

Olympic Dam seismic revisited: reprocessing of deep crustal seismic data using partially preserved amplitude processing

Tom Wise*

Geological Survey of South Australia 101 Grenfell St, Adelaide, SA 5000 Tom.Wise@sa.gov.au

Adrian Fabris

Geological Survey of South Australia 101 Grenfell St, Adelaide, SA 5000 Adrian.Fabris@sa.gov.au

Don Pridmore

HiSeis Pty Ltd Bentley, WA 6102 d.pridmore@hiseis.com

*presenting author asterisked

Anthony Reid

Geological Survey of South Australia 101 Grenfell St, Adelaide, SA 5000 Anthony.Reid@sa.gov.au

Simon van der Wielen

Geological Survey of South Australia 101 Grenfell St, Adelaide, SA 5000 Simon.vanderWielen@sa.gov.au

Graham Heinson

Geology and Geophysics, University of Adelaide Adelaide SA 5005 graham.heinson@adelaide.edu.au

Sara Jakica HiSeis Pty Ltd Bentley, WA 6102

Sasha Ziramov

Department of Exploration Geophysics, Curtin University Bentley, WA 6102 Sasha.Ziramov@curtin.edu.au

Paul Soeffky

Geology and Geophysics, University of Adelaide Adelaide SA 5005 paul.soeffky@adelaide.edu.au

SUMMARY

Two deep crustal seismic profiles, centred on the Olympic Dam Cu-Au-U deposit, were reprocessed by HiSeis Pty Ltd. using a proprietary method. This processing method aimed to enhance subtle variations in signal strength and highlight upper crustal discontinuities. The resulting images enable interpretation of steep structures and regions of enhanced/reduced reflectivity possibly associated with large-scale alteration zones. This work highlights additional information within these deep crustal seismic lines that illuminate different aspects of the geology.

Key words: Seismic, Olympic Dam, IOCG, Alteration, Conductivity

INTRODUCTION

Deep seismic reflection data is collected around the world in order to image the structure of the crust. Two dimensional seismic data can be processed in a variety of ways, each technique permitting investigation of different aspects of the data and thus of the geology the line is transecting. A focus of deep crustal seismic surveys has been to investigate the nature of the lower crust, the geometry across the Moho, or the geometry of paleosuture zones between crustal blocks (Hammer et al., 2010; Kennett et al., 2013). The processing methods that are applied in order to image the Moho at depths of 30 to 50km, can be adjusted to enhance the reflectivity features in the upper crust. For example, the application of a low pass filter emphasizes continuity between individual seismic traces, which enhances consistency between individual traces to produce a 'smooth' image.

An alternative method to extract more detail on the upper crust is to apply a processing method known as Partially Preserved Amplitude (PPA) processing, a proprietary method of HiSeis Pty Ltd. (Jakica and Pridmore, 2014). This processing technique emphasizes variations in signal strength by preserving the temporal relative amplitude ratio, which has the effect of sharpening the output image. This resulting image is more sensitive to fabric within a rock, particularly in the upper crust but also in the presence of discontinuities.



Figure 1; Location map of seismic lines 03GA-OD1 and 03GA-OD2

In this paper we provide new observations on the upper and middle crust around the Olympic Dam Cu-Au-U deposit, South Australia, from seismic data re-processed using the PPA technique. Olympic Dam is the type example of hematite breccia iron oxide-Cu-Au (IOCG) style deposits (Williams, Barton, Fontboté et al., 2005; Skirrow, 2009) and lies buried ~400m beneath sedimentary cover of the Stuart Shelf. A major challenge to exploration in much of the Olympic Cu-Au Province is thick sedimentary cover that results in a reliance on geophysical data and limited drillholes to obtain an understanding of the geology. In

2003, two orthogonal deep crustal seismic lines were acquired by Geoscience Australia, centered on the Olympic Dam deposit (03GA-OD1 and 03GA-OD2; Figure. 1; Goleby et al. 2003). Seismic images with original Geoscience Australia processing were downloaded from the Geoscience Australia website (http://www.ga.gov.au/metadata-gateway/metadata/record/gcat_74869). We discuss some of the geological features that appear to be enhanced using PPA processing and suggest that seismic data may be directly imaging the hematite alteration associated with the Olympic Dam deposit.

Seismic data acquisition and processing

The seismic reflection data was collected in 2003 along two broadly orthogonal lines totalling ~250km (Jones et al, 2005). The longer of the two lines known as 03GA-OD1 was 193 km long and oriented approximately north–south, broadly orthogonal to the regional strike. The shorter line, 03GA-OD2 was 57 km long and oriented approximately east–west, thus providing a three-dimensional image of the Olympic Dam region (Figure. 1). The lines were recorded to 18 s two way time, equivalent to ~55 km depth at a sample rate of 2 ms using three in-line 60,000 lb vibrators (IVI HEMI60) as the energy source. Vibration points were 80 m apart and three upsweeps of 12 s-duration, with a frequency sweep of 7 to 56 Hz, 12 to 80 Hz and 8 to 72 Hz at each vibration point. Receiver groups were spaced at 40 m intervals with 12 geophones being spaced at 3.33 m apart. The data were correlated in SEG-Y format (Jones et al, 2005).

