

A VLA* Survey of Rich Clusters of Galaxies†

III. The Weaker Sources: Maps and Identifications

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Abstract

We present radio and optical parameters for 737 weak sources in 60 Abell cluster fields observed with the Very Large Array (VLA) using scaled arrays at 1.5 and 4.9 GHz. The measurements extend to a lower 1.5 GHz limit of 1.0 mJy and comprise a complete sample with $1.5 \text{ GHz flux density } 2.5 \leq S_{1.5} < 20 \text{ mJy}$. The combined sky area within the half-power circle on the maps is $3.5 \times 10^{-3} \text{ sr}$, and the cluster fields are distributed over 24 h of right ascension and between declinations $+35^\circ$ and -30° . Contour maps of the extended sources at 1.5 GHz are presented and source parameters such as position, angular size and spectral index are tabulated. We also derive the emitted power and linear size for those sources with published redshifts. We try to identify the radio sources with optical images on the Palomar and SERC survey plates and give their accurate optical positions, morphologies and apparent magnitudes.

1. Introduction

From 1982 to 1985 Slee *et al.* (1989; hereafter SPS89, Paper I) used scaled arrays at the VLA to survey 60 fields near rich clusters of galaxies. The survey fields were centred on the steep-spectrum sources with spectral index $\alpha \leq -0.90$ (defined by $S \propto \nu^\alpha$) discovered in earlier low-resolution surveys by Slee and Siegman (1983) and Slee *et al.* (1983). Fifty-two of the fields were surveyed with scaled arrays at 1.5 and 4.9 GHz (with the C- and D-arrays respectively), using identical phase and delay centres at the two frequencies. Five fields (A13, A85-2, A2354, A2399 and A2575) were mapped only with the C-array at 1.5 GHz. The remaining three fields (A1791, A2029 and A3528) were mapped with the scaled B- and C-arrays, resulting in a threefold improvement in angular resolution. The half-power-beam width (HPBW) in the C- and D-arrays was ~ 14 arcsec in right ascension but was up to a factor of two larger in declination at the southern declination limit of -30° .

The VLA observations, data reduction, whole-field maps and general source statistics were described in Paper I. The results (maps, polarisation and identifications) for the stronger sources are given in Slee *et al.* (1994; hereafter

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SRS94, Paper II). This paper, the third of the series, provides similar radio and optical parameters for the weaker sources with 1.5-GHz flux densities $1 < S_{1.5} < 20$ mJy.

The only other major survey of Abell clusters with similar angular resolution is that described in the three publications of Zhao *et al.* (1989) and Owen *et al.* (1992, 1993), who made their observations only at 1.5 GHz. Their published maps and measurements were confined to the strongest sources near the cluster centres and only a few clusters are common to both surveys. Therefore, it is more appropriate to compare their results with those on the stronger sources in our Paper II; this will be done in a future publication.

The weak-source measurements are presented in Section 2, including contour maps of the more resolved sources. The optical identifications for these sources are discussed in Section 3 and a conclusion is given in Section 4.

Throughout this paper computations of emitted power and linear source dimensions make use of $H_0 = 75 \text{ km s}^{-1} \text{ Mpc}^{-1}$ and $q_0 = 0.5$.

2. Results

The observations and reductions have been adequately treated in SPS89 (Paper I). The data and maps presented here come from processing further the results in Paper I and are similar to the detailed source parameters given in Paper II. The results presented here include:

- (i) elliptical Gaussian brightness distributions fitted to the sources;
- (ii) contour mapping for well-resolved sources;
- (iii) determination of spectral indices;
- (iv) computation of power output and linear size for sources with redshifts.
- (v) optical identifications.

In contrast to the stronger sources in Paper II, we have no polarisation data for this sample, nor do we have any high-resolution interferometer measurements of their core components. Table 1 provides a list of the cluster fields that we observed. The more useful optical and X-ray parameters of the clusters are listed, and the positions of the VLA field centres with respect to the cluster centres are given. The rms fluctuation level over a large, relatively clear area of each VLA map is shown in columns 7 and 8; a blank in either of these columns means that no map is available at that frequency. The column headings are explained in a footnote to the table. The values of L_x followed by 'R' in column 17 are ROSAT logarithmic luminosities (Ebeling 1993) that have been transformed to the EINSTEIN luminosity scale. This was done by finding the average difference between EINSTEIN and ROSAT logarithmic luminosities for the 11 clusters in Table 1 that were observed by both telescopes. The average difference $\text{ROSAT} - \text{EINSTEIN} = +0.45$ in $\log L_x$ was then subtracted from the ROSAT logarithmic luminosities for those clusters with no EINSTEIN observations. This gives a more complete, self-consistent set of X-ray luminosities for subsequent analysis.

The optical angular radius of the cluster R_c is not the Abell radius that is usually quoted in cluster publications, but is the value obtained from galaxy counts on the PSS plate by Struble and Rood (1987). The Abell radius assumes that all clusters have a linear radius of 2 Mpc ($H_0 = 75 \text{ km s}^{-1}$, $q_0 = 0.5$), but

we prefer to preserve the differences between clusters by using their measured angular radii. For comparison with the Abell radius, the mean linear radius derived from R_c in Table 1 is 1.79 Mpc with a standard deviation of 0.64 Mpc.

(2a) Radio Parameters of the Sample

Table 2 contains the basic radio measurements of the detected sources, excluding the radio positions, which are given in Table 5. Sources in this paper include:

- (i) all sources listed in Paper I with $S_{1.5} < 20$ mJy. A few of them (e.g. Abell 13_6a/b/c) were also in Paper II because of a special interest in them;
- (ii) a number of sources with $S_{1.5} > 20$ mJy that had been accidentally omitted from Paper II;
- (iii) a significant number of sources with $S_{1.5} > 20$ mJy (usually located near the field edges), which had been deliberately omitted from Paper II.

We omitted a few of the weak sources listed in Paper I because subsequent analysis showed that they were probably spurious. To avoid later confusion, the additional sources are inserted in the Table at the correct right ascension but are given an extra lower case Roman numeral. For example, the source A13_13 in Table 2 of Paper I is now A13_13i, while an added source of slightly later RA, called A13_13ii, has been inserted in Table 2 of this paper. The column headings are explained in a footnote to the table.

On the basis of the statistical analysis of Paper I, only a few of the present sources are expected to be cluster members, i.e. for cluster membership, the integrated 1.5-GHz flux density should be ≥ 20 mJy and $R/R_c \leq 0.28$ (see explanation of R_c in Section 1). Many sources are close to the cluster centres in angular spacing, but only those that can be optically identified with galaxies with published redshifts, agreeing with the cluster redshifts, can be accepted as cluster members. Accordingly, there are few computations of emitted power and linear size in Table 2.

The angular size parameters in columns 8, 9 & 10 of Table 2 were found by fitting a single Gaussian ellipse to the 1.5-GHz brightness distribution, making allowance in the deconvolution for the beam width and bandwidth smearing. A base level was subtracted during the fitting procedure. In most cases the fitted position (given in Table 5) is close to that of the centroid of the distribution, but in some well-resolved doubles this position is that of the peak of the dominant component. In these cases we have omitted the angular diameter but retained the position as a reference point for the optical identifications in Table 5. The deconvolution of the fitted ellipse for the beam shape and bandwidth smearing did not converge for many of the weaker sources. In these sources (indicated by blanks in the Gaussian-fitted parameters in Table 2), the fitting errors can be so large that the parameters of the derived ellipse may not be consistent with the beam shape and smearing magnitude. The integrated flux densities given in columns 5 & 6 in Table 2 were not obtained from the Gaussian fitting but from the AIPS task IMEAN, which sums the pixel amplitudes in a small box placed around the source image. This method ensures a more accurate result when the source shape departs markedly from an elliptical Gaussian.

The spectral index in column 7 of Table 2 was preferentially computed from our 1.5- and 4.9-GHz measurements of flux density with scaled arrays. If we did not have a 4.9-GHz flux density (because of the smaller primary beam), we combined our 1.5-GHz flux density with other measurements from the references in column 11.

The tabulations of 1.5-GHz spectral power density and linear size in columns 12 and 13, use the few published redshifts of the brighter galaxy identifications. Most of these redshift references are identified in the NASA/IPAC Extragalactic Database* (NED) or the compilation of Andernach *et al.* (1995), but a few more redshifts were obtained from an independent scan of the literature.

(2b) Components of Double Sources

The detailed parameters of the doubles included in Table 2 are set out in Table 3. The column headings are explained in a footnote to the table. Component 'a' of a double is that with the higher 1.5-GHz flux density. Our angular resolution (~ 14 arcsec FWHP) is too low to refine the morphological classification. As for the fitting of the single ellipses described in Section 2a, the Gaussian fits to the components often had errors large enough to prevent the convergence of the deconvolution for beam shape and bandwidth smearing.

