$2.94 \times 10^{-11}$	$(5.69 \times 10^{-12})$
SAUT-86	0.87	40	7	1508	305.1	$4.76 \times 10^{-11}$	$(9.22 \times 10^{-12})$
SAUT-87	1.14	40	8	1501	1113.4	$1.32 \times 10^{-10}$	$(2.56 \times 10^{-11})$
SAUT-88	1.12	40	9	1504	2748.5	$3.31 \times 10^{-10}$	$(6.42 \times 10^{-11})$
SAUT-89	0.87	40	10	1477	1665.9	$2.54 \times 10^{-10}$	$(3.77 \times 10^{-11})$
SAUT-90	1.15	40	11	1512	2737.6	$3.26 \times 10^{-10}$	$(6.31 \times 10^{-11})$
SAUT-91	1.15	60	6	2431	238.9	$4.58 \times 10^{-11}$	$(8.86 \times 10^{-12})$
SAUT-92	1.59	60	7	2442	310.8	$6.00 \times 10^{-11}$	$(1.16 \times 10^{-11})$
SAUT-93	0.86	60	8	2432	274.9	$6.98 \times 10^{-11}$	$(1.03 \times 10^{-11})$
SAUT-94	0.87	60	9	2426	743.7	$2.04 \times 10^{-10}$	$(2.76 \times 10^{-11})$
SAUT-95	0.86	60	10	2429	2736.3	$6.98 \times 10^{-10}$	$(1.03 \times 10^{-10})$
SAUT-96	1.14	60	11	2421	2026.7	$3.89 \times 10^{-10}$	$(7.53 \times 10^{-11})$

## References

- [1] R. Guillaumont, T. Fanghänel, J. Fuger, I. Grenthe, V. Neck, D. A. Palmer, M. H. Rand M.H, *Update on the Chemical Thermodynamics of Uranium, Neptunium, Plutonium, Americium and Technetium*, **2003**, Vol. 5, (Elsevier for OECD Nuclear Energy Agency).
- [2] *Critically Selected Stability Constants of Metal Complexes Database, version 8.0* **2010** (National Institute of Standards and Technology: Gaithersburg, MD).