The original processing of surveys 03GA-OD1 and 03GA-OD2 was conducted by Geoscience Australia using the Disco software package. The processing workflow was designed to image the entire crust while avoiding down grading the data in the near surface (Jones et al, 2005). The processing work flow summarised in Table 1 consists of crooked line processing, refraction statics corrections, velocity analysis, spectral equalisation, sort to common mid-point gathers, dip moveout corrections, stack, post-stack migration, bandpass filtering and post-stack signal enchantment (digistack).

HiSeis Pty Ltd reprocessed approximately 160 km of surveys 03GA-OD1 and 03GA-OD2 with the aim to enhance structural and stratigraphic features in the top 5 km as well as attempting to image alteration related to IOCG mineralisation (Jakica and Pridmore, 2014) whilst preserving the amplitude integrity. The processing work flow used by HiSeis is summarised in Table 1. Attention was paid to attenuating strong noise trains (such as vehicles travelling along the seismic line whilst data was being acquired) during the pre-processing phase to better image shallow features (Jakica and Pridmore, 2014). The main difference to the Geoscience Australia processing work flow (Jones et al, 2005) is that HiSeis used partially preserved amplitude processing and in deeper areas a low-pass filter, and did not use 3 trace running mix nor digistack.

Initially, Constant Velocity Stacks (CVS) were used to obtain a velocity function for input into the residual static calculation and dip-moveout (DMO). The final Interactive Velocity Analysis (IVA) was carried out on DMO-corrected gathers in order to reduce velocities of dipping reflectors and obtain the velocity model that was used for migration. Quality control stacks were created and used as the basis on which to judge improvement of the data after subsequent processing steps. The application of DMO correction, or partial pre-stack migration, removes any dipping component to seismic events in common depth point (CDP) gathers, and solves conflicting dips at consecutive CDP positions. The edges of faults are more clearly defined and the resolution of events is increased. The application of DMO also facilitates the use of a post-stack migration algorithm as the final processing step of the data. A post-stack phase-shift migration was applied to migrate the seismic events to their true geological position. This typically results in dipping events steepening and moving up-dip. The algorithm migrates data, regardless of where the energy was reflected from in 3D space and therefore geological features out of the 2D plane will appear within the 2D plane.

Observations and discussion on the reprocessed data

While broadly similar features can be observed with both processing techniques (Figure 2), the PPA technique enables several distinct features to be detected. Three features of particular interest in the PPA processed data near the Olympic Dam deposit are described herein.



Figure 2; North-south line 03GA-OD1: HiSeis partially preserved amplitude processing (top) and Geoscience Australia original processing (bottom).

Detection of Fe-oxide alteration associated with Olympic Dam deposit within the Burgoyne Batholith

The Burgoyne Batholith, a large Hiltaba Suite granite in which the Olympic Dam deposit is hosted, has previously been identified by potential field data and drillhole intersections. It is broadly imaged as a non-reflective zone within both 03GA-OD01 and 03GA-OD02 allowing interpretation of its extent both laterally and vertically. Of particular interest, is a zone with numerous stronger reflectors within this generally non-reflective body (Figure 3). On the north-south line (03GA-OD1), the reflective zone narrows at depth and is made up of sub-horizontal reflectors typically several hundred meters long at depths ranging from ~400m to ~4000m (between 683000mE 6628500mN and 684300 mE 6631450 mN) with a width of approximately 3000 m (Figure 3a, c and d) and corresponds to the known location of the Olympic Dam orebody. These reflectors are bound by narrow, semi-continuous, subvertical and non-reflective features. This more reflective zone correlates with a high gravity (and elevated magnetic) response (Figure 3f). Taken together, the seismic and potential field data suggest that these seismic features are likely imaging the Fe-oxide alteration of the Olympic Dam Breccia Complex (Jakica and Pridmore, 2014), which demonstrated that the contact between Fe-oxide alteration and silica-rich lithologies should be reflective, and hence can be imaged with reflection seismic techniques.



Figure 3; North-south line 03GA-OD1. (a) HiSeis partially preserved amplitude processing displaying the zone of high reflectivity (red box) within the non-reflective zone of Hiltaba Suite granite. (b) Geoscience Australia original processing. (c) Enlarged section of HiSeis processed line showing increased reflectivity and possible vertical fractures (examples highlighted in black). Unmodified low reflectivity zones shown in orange. (d) Enlarged section of HiSeis processed line superimposed over Ehrig et al (2012) breccia complex cross-section. This shows a correlation between the known distribution of >5% total Fe in Hiltaba Suite granite and the zone of high reflectivity made up of subhorizontal reflectors typically several hundred metres long (~300 m wide at ~400–4000 m depth). (e) Ehrig, McPhie and Kamenetsky (2012) plan view of the Olympic Dam breccia complex. The cross-section displayed in (d) is positioned ~3 km east, and is subparallel to the seismic line.

An approximate section through Olympic Dam can be projected onto line 03GA-OD1 (N-S line; Figure 4d and e). This shows an approximate correlation between the known distribution of >5% total Fe in Hiltaba granite from Ehrig et al, (2012) and the more reflective zone. This suggests that the seismic data can directly map the extent of Fe alteration and may be a potential exploration tool for this style of deposit in deeply covered terrains.