Unlike the stronger sources in Paper II, far fewer of the sources identified with optical galaxies (see Table 5) are double sources; only 18 of the 174 galaxy identifications (10%) have definite double structure. For the star-like identifications, 9 out of a total of 61 (15%) are doubles. The larger fraction of doubles 35/62 (56%) remains unidentified. A plausible explanation of this difference is that the weaker sources in this sample are correspondingly more distant so that the angular scale of their lobe structure cannot now be resolved. Alternatively, these are intrinsically weak radio sources and may have correspondingly small linear dimensions (see the radio power—linear size relationship for the stronger sources shown in Paper I).

(2c) Components of Triple and Quadruple Sources

Table 4 gives the parameters of the 6 triple and quadruple sources; one of these (Abell 1631-a/b/c/d) has a total flux density $S_{1.5} = 32.7$ mJy and was accidentally omitted from Paper II. Only two of the six sources can be identified with galaxies (see Table 5). Neither galaxy has a published redshift, so we are unable to derive an emitted power or linear size.

(2d) Contour Maps

The contour maps in Fig. 1 (see p. 1030) have been assigned numbers, which also appear in Tables 2, 3 and 4 for the relevant sources. The maps have been corrected for primary beam attenuation but not for image distortion caused by bandwidth smearing in the outer regions of the radio fields. The map numbers

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* The NASA/IPAC Extragalactic Database is operated by the Jet Propulsion Laboratory, California Institute of Technology, under contract with the National Aeronautics and Space Administration.

Table 1. Properties of the observed clusters

Cluster Field	RA h m (1)	Dec ° (2)	Radio Offset R/Rc (4)	Pos. Ang. ° (5)	Map rms-uJy/beam 1.5 GHz (6)	Map rms-uJy/beam 4.9 GHz (7)	Rich. Class (8)	Dist. Class (9)	m10 (10)	BM Class (11)	R _{c†} Mpc (12)	Redshift z (13)	Ref. z (14)	Log L _x (erg/s) Einstein (15)	Log L _x (erg/s) Rosat (16)	
A 13	00 11.1	-19 47	2.5	0.15	-81.1	58	2	5	16.6	III	17	1.59	0.0945	6	43.97 R 44.42	
A 76	00 37.2	06 30	31.8	0.93	16.3	105	42	0	15.0	II-III	34	1.53	0.0416	1		
A 85-1	00 39.1	-09 37	30.6	0.90	-157.3	97	44	1	15.7	I	34	2.00	0.0556	1		
A 85-2	" "	2.1	0.06	-127.1	30	"	"	"	"	"	"	"	"	"	44.60 45.07	
A 86	00 40.2	-22 04	11.4	0.46	-145.2	71	47	0	4	15.9	II-III	25	1.64	0.0627	1	42.92
A 115	00 53.3	26 03	5.6	0.37	-21.3	288	43	3	6	17.3	III	15	2.51	0.1971	1	44.51
A 133	01 00.3	-22 09	1.2	0.04	-64.1	78	33	1	5	15.9	I	27	1.61	0.0566	1	44.11
A 154+1	01 08.3	17 24	27.0	0.48	65.5	100	45	1	3	15.6	II	56	3.73	0.0638	1	
A 154+2	" "	18.6	0.33	43.9	198	64	"	"	"	"	"	"	"	"		
A 196	01 24.5	22 57	1.5	0.11	-37.1	159	41	1	6	17.5	III	14	1.97	0.156	2	
A 240	01 39.3	07 22	15.7	0.60	-64.3	68	38	0	3	15.6	II-III	26	1.68	0.0618	1	
A 278	01 54.4	31 59	1.2	0.04	149.2	130	33	0	3	15.6	III	27	2.42	0.0894	8	43.66
A 357	02 26.7	13 01	8.0	0.30	-117.3	145	41	0	5	16.8	"	27	2.88	0.110	2	
A 362	02 29.1	-05 05	1.8	0.16	145.8	79	36	1	6	17.7	II-III	11	1.66	0.172	2	
A 407	02 58.6	35 38	2.0	0.06	85.3	141	42	0	2	14.7	II	34	1.69	0.0463	1	43.34 43.67
A 416	03 04.9	-16 54	3.7	0.37	56.6	93	60	0	6	17.7	I-II	10	1.51	0.172	2	
A 474 *	04 09.6	-16 49	58.7	6.52	-87.4	117	37	0	5	17.1	II	9	1.08	0.128	2	
A 496	04 31.3	-13 21	0.4	0.09	141.0	166	42	1	3	15.3	I	45	1.62	0.0327	1	44.16 44.55
A 514	04 45.7	-20 31	11.0	0.32	126.3	110	33	1	4	15.2	II-III	34	2.54	0.0728	7	
A 519	04 51.2	00 36	1.1	0.05	119.5	75	33	0	5	17.0	"	23	2.67	0.122	2	
A 531	04 58.8	-03 37	1.8	0.10	45.3	60	41	1	5	17.0	III	18	2.09	0.122	2	
A 658	08 21.0	15 50	6.8	0.49	150.4	78	30	1	5	17.0	III	14	1.62	0.122	2	
A 912	09 58.6	00 08	10.4	0.42	6.9	292	38	0	4	15.9	"	25	1.81	0.070	2	
A 1142	10 58.3	10 49	20.5	0.60	100.5	177	53	0	3	15.4	II-III	34	1.31	0.0353	1	
A 1171	11 04.9	03 13	11.6	0.41	-146	86	36	0	4	16.2	"	28	2.13	0.0741	1	
A 1189	11 08.5	01 24	1.1	0.04	0.0	135	45	0	5	17.0	"	25	2.90	0.122	2	
A 1238	11 20.4	01 22	1.6	0.11	-38.7	102	37	1	4	16.0	III	15	1.14	0.074	2	
A 1273	11 26.8	-06 46	1.8	0.16	-105.5	195	54	1	6	17.6	III	11	1.61	0.164	2	
A 1620	12 47.2	-01 19	4.7	0.21	65.2	128	43	0	5	17.2	III	22	2.75	0.134	2	

A 1631	12	50.2	-15	10	5.9	0.21	7.1	54	29	0	3	15.4	1	28	1.40	0.0465	1	43.28	43.84
A 3528#	12	51.6	-28	45	13.4	0.36	156.1	53	1	4	16.3	II	37	2.00	0.0506	3			
A 1689	13	09.0	-01	06	2.0	0.18	-61.5	67	33	4	6	17.6	II-III:	11	1.74	0.1832	1	44.98	45.47
A 1772	13	39.4	-10	50	1.9	0.15	156.6	59	35	1	5	17.0	II-III	13	1.51	0.122	2		
A 1775	13	39.6	26	37	1.2	0.04	-47.6	55	35	2	4	15.7	I	28	2.07	0.0717	1	44.01	44.48
A 1791	13	46.0	-25	12	1.7	0.06	100.3	111	38	1	6	17.0	I	26	3.01	0.122	2		
A 1913	14	24.5	16	54	3.6	0.16	46.8	56	40	1	4	16.0	III	22	1.23	0.0528	1	43.39	
A 2009	14	58.0	21	34	1.3	0.12	53.8	29	29	1	5	17.2	I-II:	11	1.52	0.1530	1	44.63	45.09
A 2029	15	08.5	05	57	1.5	0.07	-152.8	190	32	2	4	16.0	I	22	1.73	0.0768	1	44.85	45.31
A 2052	15	14.3	07	11	1.6	0.07	9.0	764	260	0	3	15.0	I-II	22	0.84	0.0348	1	43.95	44.39
Zw1518.80	15	18.8	07	47	10.1	0.24	59.5	29	31	4	2	15.2	II	42	2.00	0.0440	5	44.02	
A 2082	15	28.2	03	37	12.4	0.48	51.8	79	39	0	5	17.0		26	3.01	0.122	2		
A 2091	15	31.9	10	24	2.9	0.32	9.8	38	58	1	6	17.5	III	9	1.27	0.156	2		
A 2094	15	34.0	-01	52	2.2	0.20	34.0	58	42	1	5	16.7	III	11	1.13	0.105	2		
A 2103	15	37.3	-02	00	12.6	0.48	-96.5	93	44	0	5	17.1		26	3.13	0.128	2		
A 2108	15	37.8	18	03	17.3	1.08	57.0	68	39	0	4	15.7	III	16	1.47	0.0919	1		
A 2151	16	03.0	17	53	35.6	1.27	42.9	92	37	2	1	13.8	III	28	1.12	0.0368	1		
A 2249	17	07.9	34	31	2.4	0.09	160.0	71	38	0	3	15.4	III	26	2.13	0.0809	1	44.21 R	44.66
A 2354	21	33.1	-15	08	2.1	0.19	-110.4	54	2	5	17.1	III	11	1.33	0.128	2			
A 2396	21	53.2	12	15	2.7	0.30	26.5	110	136	1	6	17.5		9	1.27	0.156	2		
A 2399	21	54.9	-08	02	31.3	1.20	-161.1	99	1	3	15.6	III	26	1.62	0.0594	7			
A 2443	22	23.7	17	05	1.5	0.13	-14.0	83	47	2	5	16.5	II	12	1.13	0.095	2	43.96 R	44.41
A 2456	22	32.4	-15	33	1.1	0.14	166.9	54	52	1	5	17.2	I	8	1.00	0.134	2		
A 2457	22	33.2	01	13	11.8	0.45	139.0	56	48	1	4	16.0	I-II:	25	1.51	0.0573	1	43.76	44.30
A 2575	23	17.1	-22	19	2.1	0.30	129.1	166	0	6	17.9	III	7	1.14	0.190	2			
A 2593	23	22.0	14	22	0.5	0.02	78.3	70	98	0	3	15.1	II	28	1.27	0.0421	1	43.63	44.02
A 2622	23	32.4	27	09	3.4	0.17	138.5	100	56	0	4	15.9	II-III:	20	1.45	0.070	2	43.56 R	44.01
A 2626	23	34.0	20	53	1.0	0.04	167.7	74	25	0	3	15.2	I-II	25					
A 2657	23	42.3	08	52	27.3	1.05	125.4	68	70	1	3	14.9	III	26	1.17	0.0414	1		
A 4038#	23	45.1	-28	25	0.5	0.01	-2.5	68	43	2	2	14.2	II	64	2.00	0.0283	4		
A 2670	23	51.6	-10	41	20.0	0.91	-128.1	78	60	3	4	15.7	I-II	22	1.71	0.0761	1		