Similar seismic features appears on the E-W line (03GA-OD2) at depths from ~900 m to ~2500 m (Figure 4b), which is slightly deeper than on the N-S line. This apparent difference in depth may be a result of out-of-plane effects, imaging reflectors not directly beneath the line. In such a situation, the reflectors coming from the dense body take longer to return to the receivers, and hence appear deeper in a 2-D section. The displacement of the seismic feature is consistent with the reflectors being derived from the dense Fe-alteration related to the Olympic Dam system.

Using the conventional Automatic Gain Control (AGC) processing, these amplitude differences between seismic events are normalised and hence the change in reflectivity is more difficult to detect. PPA processing preserves the amplitude differences of the reflections to the extent the data quality permits, and better represents the amplitude variation related to contacts of different lithologies and textures. Using PPA processing, a zone with distinct reflectors is imaged underneath the Olympic Dam deposit and is interpreted to reflect different lithologies of the deposit, with narrow, sub-vertical non-reflective features potentially mapping the location of faults through the system (Figure 3c). A series of short but distinct reflectors extends from the base of the projected section of known Fe-alteration at Olympic Dam (Figure 3d) and may represent the extension of Fe-alteration within narrow structures at depth.



Figure 4; Central section of east-west line 03GA-OD2 displaying differing geometries of folding and faulting. HiSeis partially preserved amplitude processing: (a) un-interpreted seismic data; (b) partially interpreted seismic section (note that only interpretations in the middle part of the section are shown in this figure). Geoscience Australia original processing: (c) un-interpreted seismic data; (d) original Geoscience Australia interpretations (Drummond et al. 2006).

Steep faults within the upper crust

The processing sequence used by HiSeis enables imaging of steeper structures than that used by Jones et al (2005). One of the dominant features of the E-W profile in both the PPA and original GA processed lines is a highly reflective zone beneath the interpreted Hiltaba Suite granite (Figure 4). Using both methods, this zone appears to be disrupted by major west dipping faults. However, using the PPA reprocessed image, the lateral continuity of reflectors appears to stop against a zone of low reflectivity

that forms an apparent wedge shape, the edges of which are orientated at $\sim 70^{\circ}$ and $\sim 45^{\circ}$ (Figure 4). The original interpretation emphasised the lower bound of this zone and hence the area was considered to represent a low angle, west-dipping fault (Figure 4). In the reprocessed data, the eastern boundary of this low amplitude zone is much steeper, and could be interpreted as a wedge of rock between two faults.

Whilst one example is highlighted in this paper, a thorough interpretation of these re-processed lines is warranted as it may have significant implications for the structural architecture and style in the region. A possible inference that could be drawn from the identification of more steep structures in this region is that deformation in the Olympic Dam region may not have developed as a purely fold-thrust regime as proposed by Drummond et al. (2006).

Regional sub-vertical zones of low seismic reflectivity

One of the features evident in the seismic data is a mid-upper crustal zone of high reflectivity at 10km depth which is particularly prominent in the N-S line. In the original processed image, the top of this mid-crustal layer is well defined and appears to shallow to the north-east. Drummond et al. (2006) described this zone as being dominated by laterally continuous sub-horizontal reflectors, between which lateral reflections of limited extent vary from sub-horizontal to north-dipping. These reflectors were interpreted from the original imagery as being faults associated with apparent roll over structures (Drummond et al. 2006)

In the reprocessed image this reflective zone, while still evident, does not show the same evidence for dipping reflectors. Rather, disruption to the lateral continuity is evident as a series of broadly sub-vertical zones of lower reflectivity with widths up to ~5 to 10km (Figure 5). These apparent sub-vertical zones appear throughout the N-S line and are shown on Figure 5. Four of these zones correspond to the approximate position of known IOCG deposits or prospects (A- Wirrda Well; B-Olympic Dam; C-Vulcar; D-Titan). Such zones of reduced reflectivity are potentially caused by pervasive textural destruction of large regions of the crust. Textural destruction on this scale may be caused by geological processes such as fluid migration either in the form of partial melt migration, or via pervasive hydrothermal alteration. Melt movement through sub-vertical vein networks (e.g. Brown, 1994; Diener et al, 2014) could readily explain the lack of laterally continuous reflectors observed in these regions of the crust. Large scale granitic plutonism is observed above, or proximal to, these broad zones of reduced reflectivity, e.g. Burgoyne Batholith, which is consistent with this notion. Hydrothermal alteration, as suggested above, may link these features to the broad zones of enhanced electrical conductance observed in regional magnetotelluric data in the vicinity of Olympic Dam (Heinson et al, 2006; Thiel and Heinson, 2015).



Figure 5; HiSeis partially preserved amplitude processing imaging subvertical zones of reduced reflectivity on north-south line 03GA-OD1. A – Wirrda Well; B – Olympic Dam; C – Titan (15 km NNW of section); D – Vulcan.

CONCLUSIONS

To obtain a crustal-scale image of reflection seismic data, certain processing techniques are favoured. This necessarily limits the degree to which certain upper crustal features can be imaged/and or enhanced. However, there is a range of processing techniques available and each can emphasize different aspects of the data. The Partially Preserved Amplitude processing (PPA) technique is interpreted to have detected features that relate to Fe-alteration around the Olympic Dam orebody and has revealed steeper structures than were imaged with previous processing techniques. Several kilometre-scale, sub-vertical 'bland' zones that extend from at least the mid-upper crust to the near-surface in the vicinity of several known IOCG deposits have been identified and these correlate to conductive features in magnetotelluric modelling. Such features may relate to partial melt migration or pervasive hydrothermal alteration.

ACKNOWLEDGMENTS

Steve Hill and Laz Katona provided support for this collaboration between HiSeis and the Geological Survey of South Australia. We acknowledge Geoscience Australia for making the seismic data (L163 Gawler Craton 2D Seismic Survey,2003) available for the public use.

REFERENCES

Brown M 1994. The generation, segregation, ascent and emplacement of granite magma: the migmatite-to-crustally-derived granite connection in thickened orogens. Earth-Science Reviews 36:83–130.

Diener JFA, White RW and Hudson TJM 2014. Melt production, redistribution and accumulation in midcrustal source rocks, with implications for crustal-scale melt transfer. Lithos 200–201:212–225.

Drummond B, Lyons P, Goleby B and Jones L 2006. Constraining models of the tectonic setting of the giant Olympic Dam iron oxide–copper–gold deposit, South Australia, using deep seismic reflection data. Tectonophysics 420:91–103.

Ehrig K, McPhie J and Kamenetsky V 2012. Geology and mineralogical zonation of the Olympic Dam iron oxide Cu-U-Au-Ag deposit, South Australia. In JW Hedenquist, W Harris and F Camus eds, Geology and genesis of major copper deposits and districts of the world: a tribute to Richard H. Sillitoe, Special Publication 16. Society of Economic Geologists, pp. 237–268.

Goleby BR, Lyons P, Drummond BJ, Schwarz M, Shearer AJ, Fairclough MC, Korsch RJ and Skirrow RG 2003. General basement interpretation (18 s data). In P Lyons and BR Goleby eds, The 2003 Gawler Craton Seismic Survey: notes from the Seismic Workshop held at Gawler Craton State of Play 2004, Record 2005/019. Geoscience Australia, Canberra, pp. 48–57.

Hammer PTC, Clowes RM, Cook FA, van der Velden AJ and Vasudevan K 2010. The lithoprobe trans-continental lithospheric cross sections: imaging the internal structure of the North American continent. Canadian Journal of Earth Sciences 47:821–857.

Heinson G, Direen NG and Gill RM 2006. Magnetotelluric evidence for a deep-crustal mineralizing system beneath the Olympic Dam iron oxide copper-gold deposits, southern Australia. Geology 34:573–576.

Jakica S and Pridmore D 2014. Reflection seismic in the search for IOCG deposits on the Stuart Shelf - a multiclient study. HiSeis Pty Ltd, Bentley, Western Australia.

Jones LEA, Johnstone DW and Goleby BR 2005. Seismic acquisition and processing - 2003 Gawler Craton seismic reflection survey (L163). In P Lyons and BR Goleby eds, The 2003 Gawler Craton Seismic Survey: notes from the Seismic Workshop held at Gawler Craton State of Play 2004, Record 2005/019. Geoscience Australia, Canberra, pp. 35–47.

Kennett BLN, Saygin E, Fomin T and Blewett R 2013. Deep crustal seismic reflection profiling: Australia, 1978–2011. ANU E Press and Geoscience Australia, Canberra.

Thiel S and Heinson G 2015. Crustal and mantle resistivity architecture of SA and its relation to mineral systems, presentation. Unlocking South Australia's Mineral Wealth Technical Forum, 15 April 2015. Department of State Development, Adelaide, viewed 20 October 2015, http://www.minerals.statedevelopment.sa.gov.au/knowledge centre/events/sareic technical forum>.

Williams PJ, Barton MD, Fontboté L, De Haller A, Johnson D, Mark G, Marschick R and Oliver NHS 2005. Iron oxide coppergold deposits: geology, space-time distribution, and possible modes of origin. In JW Hedenquist, JFH Thompson, RJ Goldfarb and JP Richards eds, Economic Geology 100th Anniversary Volume. Society of Economic Geologists, Littleton, CO, USA, pp. 371– 405.