* The RA is from Abell et al. (1989) . The incorrect RA of Abell (1958) was used for the radio field centre - hence the large offset.

† Rc is the cluster radius from the Palomar Sky Survey (Struble & Rood, 1987) except that the Abell radius (approximately 1.72 π arcmin) is quoted for A 3528, Zw 1518.8 & A 4038.

Data from Abell et al. (1989)

◊ Data from Zwicky et al. (1961) & Slee & Quinn (1979)

R ROSAT measurement converted to the Einstein luminosity scale (see text Section 2).

Column headings :

Redshift references :

1. Struble & Rood (1991)
 2. From the m10 - z relationship in SRS94 (Paper II)
 3. Melnick & Quintana (1981)
 4. Abell et al. (1989)
 5. Beers et al. (1991)
 6. Shee & Reynolds (1984)
 7. Reynolds (1986)
 8. Postman et al. (1992)
- Column 1. The cluster of galaxies nearest the observed radio field.
- Columns 2,3. The centroid position (B,1950) of the optical cluster, mainly from Abell (1958), but data for for three clusters come from Abell et al. (1989) & Zwicky et al. (1961).
- Columns 4,5,6. The angular distance & position angle (positive from north through east) of the centre of the radio field with respect to the optical centroid in columns 2 & 3.
- Columns 7,8. The rms levels over a large clear area of the maps at 1.5- and 4.9 GHz.
- Columns 9,10. The richness and distance class of the cluster, mainly from Abell (1958), but for three clusters we obtain the data from Abell et al. (1989) or Shee & Quinn (1979).
- Column 11. The magnitude of the tenth brightest galaxy in the cluster, mainly from Abell (1958), but in three cases cases from Abell et al. (1989) or Zwicky et al. (1961).
- Column 12. The Bautz-Morgan classification of the cluster, mainly from Abell et al. (1989), but for Zw1518.8 from Shee & Quinn (1979).
- Column 13. The angular radius of the cluster as quoted by Struble & Rood (1987).
- Column 14. The linear radius of the cluster
- Columns 15,16. The mean redshift of the cluster and a corresponding reference.
- Column 17. The EINSTEIN X-ray luminosity in the energy range 0.5-4.5 keV and out to a radius of 1 Mpc from the cluster centre. The data (adjusted for $H_0 = 75 \text{ km/s/Mpc}$) are from Jones & Forman (1995).
- Column 18. The ROSAT X-ray luminosity from Ebeling (1993).

Table 2. Radio source measurements

Cluster Field	Source Number	Map Number	Ang. Dist. R/Rc	1.5-GHz Flux Dens. mJy	4.9-GHz Flux Dens. mJy	Spect. Index	Gaussian Axes	Other Radio References	Log 1.5- GHz Power W/Hz	Largest Lin. Size kpc	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	Maj. "	Min. "	PA °	(12)	(13)
A13	2i		1.29	7.0							
	2ii		1.44	22.2							
	3		1.08	1.9							
	4		0.59	3.4							
	5		0.54	1.6							
	6a/b/c	1	0.19	3.9		-2.1	53	20	99	6,9,11	
	8		0.36	1.4							
	9i		0.07	1.0							
	9ii		0.30	1.1							
	10		0.68	1.0							
	11		1.09	16.7							
	12		1.00	7.8			17	6	203		
	13i		1.11	18.5			14	5	118		
	13ii/a/b	2†	0.94	9.2							
	14		0.96	8.1							
A76	2	3†	0.78	2.9			21	10	67		
	3		0.80	3.4							
	4		0.67	4.8							
	6i		1.16	8.5			14	7	48		
	6ii		0.82		3.0						
	7		0.99	1.3							
	9		0.81	7.5			3	3	73		
	10		0.99	0.6							
	11		1.20	2.4							
	12		0.97	2.1	0.4	-1.5	18	9	77		
	14		1.11	2.2			14	7	40		
	15		1.13	8.1	4.2	-0.6					
	16	4†	1.31	3.9			20	7	5		
	18		1.18	3.3			12	5	68		
	19		0.84	123		+0.3				3,6,7,20	
A85	2i		1.33	8.9			14	6	49		
	2ii		1.09	3.1							
	4		1.24	9.7			16	7	133		
	5		0.51	6.4							
	6		0.75	2.9							
	8		0.98	3.6	1.6	-0.7	8	4	13		
	9a/b	5†	0.41	1.7			30	4	120		
	10		0.47	8.7			10	5	48		
	11		0.45	3.4							
	14		0.61	3.6		-3.0				8	
	15		1.10	3.2							
	16		0.77		1.7						
	17		0.74	7.3			13	6	4		
	18		0.88	17.1	4.0	-1.2	5	2	150		
	19		0.32	8.7		-0.6	4	1	119	8	
	20i		0.43	0.7							
	20ii		0.30	1.9							
	21i		0.13	0.5							
	21ii/a/b	6†	0.33	1.1							
	22a/b/c	7†	0.46	5.3			23	2	6		
	23i		1.06	4.4							
	23ii		0.19	0.5							
	24		0.25	0.6							
	25a/b/c	8	0.08	7.8		-2.4	97	16	143	6,8,9,10,11	
	26i		0.17	6.6			8	2	133		22.39
	26ii		0.60	1.8							17
	27		0.21	1.4							
	28		0.55	11.0		-0.2	7	4	122	8	
	29		1.01	5.6		-1.3				8	

Table 2. (Continued)

30i		0.54	1.4						
30ii		0.02	0.5						
31		0.05	1.6		6	3	169		
32i		0.21	2.2						
32ii		0.29	1.1						
33i		0.36	0.6						
34i		0.07	6.7		8	4	127		
34ii		0.47	1.3						
37		0.16	2.5						
38i		0.27	1.3						21.82
38ii/a/b	9†	1.30	23.4		24	7	137		
39		0.49	3.2						
40		0.19	2.5						
41		0.56	5.5						
42i		0.17	1.0						
42ii/a/b/c	10†	0.17	3.5		83	17	85		
43		0.27	1.6						
44		0.57	4.1						
47i		0.32	0.7						
47ii		0.28	0.8						
47iii		0.38	0.8						
48i		0.44	1.1						
48ii		0.43	3.3	-2.6				8	
49		0.32	1.0						
50		0.31	1.7						
51ii		0.44	1.3						
52		0.59	6.4						
53i		0.39	1.1	-3.8	5	3	48	8	
53ii		0.58	1.4						
54i		0.44	1.1						
55		0.54	4.1						
56i		0.41	1.6						
56ii		0.49	1.4						
57		0.47	2.8						
A86	1	0.86	11.0						
	2	0.64	2.7						
	3	0.59	2.0						
	4i	0.48	1.3						
	4ii	0.24	2.6		9	6	138		
	6	0.59	2.0		19	4	3		
	7	0.16	3.2						
	8	0.78	16.5	-1.1				8	
	9	0.48	2.0						
	10	0.24	3.6	-1.8				8	
	11i	0.59	3.3						
	11ii	0.23	2.2		14	6	7		
	13i	0.32	1.7						
	13ii	0.22	3.5			16	5	179	
	14	0.88	13.6	-1.3				8	
A115	1ia/b	11	0.73	3.9		40	21	80	
	1ii		1.30	14.8					
	3a/b	12	0.71	4.9					
	4		0.15	5.4					
	6		0.37	1.4					22.99
	7		0.41	12.1		11	4	109	23.89
	8		0.64	6.3					77
	9a/b	13†	0.51	11.3		23	10	90	
A133	1		0.65	9.6					
	3		0.24	7.2	-1.2				8
	4		0.25	1.5		5	4	114	
	5		0.15	2.2		3	1	114	
	6		0.17	3.8	1.8	-0.6	4	3	60
	9		0.81	5.8				11	22.36
	11		0.79	6.7	-0.9				10
	12		0.61	3.1	-2.6				
	13i		0.50	14.0	-1.0				
	13ii		0.59	5.8	-0.9				

Table 2. (*Continued*)

14		0.35	8.8	-0.8				8
15	14†	0.48	3.0		34	16	143	
16	14†	0.52	3.9		32	9	58	
17		0.63	5.2					
A154	1	0.13	4.4		14	2	60	
	3	0.31	2.2					
	5i	0.23	4.1					
	5ii	0.25	4.1		16	4	53	
	6i	0.40	2.0					
	6ii	0.28	3.5					
	7i	0.43	1.8					
	7ii	15†	0.57	4.6		18	6	145
	7iv	0.39	1.2					
	8	0.44	2.8					
	9	0.52	5.4					
	10	0.42	5.0	2.0	-0.8			
	13	0.61	3.0					
A196	1ii	1.06	8.5					
	5i	0.74	3.2					
	5ii	0.96	6.7					
	6	0.48	3.3					
A240	1	1.07	14.4					
	3	0.88	4.5					
	4	0.90	3.0					
	5	0.82	4.2					
	7	16†	1.06	5.9		22	6	36
	10		0.60	6.9		9	3	162
	11		0.80	3.2				
	12		0.50	1.9				
	13a/b	17	0.47	11.6	3.5	-1.0		
	14		0.43	14.7	3.7	-1.2	10	3
	15a/b	18†	0.75	14.6			29	7
	16	19†	0.13	13.8			20	16
	18	20†	0.15	7.1			21	13
							41	4,5
A278	1	0.58	8.7					
	2	21†	0.36	22.8		29	18	7
	3		0.23	4.4				
	7		0.05	13.6	2.6	-1.4	11	6
	9	22†	0.72	20.5			22	13
	11		0.37	8.7			29	
A357	1	0.70	4.4					
	2	0.69	3.1					
	3	0.58	6.9					
	4	0.60	4.9					
	6	0.30	5.9		18	3	57	
	7	0.27	9.2					
A362	1	1.03	4.3		11	6	81	
	3	1.01	2.4					
	4	0.46	1.0					
	5	1.01	2.0					
	7	0.01	2.8					
	9	0.64	5.3	0.8	-1.6			
	11	0.40	1.1					
	12	0.69	1.2		13	3	160	
	13i	0.58	1.4					
	13ii	1.70	120.0	-0.5	14	7	22	20
	13iii	1.97	13.8		19	3	137	
	15	1.60	5.2		15	9	3	
	16a/b	23†	1.33	10.1				
A407	1	24†	0.50	13.4		31	3	58
	2		0.47	18.3		17	4	115
	5		0.34	11.8				16

Table 2. (Continued)

Table 2. (Continued)

6		0.71	4.5		13	4	104	
7i		0.71	6.8					
7ii	32†	0.85	13.5					
7iiia/b	32†	0.83	9.2		38	6	5	
9		0.21	1.9		9	4	159	
10		0.34	8.9	1.8	-1.4	8	3	131
11		0.44	2.5					
12		0.56	2.3					
A531	2	0.66	14.2		10	7	84	
3		0.38	1.3					
4		0.65	9.8		8	4	132	
5		0.18	3.8		8	3	166	
6		0.35	1.1					
8		0.46	2.1					
9		0.05	16.3	0.4	-3.1	14	11	37
10		0.85	2.6					
12		0.34	6.3					
13	33	0.40	2.6		21	14	153	
14		0.38	3.6	1.9	-0.5	5	2	122
15		0.26	6.7	1.9	-1.1			
16		0.53	9.4					
17		0.50	2.2		7	2	136	
19		0.43	6.3		10	5	143	
20		0.69	11.3					
A658	1	1.51	7.6					
4		1.11	8.0		11	4	41	
5		0.87	13.6					
7		0.69	7.3					
8a/b	34†	0.20	3.9		46	34	66	
9		0.12	3.5					
12		0.58	1.3					
13		1.12	0.9					
14	35†	1.81	6.8		84	28	156	
15		1.54	2.5					
17		0.98	3.5					
18		1.88	12.7					
19/20		1.23	10.1		10	1	118	
21		1.56	4.7					
22	36†	1.43	11.2		30	2	55	
A912	2i	37†	0.77	12.9		26	16	137
3		0.41		1.0				
5i		0.46		1.2				
5ii	38†	0.89	12.6					
6		0.54		1.1				
8a/b	39†	0.70	25.3					
9	40†	0.92	14.3					
A1142	1		0.34	10.6				
2		0.73	13.9					
3/4		0.63	3.1	2.2	-0.3			
5i		0.63	4.1					
5ii		0.58	2.9					
7		0.74	4.0					
8		0.76	4.1					
9		0.78	3.4					
10		0.81	3.6					
11		0.80	2.6		18	3	85	
13		0.95	5.9					
14		0.91	7.0					
15		0.94	5.3					
16a/b	41†	1.01	8.1		21	5	101	
A1171	1		0.59	3.1				
3		0.55	2.7					
5		0.55	1.5					
7	42	0.48	1.5		20	17	112	
8a/b	43†	0.74	4.6		58	8	26	

Table 2. (*Continued*)

9		0.42	1.2	0.3	-1.2				
10i		0.61	1.2			12	6	120	
10ii		0.40	1.8			15	10	96	
12/13		0.29	0.7	0.8	+0.1				
14		0.15	2.2						
15		0.17	2.0						
17		0.93	2.9						
18		0.44	3.9						
19		0.08	4.2						
20		0.08	2.1						
23		0.32	12.5						
24		0.79	9.2						
A1189	2ii	0.40	3.6						
	2iii	0.28	2.1						
	3	0.11	5.4	2.6	-0.6				
	4	0.16	12.3	4.5	-0.9	8	5	156	
	7	0.18	2.4			10	4	76	
	8	0.33	2.8						
9a/b	44	0.26	5.5						
11		0.55	3.3						
12i		0.29	16.6						
12ii		0.58	3.8						
13iii		0.68	4.6						
A1238	1	1.21	9.6						
3	45†	0.82	2.0			30	20	131	
4		0.52	2.2						
5a/b	46†	0.84	2.6						
6		1.39	7.7						
7		0.44	12.9	5.9	-0.7				
8a/b	47	0.36	1.8	1.4	-0.2				
9		0.12	2.8						
10		0.39	1.4						
12	48†	0.62	6.0			29	14	125	
13		0.19	1.8						
14		0.74	2.9						
16		0.53	6.2						
17		0.27	2.5						
18		1.16	1.4						
19a/b/c	49†	0.45	3.4			26	10	110	
20/21	50†	0.80	6.9						
22		0.66	3.3						
23		1.20	4.0						
25		1.29	3.8						
26		1.22	3.9						
27		1.37	2.9						
A1273	1i	1.37	3.5						
1ii		0.99	2.6			24	15	158	
1iii		0.88	3.8						
3i/4	51	0.37	9.7	3.4	-0.9	50	27	52	
3ii	52	0.27	7.1			35	18	173	
3iii		1.12	4.2			35	20	39	
6		0.18	2.8	1.8	-0.4	14	5	64	
7		0.65	4.2			18	8	174	
8i		0.97	10.1						
8ii		0.99	5.0			38	8	87	
A1620	2		0.26	16.7	5.5	-0.9	14	3	135
4		0.29	2.1	5.1	+0.8	5	3	135	
6		0.58	2.7						
7		0.57	7.4						
8	53†	0.88	15.9			29	6	54	
A1631	1a/b/c/d	54†	0.73	32.7		105	16	138	
2ii	55†	0.64	11.7			60	14	50	
3a/b	56†	0.49	7.7			42	4	15	
5		0.38	14.1		+1.0	6	1	55	
7		0.17	22.4		-1.0			8	

Table 2. (*Continued*)

Table 2. (Continued)