Line geometry and crooked line definition (fixed common depth-point interval)SEG-Y inputField SEG-Y to Disco format: resample to 4 m/s and 8 s Quality control display. Selected trace edits and 50 Hz notchSectral equalisation (with 1000 m/s gate automatic gain control)Spectral equalisation (with 1000 m/s gate automatic gain control)Gain recovery (spherical divergence)Gain recovery (spherical divergence)Sufface consistent amplitude recoveryApplication of refraction statics, datum 0 m (AHD)Sufface consistent spiking deconvolution – operator length 80 mApplication of automatic residual statics (autostatics calculated on 0.25–4. 0 s gate)Sufface consistent spiking deconvolution – operator length 80 mTime (s) 0.0-1.5Bandpass (Hz)/slope (db/octave) 0.0-1.5Sufface anticons utions 20036Velocity analysis using VELEX. First pass after refraction statics. Second pass differ autostatics. Third pass after differNoise attenuation Constant velocity stack analysisNormal moveout correction on common offset gathersTime gate picked for residual static calculation Computation of sucre consistent residual reflection statics (delay time based) normal moveout and application of residual staticNO correction on common offset gathersApplication of TX DMO Interactive velocity analysis using VELEX. First pass a frace running mix (weights 1:1:0)Signal enhancements (digistack 0.8) Trace amplitude scalingSector fire and trace mix (3/2) Generation of sesimic attributes – perigram x cosine phase Time/depth conversion using average velocities SEG-Y files to specification	Geoscience Australia	HiSeis P/L
depth-point interval)Geometry assignment and quality control – bin size 20 mField SEG-Y to Disco format: resample to 4 m/s and 8 sGuality control display. Selected trace edits and 50 HzQuality control display. Selected trace edits and 50 HzFirst break picking and refraction static computation: final datum at 120 m; replacement velocity 4500 m/sSpectral equalisation (with 1000 m/s gate automatic gain control)Guality control of the refraction static solution (on shot records, every 20th shot)Common mid-point sort (bin wide open)Spherical divergence:Gain recovery (spherical divergence)Spherical divergence correction: time-power 1.2Application of automatic residual statics (autostatics calculated on 0.25–4.0 s gate)Surface consistent spiking deconvolution – operator length 80 mSurface ave noise attenuation (apparent velocity of 2200 m/s)Surface varve noise attenuation (apparent velocity of 2200 m/s)Band filteredAir-blast attenuationTime (s)Bandpass (Hz)/slope (db/octave)0.0-1.520/36 – 80/362.0-8.010/36 – 80/36Velocity analysis using VELEX. First pass after refraction statics. Third pass after dipmoveout (DMO)Normal moveout correction on common offset gathersStretch mute used as front end muteDMO correction on common offset gathersCommon mid-point stackTrace amplitude balanceF-X migration using 90% of modified velocities3 trace running mix (weights 1:1:0)Signal enhancements (digistack 0.8)Trace amplitude scalingTrace amplitude scalingTrace amplitude scalingPost-stack F-X	Line geometry and crooked line definition (fixed common	n SEG-Y input
Field SEG-Y to Disco format: resample to 4 m/s and 8 sQuality control display. Selected trace edits and 50 HzNotchSpectral equalisation (with 1000 m/s gate automatic gain control)Common mid-point sort (bin wide open)Gain recovery (spherical divergence)Application of refraction statics, datum 0 m (AHD)Application of automatic residual statics (autostatics calculated on 0.25-4.0 s gate)Band filteredTime (s)Bandpass (Hz)/slope (db/octave)0.0-1.520/36 - 80/362.0-8.010/36 - 80/36Velocity analysis using VELEX. First pass after refraction statics. Scom pass after autostatics. Third pass after differedNormal moveout correction on common offset gathersStretch mute used as front end muteDMO correction on common offset gathersCommon mid-point stackTrace amplitude balanceF.X migration using 90% of modified velocities3 trace running mix (weights 1:1:0)Signal enhancements (digistack 0.8)Trace amplitude scalingTrace amplitude scalingCommon mid-point stackTrace amplitude scalingCommon mid-point stackTrace amplitude scalingCommon mid-point stackTrace amplitude scalingCommon mid-point stackStretch mute used as front end muteDMO correction on common offset gathersCommon mid-point stackCommon mid-point stackTrace amplitude scalingCharles as a file end usationSignal enhancements (digistack 0.8)Trace amplitude scaling <td>depth-point interval)</td> <td>Geometry assignment and quality control – bin size 20 m</td>	depth-point interval)	Geometry assignment and quality control – bin size 20 m
Quality control display. Selected trace edits and 50 Hz notch datum at 120 m; replacement velocity 4500 m/s Spectral equalisation (with 1000 m/s gate automatic gain control) Guality control of the refraction static solution (on shot records, every 20th shot) Common mid-point sort (bin wide open) Surface consistent amplitude recovery Gain recovery (spherical divergence) Application of automatic residual statics (autostatics calculated on 0.25–4.0 s gate) Band filtered Surface wave noise attenuation (apparent velocity of 200 m/s) Band filtered Air-blast attenuation Time (s) Bandpass (Hz)/slope (db/octave) 0.0-1.5 20/36 – 80/36 2.0-8.0 10/36 – 80/36 Automatic gain control based trace normalisation 3000 m/s Velocity analysis using VELEX. First pass after refraction statics. Second pass after autostatics. Third pass after dig moveout (DMO) Noise attenuation Normal moveout correction on common offset gathers Computation of surface consistent residual reflection statics (delay time based) normal moveout and application of residual statics Computation using 90% of modified velocities 3 trace running mix (weights 1:1:0) Signal enhancements (digistack 0.8) Trace amplitude scaling Post-stack F.X deconvolution, TV bandpass filter and trace mix (3/2) Generation of seismic attributes – perigram x cosine phase Time/depth conversion using average velocities	Field SEG-Y to Disco format: resample to 4 m/s and 8 s	First break picking and refraction static computation: final datum at 120 m; replacement velocity 4500 m/s