4	0.39	4.5					
5	0.68	7.8					
7	0.49	5.2					
9	0.24	2.0					
10	0.32	4.6					
11	0.12	16.3	3.4	-1.3			
12	0.10	0.9					
13	0.27	1.1					
17	0.78	5.2					22.93
18	0.37	1.3	0.7	-0.5			
19	0.87	8.5			13	4	13
20	0.41	12.5			9	3	139
21	0.74	4.1					5
23	0.70	4.9					
24	0.93	4.1			14	11	60
<hr/>							
A2009	1	1.43	15.8		15	1	25
	2	1.11	2.9				
	3	0.54	1.5				
	4	0.99	1.7				
	5	0.46	5.1	1.9	-0.8		
	6	0.71	6.9			10	6
	7	66†	1.52	6.3		42	5
	8	0.75	0.9				71
	9	0.80	1.0				
	11	1.01	2.4				
	15	0.81	0.8				
	17	0.97	9.9				18
	18	1.30	3.5				
	19	1.49	7.6			12	1
	22	1.41	3.0			16	8
	23ia/b	67†	1.93	12.2			166
	23ii		1.90	3.5			
	24		2.02	10.2			
	26		1.56	5.4			
	27		2.05	10.2			
<hr/>							
A2029	3	0.09		2.4			22.96
	4	0.15	3.0	5.2	+0.5		
	5	0.22		1.6			
<hr/>							
A2052	No sources < 20 mJy						
<hr/>							
Zw1518.8	2	0.59	3.6				
	5	0.11	3.1	0.6	-1.4		
	9	0.28	7.7	2.8	-0.9	5	2
	10	0.26	1.6				96
	13a/b	68†	0.35	3.9		20	5
	14	0.45	2.6				144
	15	0.51	2.1				
	16a/b	69†	0.72	4.1			
	17	0.48	2.2				
	18	0.77	6.8				
	20	0.45	2.2				
	22	0.65	1.6				
	23	0.65	2.0				
<hr/>							
A2082	1	0.10	5.1				
	2	0.21	4.7				
	3a/b	70†	0.21	15.2			
	4	0.21	2.0				
	5	0.52	1.8			17	4
	7	0.66	4.3				164
	9i	0.55	3.6				
	9ii	0.51	2.4				
	11	0.55	5.3	2.1	-0.8	5	1
	14	0.81	4.4			9	2
	15	0.73	6.1				25
	16	0.80	2.7				16
	17	0.78	3.3				

Table 2. (Continued)

	19a/b	71†	0.90	21.2		28	11	70	
A2091	1ia/b	72†	2.46	78.9	-0.6	20	5	50	3
	1ii/a/b	73†	1.58	9.2					
	2		0.77	2.8					
	3		1.87	6.6					
	4		1.85	4.4					
	5		0.59	14.9	5.4	-0.9			
	7a/b	74	0.35	16.9	5.7	-0.9	34	4	82
	9		0.57	1.3	0.9	-0.3	11	6	48
	10		1.56	3.1			16	1	116
	11		0.78	2.2					
	12		0.79	3.3			6	2	95
	13		1.79	5.2					
	15		1.23	2.3					
	16		1.49	8.8			9	2	58
	17		1.75	6.1			14	3	100
	18		1.78	4.9					
	19		1.81	12.6			14	4	93
A2094	1		1.62	5.7					
	4		0.51	2.1					
	6		0.18	1.4					
	7		0.47	11.6	4.1	-0.9			
	8		1.18	3.0					
	10a/b	75	0.30	4.2	0.5	-1.8			
	11		0.66	19.5	5.8	-1.0	4	1	95
	12a/b	76†	0.93	11.2					12
	13		1.38	7.8					
	14		1.23	2.7					
	15		1.33	4.7					
	16		1.05	3.0					
	17		1.03	4.2					
	18		1.46	3.5					
	19		1.06	8.8					
A2103	1		0.95	8.2			7	4	35
	2		0.74	17.8			10	4	5
	3		0.78	5.9					
	4		0.65	2.3					
	5	77†	0.77	2.9			24	8	165
	7		0.55	3.0	1.7	-0.5	4	3	46
	8		0.40	2.8			8	5	68
	9a/b	78†	0.53	19.8					
	10		0.23	8.8			19	10	88
A2108	1		0.65	7.7					
	2		0.23	18.7					
	7		1.13	5.1	0.9	-1.5			
	10		1.42	3.2					
	15		1.84	14.6					
	17		1.99	7.2					
	20		2.07	8.3					
A2151	3		1.11	5.5					
	4		1.06	4.9					22.14
	6		1.34	4.2					
	7a/b	79†	1.14	19.0	4.1	-1.3	36	8	97
	8		1.28	3.0					21.93
	9		1.70	6.5					
	10		1.15	19.4	6.1	-1.0			
	13		1.07	3.1					
	14		1.11	4.0					
	15		1.46	7.9	3.5	-0.7			
	17a/b	80†	1.25	16.0					2
	18		1.99	7.4					22.29
A2249	1/2		0.52	3.7					
	3i		0.11	1.0					
	4a/b	81†	0.74	9.6			32	11	138

Table 2. (Continued)

5		0.15	18.9	4.5	-1.2	14	5	135	4	23.34	49		
7		0.50	25.1			26	7	102					
9		0.73	13.2			12	5	92					
A2354	1		1.74	6.8		19	4	37					
2			1.39	2.6									
3			0.72	1.4									
5a/b	83	0.40	12.6			52	9	12					
7		0.46	2.9										
10a/b	84	0.50	5.3										
11a/b	85	0.13	2.5			56	7	18					
12		0.89	3.9										
14		1.33	4.4										
15		1.07	2.3			22	6	96					
A2396	1		0.96	4.7									
2			0.82	7.4									
4	86	0.38	3.5	2.9	-0.2	7	4	164					
7		1.20	3.9			31	10	23					
9		0.53	3.1										
10		1.21	5.3										
12		1.61	6.4										
13		1.76	15.3										
A2399	1/3	87†	1.73	21.2									
2			1.26	15.0									
4			1.60	8.2									
7			1.21	5.6									
9			1.55	2.2									
11			1.09	2.4									
A2443	1a/b	88†	1.30	6.7									
2a/b	89†	1.15	8.2										
4		1.75	11.3										
5		1.38	4.8										
6		1.06	1.8										
8		0.21	1.3										
10		0.70	1.9										
13		1.19	2.9										
14		0.97	1.8										
15		1.58	9.6										
16		1.20	1.3										
17		0.68	1.1										
18		1.37	4.5										
19		0.74	1.2										
20		1.58	3.5										
21		1.17	3.2										
22		0.98	9.0										
23		0.98	2.1										
A2456	1		2.03	27.8									
2		1.79	21.2										
3		2.42	7.5										
4		1.47	2.3										
5		1.49	4.3										
6a/b	90†	0.94	8.6										
7		0.62	2.2										
8		0.84	6.4										
9		1.12	10.4										
10		0.18	4.8	1.4	-1.0	4	3	105					
11		1.66	3.5										
12	91†	1.31	2.0										
13ii		1.63	2.2										
13iiia/b	92†	2.27	5.8										
14i		2.34	3.2										
17		1.19	15.7										
19		2.22	6.1										
20	93†	2.32	5.4										
21		2.41	4.5										
										22.14	12		

Table 2. (Continued)

A2457	1ia/b	94†	0.14	11.8		44	7	99		
	1ii		0.01	2.3						
	2		0.24	2.6						
	4		0.45	2.1						
	5		0.79	3.5						
	9		0.52	2.1		13	3	176		
	10ii		0.71	1.6						
	11i		0.65	2.0						
A2575	1i		2.29	5.6						
	1iia/b	95†	1.78	10.7		52	11	117		
	2		2.53	8.9						
	3		2.18	9.7						
	5		0.54	12.5		6	2	145		
	8		2.36	12.0						
	9i		0.75	3.2		16	7	152		
	9ii		3.12	7.1						
	10		1.65	20.8						
	11		1.93	17.6		11	6	67		
	13		2.86	19.6						
	14		2.92	10.4						
A2593	1i		0.84	37.9						
	1ii		0.51	13.5		6	4	126		
	3		0.37	2.2						
	4i		0.08	2.3		5	2	41		
	4ii		0.34	2.2						
	5		0.12	2.0						
	6		0.05	7.3	2.2	-1.0				
	7a/b	96†	0.47	18.1		33	7	48		
	8ii		0.27	1.4		11	1	167		
	9i		0.45	1.3						
	9ii		0.23	2.1						
	11i		0.66	7.8						
	11ii		0.35	2.0		17	11	118		
	12i		0.62	2.1						
	12ii		0.42	17.3		9	6	66		
	13		0.62	3.4						
A2622	2		0.66	7.9						
	3		0.65	6.5						
	4		0.59	4.9						
	5	97	0.12	4.3		19	15	104		
	6		0.17	4.2	1.7	-0.8	7	4	152	
	7		0.24	2.2		15	1	99		
	8		0.07	10.5	1.8	-1.5				
	11a/b	98†	0.38	9.1		50	2	164		
	12		0.61	6.4						
	14a/b	99	0.23	9.1		77	14	8		
	15		0.61	12.5		17	7	111		
	16		0.47	4.1						
	17		1.11	11.9		10	5	7		
	18		0.87	9.0						
	19		0.62	4.0		17	12	172		
	20		0.63	9.8		16	10	94		
	21		0.75	30.9		-0.1	12	3	102	3
A2626	1		0.79	3.8						
	2		0.67	1.5						
	3		0.55	3.5						
	4		0.40	1.0						
	8		0.20	16.6	9.3	-0.5	3	1	36	17
	9		0.36	2.4			6	3	131	
	10		0.06	3.9	1.2	-1.0	9	6	178	17
	13		0.31	1.5						
	14		0.19	1.1	2.1	+0.5				
	16		0.35	0.9						
	18		0.87	14.5						
A2657	1		1.10	6.3			11	3	129	

Table 2. (*Continued*)

† Bandwidth smearing $\geq 7\text{arcsec}$

Column headings

Column

- 1.2 The cluster field and source number as listed by SPS89.
 - 3 Contour map number within Figure 1.
 - 4 Angular distance of the source centroid from the cluster centre, normalized to the optical radius (R_c) of the cluster.
 - 5.6 The integrated flux densities at 1.5 GHz and 4.9 GHz.
 - 7 The spectral index from our 1.5 and 4.9 GHz flux densities if the latter is available. Otherwise from our 1.5 GHz flux and flux densities listed in the references in column 11.
 - 8.9,10 The major and minor axes to 50% brightness of the fitted, deconvolved Gaussian ellipse and the position angle (measured from north through east) of the major axis.
 - 11 References to other radio measurements of the source.
 - 12,13 The emitted 1.5 GHz radio power and linear size for sources with measured red shifts

Reference to Other Measurements

1. Andernach et al (1980)
 2. Andernach et al. (1986)
 3. Becker, White and Edwards (1991)
 4. Zhao et al. (1989)
 5. Owen, White and Burns (1992)
 6. Slee and Siegman (1983)
 7. White and Becker (1992)
 8. Reynolds (1986)
 9. Mills and Hoskins (1977)
 10. Large et al. (1981)
 11. Slee and Reynolds (1984)
 12. Haslam et al. (1978)
 13. Harris et al. (1980)
 14. Feretti and Giovannini (1994)
 15. Waldhausen et al. (1979)
 16. Harris and Miley (1978)
 17. Roland et al. (1985)
 18. Riley (1975)
 19. Andernach et al. (1988)
 20. Griffith et al. (1995)

Table 3. Sources with double components

Cluster Field	Source Number	Map Number	Component Positions (B1950)						Component Fluxes mJy	Flux Ratio Sa/Sb	Component Axes a/b	Ratio of Maj. Axes a/b	Comp. Sep. °	
			RA	Dec	a	RA	Dec	b						
(1)	(2)	(3)	h m s	° ' "	h	m	s	° ' "	(8)	(9)	(10)	(11)	(12)	(13)
Abell 13	13iiia/b	2†	00 12 10.25	-19 43 08.9	00	12	12.96	-19 43 08.6	5.0	4.8	1.0			38.3, 90
Abell 85	9a/b	5†	00 38 11.43	-09 39 50.3	00	38	10.44	-09 39 42.3	1.0	0.6	1.7			16.7, 119
	21iiia/b	6†	00 38 48.56	-09 27 18.9	00	38	49.42	-09 27 37.3	0.7	0.3	2.3			22.4, 145
	36iiia/b	9†	00 39 22.30	-10 21 10.3	00	39	21.44	-10 20 54.1	13.4	9.9	1.4			20.6, 142
Abell 115	1ia/b	11	00 52 50.43	26 11 54.3	00	52	48.66	26 11 49.0	3.9	1.4	2.8			2.2
	3a/b	12	00 53 10.11	26 14 09.6	00	53	09.03	26 14 23.6	2.5	2.4	1.0			24.4, 78
	9a/b	13†	00 53 45.76	26 07 44.5	00	53	47.67	26 08 00.4	9.1	2.2	4.1			20.2, 134
Abell 240	13a/b	17	01 38 35.62	07 29 46.3	01	38	34.13	07 28 55.8	5.5	4.8	1.1			30.2, 58
	15a/b	18†	01 39 01.67	07 42 00.7	01	39	01.25	07 41 42.0	9.9	4.7	2.1			19.7, 19
Abell 362	16a/b	23†	02 30 04.31	-04 59 22.1	02	30	02.68	-04 59 11.6	3.5	3.2	1.1			26.5, 113
Abell 407	19a/b	26†	02 59 18.58	35 48 58.9	02	59	18.68	35 48 30.9	3.1	2.4	1.3			28.0, 178
Abell 474	18a/b	29	04 05 52.08	-16 46 14.4	04	05	54.16	-16 46 29.1	4.0	2.1	1.9			33.3, 116
	19a/b	30†	04 06 24.79	-16 56 27.1	04	06	23.06	-16 56 52.6	8.1	4.0	2.0			35.6, 44
Abell 519	7iiia/b	32†	04 51 24.84	00 55 03.9	04	51	24.70	00 54 38.7	5.1	3.3	1.5			25.3, 5
Abell 658	8a/b	34†	08 20 47.82	15 52 58.1	08	20	49.56	15 52 54.8	2.9	1.4	2.0			25.3, 97.5
Abell 912	8a/b	39†	09 59 31.67	00 18 38.9	09	59	37.24	00 18 24.4	13.7	11.6	1.2			84.8, 100
Abell 1142	16a/b	41†	11 00 32.38	10 42 15.8	11	00	30.73	10 42 20.3	5.1	3.0	1.7			25.101
Abell 1171	8a/b	43†	11 04 18.59	02 54 20.4	11	04	17.55	02 53 48.2	2.6	1.8	1.4			35.7, 26

Abell 1189	9a/b	44	11 08 50.95	01 27 53.9	11 08 48.73	01 27 47.8	2.5	2.3	1.1		33.8, 80
Abell 1238	5a/b	46 [†]	11 19 57.84	01 12 10.4	11 19 56.57	01 12 30.6	2.1	1.6	1.3		27.8, 137
	8a/b	47	11 20 11.88	01 27 32.0	11 20 13.68	01 27 14.4	0.9	0.7	1.3		32.2, 123
20/21		50 [†]	11 20 50.05	01 13 52.9	11 20 53.44	01 13 48.0	2.2	2.1	1.0		51.1, 96
Abell 1273	3i/4	51	11 26 34.59	-06 47 57.7	11 26 37.07	-06 47 41.1	6.9	5.8	1.2		40.5, 66
Abell 1631	3a/b	56 [†]	12 49 33.35	-15 20 00.4	12 49 32.95	-15 20 24.8	4.4	3.2	1.4		25.1, 13
	23a/b	57 [†]	12 51 17.44	-14 55 26.4	12 51 16.47	-14 55 27.4	3.0	2.1	1.4		14.1, 86
Abell 1689	2ii/a/b	59 [†]	13 07 54.65	-00 47 20.4	13 07 52.43	-00 47 29.0	64.0	48.0	1.3		34.4, 76
18a/b	60	13 09 07.94	-01 07 48.4	13 09 09.00	-01 07 30.6	9.1	2.3	4.0			23.9, 42
19a/b	61	13 09 09.02	-01 03 28.2	13 09 09.75	-01 03 49.9	6.7	5.1	1.3			24.3, 153
Abell 1772	9a/b	62 [†]	13 40 03.29	-10 55 00.7	13 40 02.12	-10 54 51.4	1.0	0.8	1.3		19.6, 118
	12a/b	63 [†]	13 40 26.44	-10 47 43.6	13 40 27.63	-10 47 40.9	2.0	1.8	1.1		17.7, 81
Abell 1775	11a/b	64 [†]	13 39 31.79	26 53 19.2	13 39 32.15	26 53 44.6	3.3	2.0	1.7		25.9, 11
	14a/b	65 [†]	13 39 44.67	26 19 12.5	13 39 44.64	26 18 52.0	5.4	3.4	1.6		20.5, 1
Abell 2009	23ia/b	67 [†]	14 59 07.66	21 19 19.9	14 59 08.05	21 19 43.5	4.8	3.1	1.5		24.2, 13
Zw 1518.8	13a/b	68 [†]	15 19 42.06	07 45 09.9	15 19 41.42	07 45 21.8	2.5	1.4	1.8		15.2, 141
	16a/b	69 [†]	15 19 52.09	08 09 05.5	15 19 52.96	08 09 21.6	1.7	0.6	2.8		20.6, 39
Abell 2082	3a/b	70 [†]	15 28 19.61	03 42 18.8	15 28 17.49	03 41 50.0	9.8	2.3	4.3		42.9, 48
	19a/b	71 [†]	15 29 42.65	03 41 37.0	15 29 41.07	03 41 30.9	14.0	4.1	3.4		24.4, 76
Abell 2091	1ia/b	72 [†]	15 30 40.76	10 11 22.9	15 30 39.66	10 11 08.9	41.4	37.4	1.1		21.4, 49
	1iiab	73 [†]	15 31 15.71	10 35 32.4	15 31 17.11	10 35 38.1	3.7	3.6	1.0		21.4, 74
	7a/b	74	15 31 57.26	10 21 51.5	15 31 58.73	10 21 53.9	10.1	7.3	1.4		21.8, 84
Abell 2094	10a/b	75	15 34 10.50	-01 49 24.9	15 34 09.00	-01 49 10.7	4.1	1.6	2.6		26.6, 122
	12a/b	76 [†]	15 34 18.43	-02 01 41.7	15 34 16.86	-02 02 17.0	5.7	5.6	1.0		42.5, 34
Abell 2103	9a/b	78 [†]	15 37 16.80	-02 14 24.1	15 37 15.08	-02 14 01.0	13.6	3.4	4.0		34.6, 132