Notify Guality control of the refraction static solution (on shot spectral equalisation (with 1000 m/s gate automatic gain control) Guality control of the refraction static solution (on shot records, every 20th shot) Common mid-point sort (bin wide open) Surface consistent amplitude recovery Gain recovery (spherical divergence) Application of refraction statics, datum 0 m (AHD) Application of automatic residual statics (autostatics calculated on 0.25-4.0 s gate) Surface wave noise attenuation (apparent velocity of 2200 m/s) Band filtered Surface wave noise attenuation Time (s) Bandpass (Hz)/slope (db/octave) 0.0-1.5 20/36 – 80/36 2.0-8.0 10/36 – 80/36 Automatic gain control based trace normalisation 3000 m/s Nerise attenuation Bandpass (Hz)/slope (db/octave) 0.0-1.5 Noise attenuation Normal moveout correction on common offset gathers Time gate picked for residual static calculation Normal moveout correction on common offset gathers Time gate picked for residual statics Common mid-point stack Application of try/bottom mute Trace amplitude balance Application of for /bottom mute F.X migration using 90% of modified velocities Final stack (DMO) Signal enhancements (digistack 0.8) Final stack (DMO) Trace amplitude scaling Post-stack Pase-s	Quality control display. Selected trace edits and 50 Hz	
Operation regreeControlControlControlSurface consistent amplitude recoveryCommon mid-point sort (bin wide open)Surface consistent amplitude recoverySpherical divergence correction: time-power 1.2Application of refraction statics, datum 0 m (AHD)Application of automatic residual statics (autostatics calculated on 0.25-4.0 s gate)Surface wave noise attenuation (apparent velocity of 2200 m/s)Band filteredSurface wave noise attenuation (apparent velocity of 2200 m/s)Surface wave noise attenuation (apparent velocity of 2200 m/s)Non-1.520/36 – 80/36Automatic gain control based trace normalisation 3000 m/sSurface wave noise attenuation Surface wave noise attenuation Surface wave noise attenuationVelocity analysis using VELEX. First pass after refraction statics. Second pass after autostatics. Third pass after dip moveout (DMO)Noise attenuation Computation of surface consistent residual static calculation Computation of surface consistent residual reflection statics (delay time based) normal moveout and application of residual staticsDMO correction on common offset gathersTime gate picked for residual static calculation Computation of surface consistent residual reflection statics (delay time based) normal moveout and application of residual staticsApplication using 90% of modified velocities 3 trace running mix (weights 1:1:0)Post-stack (DMO) Post-stack (DMO)Signal enhancements (digistack 0.8)Final stack (DMO) Post-stack (DMO)Trace amplitude scalingGeneration of seismic attributes – perigram x cosine phase Time/depth conversion using average velocities SEG-Y files to specification <td>noich Spectral equalisation (with 1000 m/s gate automatic gain</td> <td>Quality control of the refraction static solution (on shot records, every 20th shot)</td>	noich Spectral equalisation (with 1000 m/s gate automatic gain	Quality control of the refraction static solution (on shot records, every 20th shot)
Common mid-point sort (bin wide open)Spherical divergence correction: time-power 1.2Gain recovery (spherical divergence)Application of refraction statics, datum 0 m (AHD)Application of automatic residual statics (autostatics calculated on 0.25–4.0 s gate)Spherical divergence correction: time-power 1.2Band filteredSurface wave noise attenuation (apparent velocity of 2200 m/s)Band filteredSurface wave noise attenuation (apparent velocity of 2200 m/s)Time (s)Bandpass (Hz)/slope (db/octave) 0.0–1.50.0–1.520/36 – 80/362.0–8.010/36 – 80/36Velocity analysis using VELEX. First pass after refraction statics. Second pass after autostatics. Third pass after dip moveout (DMO)Normal moveout correction on common offset gathersStretch mute used as front end mute DMO correction on common offset gathersCommon mid-point stackTrace amplitude balance F-X migration using 90% of modified velocities 3 trace running mix (weights 1:1:0)Signal enhancements (digistack 0.8)Trace amplitude scalingPost-stack (DMO)Roman mid-point stackPrace amplitude scalingPost-stack phase-shift time migration 	control)	Surface consistent amplitude recovery
Gain recovery (spherical divergence)Application of refraction stratics, datum 0 m (AHD)Application of automatic residual statics (autostatics calculated on 0.25–4.0 s gate)Application surface consistent spiking deconvolution – operator length 80 mBand filteredSurface wave noise attenuation (apparent velocity of 2200 m/s)Band filteredSurface wave noise attenuationTime (s)Bandpass (Hz)/slope (db/octave) 0.0–1.5 20/36 – 80/362.0–8.010/36 – 80/36Velocity analysis using VELEX. First pass after refraction statics. Second pass after autostatics. Third pass after dip moveout (DMO)Normal moveout correction on common offset gathersStretch mute used as front end mute DMO correction on common offset gathersCommon mid-point stackTrace amplitude balance F-X migration using 90% of modified velocities 3 trace running mix (weights 1:1:0)Signal enhancements (digistack 0.8)Trace amplitude scalingTrace amplitude scalingDiagonal enhancements (digistack 0.8)Trace amplitude scalingCommon mid-point stackTrace amplitude scalingCommon mid-point stackTrace amplitude scalingCommon mid-point stackCommon mid-point stack<	Common mid-point sort (bin wide open)	Spherical divergence correction: time-power 1.2