Table 3. (Continued)

Abell 2151	7a/b 17a/b	79† 80†	16 04 14.95 16 05 16.68	18 19 21.4 18 05 03.2	16 04 13.22 18 04 58.9	18 19 24.9 18 04 58.9	10.4 7.4	7.7 5.6	1.4 1.3	10, 5, 62 1.3	14, 8, 113 1.3	0.7	24.9, 98 25.3, 100
Abell 2249	4a/b	81†	17 07 58.49	34 12 40.4	17 07 57.56	34 12 58.5	4.9	2.2	2.2				21.5, 148
Abell 2354	5a/b 10a/b 11a/b	83 84 85	21 32 50.69 21 33 11.83 21 33 13.43	-15 06 48.6 -15 14 12.4 -15 08 42.5	21 32 50.91 21 33 09.14 21 33 12.71	-15 06 17.1 -15 13 53.3 -15 09 13.0	8.3 3.0 1.4	3.3 2.0 1.0	2.5 2.0 1.4	28, 5, 31 20, 9, 166			31.7, 6 43.4, 116 32.2, 19
Abell 2399	1/3	87†	21 53 09.07	-08 37 42.1	21 53 05.57	-08 37 18.1	11.5	8.5	1.4	24, 15, 91			57.2, 115
Abell 2443	1a/b 2a/b	88† 89†	22 22 37.05 22 22 48.23	17 10 05.3 16 59 44.8	23 22 38.66 22 22 47.98	17 10 16.5 16 59 12.8	3.0 4.1	1.3 3.4	2.3 1.2	19, 11, 1			25.6, 64 32.2, 6
Abell 2456	6a/b 13iii/a/b	90† 92†	22 32 05.00 22 32 33.28	-15 39 39.7 -15 51 03.9	22 32 05.57 22 32 34.59	-15 39 23.5 -15 50 51.1	4.7 4.5	4.0 1.3	1.2 3.5	14, 7, 12			18.2, 27 22.8, 56
Abell 2457	1iiab	94†	22 33 13.35	01 16 14.5	22 33 11.55	01 16 18.6	6.0	6.0	1.0	17, 5, 111	21, 11, 82	0.8	27.3, 99
Abell 2575	1iiab	95†	23 16 23.25	-22 20 42.3	23 16 25.21	-22 20 56.1	6.1	5.0	1.2	17, 8, 29			30.5, 117
Abell 2593	7a/b	96†	23 22 00.54	14 35 24.1	23 22 01.75	14 35 40.1	10.7	6.2	1.7	9, 4, 147			23.7, 48
Abell 2622	11a/b 14a/b	98† 99	23 32 33.55 23 32 45.34	27 16 43.2 27 11 26.2	23 32 33.32 23 32 45.21	27 17 04.7 27 10 54.9	4.5 2.8	0.8 2.4	5.6 1.2	30, 3, 53	15, 7, 141	2.0	21.7, 172 31.4, 3
Abell 2657	2a/b	100†	23 43 26.67	08 27 50.0	23 43 26.91	08 28 26.9	8.5	4.1	2.1	9, 4, 137			37.1, 6
Abell 4038	13a/b 16a/b	101† 102†	23 45 20.98 23 45 44.88	-28 16 32.7 -28 30 13.5	23 45 22.74 23 45 42.69	-28 16 58.1 -28 30 23.9	2.8 2.2	2.0 1.8	1.4 1.2	12, 4, 115 40, 10, 90			34.4, 138 30.7, 70

† Bandwidth smearing ≥ 7 arcsec**Column headings**

- 1 The cluster field
- 2 Source number
- 3 Contour map number within Figure 1.

4.5 The RA and declination of the centroid of component 'a'.

6,7 The RA and declination of the centroid of component 'b'.

8,9 The 1.5 GHz flux densities of the components.

10 The ratio of the flux densities of the components.

11,12 Deconvolved ellipse axes and position angles of the components (from north through east).

13 Ratio of the major axes of the components.

14 Angular separation of the components and its position angle (from north through east).

Table 4. Sources with triple and quadruple components

Cluster Field (1)	Source Number (2)	Map Number (3)	Component Flux Density c mJy (5)	Component Flux Density d mJy (6)	Gaussian-fit Ellipses*				Component Separations#				
					a ° (4)	b ° (5)	c ° (7)	d ° (8)	a ° (9)	b ° (10)	c ° (11)	d ° (12)	
Abell 13	6a/b/c	1	1.8	1.4	0.7	32,	11,20	9, 3, 8		37.9,	104	20,3	130
Abell 85	22a/b/c	7†	3.0	1.6	0.7					18.6,	9	26,3	3
	25a/b/c	8	3.8	1.9	1.8	80,	9, 15,2	25, 9, 21	28, 20,	50.6,	11,6	74,7,	78
	421a/b/c	10†	2.0	1.0	0.5	33,	23, 7,6		121	48.0,	86	49,7,	23
Abell 1238	19a/b/c	49†	1.6	1.0	0.8	23,	12, 12,1			41.7,	7,4	37,1,	5
Abell 1631	1a/b/c/d	54†	15.5	13.2	4.3	4.0	65,	20, 12,1	119, 12, 52	108.5,	14,3	64,9,	150
										44.8,	13,3	23,9,	16,2
										66,6,	14,3		

† Bandwidth smearing > 1 arcsec

* Major and minor axes of deconvolved ellipse and position angle of major axis (from north through east).

Separation of components and it's position angle (from north through east).

Table 5. Optical Identifications

Field & Source No.	RA h (1) (2)	Dec. m (3)	Optical Position RA h m (4)	Dec. m s (5)	Angular Position Distance " " " (6)	Apparent Mag. PSSE R (7)	Morph. SRC B_J (8)	Heliocent. Redshift z (10)	Reference z (11)	Catalogue Name (12)	(13)
Abell 13											
2i	00 09 41.73	-19 54 59.8	BF								
2ii	00 09 43.95	-19 31 50.5	BF								
3	00 10 02.81	-19 37 37.2	BF								
4	00 10 31.71	-19 52 06.5	BF								
5	00 10 51.14	-19 39 03.5	00 10 51.21	-19 39 01.0	3	22	20.8	E			
			00 10 50.23	-19 38 52.1	17	-48	21.5	G			
			00 10 55.35	-19 46 47.7	12	90	19.7	E			
			00 10 53.21	-19 46 46.2	18	-85	17.7	E			
			00 10 56.27	-19 46 50.3	25	96	18.8	E			
6a/b/c	00 10 54.51	-19 46 47.7	BF								
			00 11 11.90	-19 46 21.4	2	11	20.8	E			
			00 11 14.54	-19 51 44.2	8	-114	19.0	St			
			00 11 14.94	-19 51 42.4	2	-122	2x19.3	2xSt			
8	00 11 04.67	-19 53 13.4	BF								
9i	00 11 11.87	-19 46 23.6	00 11 11.90	-19 46 21.4	2	11	20.8	E			
9ii	00 11 15.03	-19 51 41.2	00 11 14.54	-19 51 44.2	8	-114	19.0	St			
			00 11 14.94	-19 51 42.4	2	-122	2x19.3	2xSt			
10	00 11 31.18	-19 57 18.5	BF								
11	00 11 50.49	-19 32 00.3	00 11 50.49	-19 32 00.3	6	180	20.6	St			
12	00 11 58.53	-19 59 15.6	BF								
13i	00 12 09.05	-19 59 22.0	00 12 08.14	-19 59 33.4	17	-132	21.5	St			
13ia/b	00 12 11.66	-19 43 08.9	BF								
14	00 12 15.17	-19 43 55.5	00 12 15.06	-19 43 53.6	2	-39	18.8	St			
			00 12 16.46	-19 43 48.6	19	69	20.8	G			
Abell 76											
2	00 36 59.05	06 56 19.0	00 36 58.99	06 56 13.9	5	-170	19.5	G			
			00 36 58.80	06 56 06.4	13	-163	19.5	G			
			00 36 59.69	06 56 06.0	16	144	19.5	St			
3	00 37 12.65	06 57 14.2	BF								
4	00 37 12.89	06 52 54.9	BF								
6i	00 37 21.02	07 09 24.5	BF								
6ii	00 37 23.21	06 57 47.5	00 37 23.63	06 57 54.1	9	43	19.5	G			