Application of refraction statics, datum 0 m (AHD)Application of automatic residual statics (autostatics calculated on 0.25–4.0 s gate)Band filteredTime (s)Bandpass (Hz)/slope (db/octave) 0.0–1.50.0–1.520/36 – 80/362.0–8.010/36 – 80/36Velocity analysis using VELEX. First pass after refraction statics. Second pass after autostatics. Third pass after dip moveout (DMO)Normal moveout correction on common offset gathersStretch mute used as front end mute DMO correction on common offset gathersCommon mid-point stack Trace amplitude balance F-X migration using 90% of modified velocities 3 trace running mix (weights 1:1:0) Signal enhancements (digistack 0.8) Trace amplitude scalingStrace amplitude scalingOperator length 80 mSurface wave noise attenuation Surface consistent residual statics (delay time based) normal moveout and application of residual staticsApplication of T-X DMO Interactive velocity analysis on DMO-corrected data Final stack (DMO)Post-stack plase-shift time migration Post-stack plase-shift time migrationProceeding average velocities SEG-Y files to specification	Gain recovery (spherical divergence)	Application surface consistent spiking deconvolution – operator length 80 m
Application of automatic residual statics (autostatics calculated on 0.25-4.0 s gate)Surface wave noise attenuation (apparent velocity of 2200 m/s)Band filteredAir-blast attenuationTime (s) 0.0-1.5 	Application of refraction statics, datum 0 m (AHD)	
Band filteredAir-blast attenuationTime (s)Bandpass (Hz)/slope (db/octave)Bandpass filter (Ormsby, 5–12–80–100 Hz)0.0–1.520/36 – 80/36Automatic gain control based trace normalisation2.0–8.010/36 – 80/36Noise attenuationVelocity analysis using VELEX. First pass after refraction statics. Second pass after autostatics. Third pass after dip moveout (DMO)Noise attenuationNormal moveout correction on common offset gathersTime gate picked for residual static calculationStretch mute used as front end muteComputation of surface consistent residual reflection statics (delay time based) normal moveout and application of residual staticsDMO correction on common offset gathersComputation of tor/bottom muteTrace amplitude balanceApplication of tor/bottom muteF.X migration using 90% of modified velocitiesFinal stack (DMO)Signal enhancements (digistack 0.8)Post-stack phase-shift time migrationTrace amplitude scalingPost-stack phase-shift time migrationPost-stack phase-shift time deptic conversion using average velocitiesSEG-Y files to specification	Application of automatic residual statics (autostatics calculated on 0.25-4.0 s gate)	Surface wave noise attenuation (apparent velocity of 2200 m/s)
Time (s)Bandpass (Hz)/slope (db/octave)Bandpass filter (Ormsby, 5–12–80–100 Hz)0.0–1.520/36 – 80/36Automatic gain control based trace normalisation 3000 m/sVelocity analysis using VELEX. First pass after refraction statics. Second pass after autostatics. Third pass after dip moveout (DMO)Noise attenuation 	Band filtered	Air-blast attenuation
0.0-1.520/36 - 80/362.0-8.010/36 - 80/36Velocity analysis using VELEX. First pass after refraction statics. Second pass after autostatics. Third pass after dip moveout (DMO)Noise attenuation Constant velocity stack analysisNormal moveout correction on common offset gathersTime gate picked for residual static calculation Computation of surface consistent residual reflection statics (delay time based) normal moveout and application of residual staticsDMO correction on common offset gathersComputation of top/bottom mute Application of T-X DMO Interactive velocity analysis on DMO-corrected dataF-X migration using 90% of modified velocities 3 trace running mix (weights 1:1:0) Signal enhancements (digistack 0.8)Post-stack phase-shift time migration Post-stack phase-shift time migration	Time (s) Bandpass (Hz)/slope (db/octave) 0.0–1.5 20/36 – 80/36 2.0–8.0 10/36 – 80/36	Bandpass filter (Ormsby, 5–12–80–100 Hz)
Velocity analysis using VELEX. First pass after refraction statics. Second pass after autostatics. Third pass after dip moveout (DMO)Noise attenuationNormal moveout correction on common offset gathersTime gate picked for residual static calculationStretch mute used as front end muteComputation of surface consistent residual reflection statics (delay time based) normal moveout and application of residual staticsDMO correction on common offset gathersComputation of top/bottom muteDMO correction on common offset gathersApplication of top/bottom muteTrace amplitude balanceApplication of T-X DMOF-X migration using 90% of modified velocitiesInteractive velocity analysis on DMO-corrected data3 trace running mix (weights 1:1:0)Final stack (DMO)Signal enhancements (digistack 0.8)Post-stack phase-shift time migrationTrace amplitude scalingPost-stack F-X deconvolution, TV bandpass filter and trace mix (3/2)Generation of seismic attributes – perigram x cosine phaseTime/depth conversion using average velocities SEG-Y files to specification		Automatic gain control based trace normalisation 3000 m/s
statics. second pass after autostatics. Third pass after automoveout (DMO)Normal moveout correction on common offset gathersStretch mute used as front end muteDMO correction on common offset gathersCommon mid-point stackTrace amplitude balanceF-X migration using 90% of modified velocities3 trace running mix (weights 1:1:0)Signal enhancements (digistack 0.8)Trace amplitude scalingConstant velocity analysis on DMO-corrected dataFinal stack (DMO)Post-stack F-X deconvolution, TV bandpass filter and trace mix (3/2)Generation of seismic attributes – perigram x cosine phase Time/depth conversion using average velocities	Velocity analysis using VELEX. First pass after refraction statics. Second pass after autostatics. Third pass after dip moveout (DMO)	Noise attenuation
Normal moveout correction on common offset gathersTime gate picked for residual static calculationStretch mute used as front end muteComputation of surface consistent residual reflection statics (delay time based) normal moveout and application of residual staticsDMO correction on common offset gathersApplication of top/bottom muteTrace amplitude balanceApplication of T-X DMOF-X migration using 90% of modified velocitiesInteractive velocity analysis on DMO-corrected data3 trace running mix (weights 1:1:0)Final stack (DMO)Signal enhancements (digistack 0.8)Post-stack phase-shift time migrationTrace amplitude scalingPost-stack F-X deconvolution, TV bandpass filter and trace mix (3/2)Generation of seismic attributes – perigram x cosine phase Time/depth conversion using average velocities		Constant velocity stack analysis
Stretch mute used as front end muteComputation of surface consistent residual reflection statics (delay time based) normal moveout and application of residual staticsDMO correction on common offset gathersApplication of top/bottom muteCommon mid-point stackApplication of top/bottom muteTrace amplitude balanceApplication of T-X DMOF-X migration using 90% of modified velocitiesInteractive velocity analysis on DMO-corrected data3 trace running mix (weights 1:1:0)Final stack (DMO)Signal enhancements (digistack 0.8)Post-stack phase-shift time migrationTrace amplitude scalingPost-stack phase-shift time migrationPost-stack phase-shift time migrationPost-stack F-X deconvolution, TV bandpass filter and trace mix (3/2)Generation of seismic attributes – perigram x cosine phase Time/depth conversion using average velocitiesSEG-Y files to specification	Normal moveout correction on common offset gathers	Time gate picked for residual static calculation
DMO correction on common offset gathers(delay time based) normal moveout and application of residual staticsCommon mid-point stackApplication of top/bottom muteTrace amplitude balanceApplication of T-X DMOF-X migration using 90% of modified velocitiesInteractive velocity analysis on DMO-corrected data3 trace running mix (weights 1:1:0)Final stack (DMO)Signal enhancements (digistack 0.8)Post-stack phase-shift time migrationTrace amplitude scalingPost-stack F-X deconvolution, TV bandpass filter and trace mix (3/2)Generation of seismic attributes – perigram x cosine phase Time/depth conversion using average velocities	Stretch mute used as front end mute	Computation of surface consistent residual reflection statics (delay time based) normal moveout and application of residual statics
Common mid-point stackApplication of top/bottom muteTrace amplitude balanceApplication of T-X DMOF-X migration using 90% of modified velocitiesInteractive velocity analysis on DMO-corrected data3 trace running mix (weights 1:1:0)Final stack (DMO)Signal enhancements (digistack 0.8)Post-stack phase-shift time migrationTrace amplitude scalingPost-stack F-X deconvolution, TV bandpass filter and trace mix (3/2)Generation of seismic attributes – perigram x cosine phaseTime/depth conversion using average velocities SEG-Y files to specification	DMO correction on common offset gathers	
Trace amplitude balanceApplication of T-X DMOF-X migration using 90% of modified velocitiesInteractive velocity analysis on DMO-corrected data3 trace running mix (weights 1:1:0)Final stack (DMO)Signal enhancements (digistack 0.8)Post-stack phase-shift time migrationTrace amplitude scalingPost-stack F-X deconvolution, TV bandpass filter and trace mix (3/2)Generation of seismic attributes – perigram x cosine phase Time/depth conversion using average velocitiesSEG-Y files to specification	Common mid-point stack	Application of top/bottom mute
F-X migration using 90% of modified velocities 3 trace running mix (weights 1:1:0) Signal enhancements (digistack 0.8) Trace amplitude scaling Post-stack phase-shift time migration Post-stack F-X deconvolution, TV bandpass filter and trace mix (3/2) Generation of seismic attributes – perigram x cosine phase Time/depth conversion using average velocities SEG-Y files to specification	Trace amplitude balance	Application of T-X DMO
3 trace running mix (weights 1:1:0) Signal enhancements (digistack 0.8) Trace amplitude scaling Final stack (DMO) Post-stack phase-shift time migration Post-stack F-X deconvolution, TV bandpass filter and trace mix (3/2) Generation of seismic attributes – perigram x cosine phase Time/depth conversion using average velocities SEG-Y files to specification	F-X migration using 90% of modified velocities	Interactive velocity analysis on DMO-corrected data
Signal enhancements (digistack 0.8) Post-stack phase-shift time migration Trace amplitude scaling Post-stack F-X deconvolution, TV bandpass filter and trace mix (3/2) Generation of seismic attributes – perigram x cosine phase Time/depth conversion using average velocities SEG-Y files to specification SEG-Y files to specification	3 trace running mix (weights 1:1:0)	Final stack (DMO)
Trace amplitude scaling Post-stack F-X deconvolution, TV bandpass filter and trace mix (3/2) Generation of seismic attributes – perigram x cosine phase Time/depth conversion using average velocities SEG-Y files to specification	Signal enhancements (digistack 0.8)	Post-stack phase-shift time migration
Generation of seismic attributes – perigram x cosine phase Time/depth conversion using average velocities SEG-Y files to specification	Trace amplitude scaling	Post-stack F-X deconvolution, TV bandpass filter and trace mix (3/2)
Time/depth conversion using average velocities SEG-Y files to specification		Generation of seismic attributes – perigram x cosine phase
SEG-Y files to specification		Time/depth conversion using average velocities
		SEG-Y files to specification

Table 1; Processing work flows used by Geoscience Australia and HiSeis