7	00 37 24.24	07 03 22.5	00 37 23.68	06 57 46.1	21	94	19.5	G											
9	00 37 32.43	06 57 06.2	00 37 24.39	06 57 41.7	9	130	17.3	E											
10	00 37 40.48	07 02 47.0	00 37 33.23	07 03 19.5	4	143	18.5	G											
11	00 37 40.69	07 10 00.8	00 37 40.42	06 57 09.1	12	76	17.5	E											
12	00 37 47.47	07 01 47.2	00 37 41.30	07 02 52.1	5	-10	19.5	St											
14	00 37 59.25	07 05 48.1	00 37 59.26	07 05 47.7	0	18.2	E												
15	00 38 05.76	07 05 46.1	BF																
16	00 38 16.79	07 11 26.3	BF																
18	00 38 23.45	07 06 01.7	00 38 23.65	07 06 03.4	3	60	19.3	G											
19	00 38 57.38	06 41 33.0	BF																
Abell 85																			
2i	00 37 50.49	-10 18 19.9	00 37 49.56	-10 18 31.3	18	-130	17.4	St											
2ii	00 37 51.54	-10 09 29.7	00 37 50.95	-10 09 25.2	10	-63	21.9	G											
4	00 37 56.25	-10 15 39.5	BF																
5	00 37 58.25	-09 41 02.3	00 37 58.99	-09 40 51.8	15	46	17.5	E											
6	00 37 58.89	-09 56 40.1	BF																
8	00 38 11.79	-10 07 36.9	BF																
9ab	00 38 11.02	-09 39 46.8	00 38 10.01	-09 40 01.2	21	-134	14.3	St											
			00 38 11.50	-09 39 38.0	11	39	15.5	St											
10	00 38 12.51	-09 46 07.0	BF																
11	00 38 15.66	-09 29 07.9	00 38 15.39	-09 29 04.0	6	-46	19.5	22.3	G										
14	00 38 22.65	-09 20 02.4	BF																
15	00 38 23.24	-10 12 54.7	BF																
16	00 38 23.80	-10 01 17.3	BF																
17	00 38 27.66	-10 00 28.5	00 38 27.47	-10 00 25.7	4	-45	>19.5	21.4	G										
18	00 38 28.58	-10 05 49.4	BF																
19	00 38 34.92	-09 45 11.6	BF																
20i	00 38 41.87	-09 50 30.5	00 38 41.68	-09 50 34.3	5	-144	21.8	G											
20ii	00 38 42.45	-09 29 35.4	00 38 42.45	-09 29 36.4	1	180	>19.5	21.9	G										
21i	00 38 48.22	-09 35 52.1	BF																
22ab/c	00 38 48.69	-09 27 21.4	BF																
23i	00 38 49.70	-09 52 30.6	BF																
	00 38 52.29	-10 13 09.7	BF																

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Table 5. (*Continued*)

Abell 86									
4	00 39 34.17	-09 55 42.3	00 39 32.69	-09 30 58.1	18	27	22.7	G	
7i	00 39 38.79	-09 44 02.1	00 39 38.43	-09 44 11.9	11	-151	16.8	St	
7ii			00 39 39.90	-09 43 59.2	17	80	19.1	E	
8i	00 39 39.35	-09 33 00.8	BF						
8ii	00 39 40.87	-09 27 08.5	BF						
9	00 39 41.12	-09 24 41.2	BF						
0	00 39 42.28	-09 49 09.4	00 39 41.43	-09 49 20.7	17	-132	17.5	E	
1-ii	00 39 44.24	-09 42 54.7	00 39 43.46	-09 42 48.0	13	-60	17.6	17.3	E
1-iii	00 39 44.74	-09 42 09.8	00 39 44.17	-09 42 22.4	15	-146	19.5	20.8	E
1-iv	00 39 48.08	-09 26 02.4	00 39 45.90	-09 41 57.2	21	54	>19.5	22.8	G
1-iii	00 39 49.57	-09 20 48.5	00 39 49.28	-09 20 56.6	20	-57	18.4	St	
1-ii	00 39 53.25	-09 43 28.6	00 39 52.80	-09 43 42.6	16	-155	18.8	19.3	St
1-iii	00 39 55.40	-09 52 36.8	BF						
1-iv	00 39 56.87	-09 28 46.6	00 39 56.28	-09 28 59.5	16	-146	19.3	St	
1-iii	00 40 01.90	-09 50 29.2	BF						
1-ii	00 40 04.03	-09 28 36.4	BF						
1-iii	00 40 09.05	-09 41 37.2	BF						
1-ii	00 38 32.53	-22 09 55.0	00 38 33.28	-22 10 09.9	18	145	20.3	St	
2	00 38 53.40	-22 03 14.7	00 38 54.01	-22 03 29.2	17	150	20.6	St	
3	00 39 24.64	-22 16 20.2	BF						
4i	00 39 34.00	-22 12 10.1	00 39 33.47	-22 12 14.4	8	-120	21.5	G	
4ii	00 39 40.02	-22 07 51.0	00 39 39.17	-22 07 45.5	13	-65	20.6	St	
5	00 39 44.27	-22 18 40.6	00 39 43.94	-22 18 45.6	7	-138	20.8	G	
6	00 39 45.41	-22 03 31.9	00 39 45.35	-22 03 33.1	1	-26	21.0	G	
7	00 39 46.82	-22 23 30.4	00 39 45.97	-22 23 28.2	12	-79	20.4	G	
8	00 39 56.22	-22 16 24.6	00 39 56.30	-22 16 26.9	3	154	19.5	St	
9	00 39 58.05	-21 58 53.1	BF						
10	00 40 01.49	-22 19 10.6	BF						
11i	00 40 08.52	-22 09 46.9	00 40 08.39	-22 09 53.5	7	-165	18.2	E	
11ii			00 40 10.14	-22 09 43.6	23	82	20.5	G	
13i	00 40 23.07	-22 11 35.6	BF						
13ii	00 40 36.20	-22 04 22.5	00 40 34.94	-22 04 22.4	18	-90	18.9	E	

Table 5. (*Continued*)

14	00 40 57.91	-22 22 03.3	00 40 35.56	-22 04 23.2	9	-94	20.9	St
Abell 115								
1ia/b	00 52 49.96	26 11 53.0	00 52 49.16	26 11 41.9	15	-136	19.6	St
1ii	00 52 58.88	26 22 56.9	BF					
3a/b	00 53 09.90	26 14 12.8	BF					
4	00 53 17.52	26 01 41.5	BF					
6	00 53 27.07	26 08 57.6	00 53 27.09	26 08 57.1	1	152	17.3	E
7	00 53 41.05	26 06 49.0	00 53 40.99	26 07 05.2	16	-3	19.5	G
8	00 53 41.57	26 11 38.1	00 53 40.85	26 06 45.6	4	-142	17.5	E
9a/b	00 53 45.86	26 07 45.0	00 53 41.85	26 11 19.0	19	169	18.0	St
Abell 133								
1	00 59 04.56	-22 10 42.4	00 59 04.23	-22 10 30.4	13	-21	19.3	St
3	00 59 54.00	-22 00 04.7	00 59 53.83	-22 00 09.0	5	-151	20.5	E
4	00 59 57.76	-22 09 51.2	BF			-5	21.5	G
5	01 00 02.22	-22 07 13.3	BF					
6	01 00 11.23	-22 09 12.5	01 00 11.17	-22 09 11.5	1	-40	17.4	E
9	01 00 18.87	-22 26 00.0	BF			71	17.4	E
11	01 00 23.89	-22 25 32.6	01 00 23.80	-22 25 36.3	4	-161	18.6	St
12	01 00 42.27	-22 19 17.2	01 00 42.07	-22 19 13.1	5	-34	21.8	G
13i	01 00 43.96	-22 15 48.5	BF					
13ii	01 00 53.66	-22 22 41.0	BF					
14	01 00 55.93	-22 04 28.1	BF					
15	01 01 07.61	-22 15 12.0	01 01 06.47	-22 15 10.3	16	-84	21.1	E
16	01 01 10.69	-22 15 44.5	01 01 11.11	-22 15 18.9	10	-134	22.0	G
17	01 01 30.44	-22 10 58.8	01 01 30.08	-22 10 39.2	20	-14	20.1	E
Abell 154								
1	01 08 30.52	17 31 22.8	BF					
3	01 09 00.62	17 38 47.8	01 09 00.30	17 38 47.5	5	-94	16.2	E
5i	01 09 03.61	17 30 33.8	BF					

Table 5. (Continued)

3	01 53 58.89	32 02 37.1	01 53 59.70	32 02 52.5	19	34	17.7	E
7	01 54 27.56	31 58 16.0	01 54 27.49	31 58 15.7	1	-109	16.2	E
9	01 54 51.04	31 40 45.4	01 54 50.40	31 40 49.7	9	-62	17.5	St
11	01 55 06.90	32 02 11.9	01 55 07.96	32 02 13.6	14	-102	18.3	G
		01 55 07.29	32 02 02.3	11	153	83	19.5	G
						16.1	St	
<i>Abell 357</i>								
1	02 25 31.51	12 56 17.2	BF					
2	02 25 42.78	13 12 16.2	02 25 43.04	13 12 32.7	17	13	19.3	St
3	02 25 44.76	13 06 39.0	BF					
4	02 26 01.54	13 13 52.6	BF					
6	02 26 40.63	13 09 33.8	02 26 40.81	13 09 36.0	3	50	19.3	G
7	02 26 45.23	13 08 47.2	BF					
<i>Abell 362</i>								
1	02 28 22.60	-05 04 37.1	02 28 22.58	-05 04 34.6	3	-7	18.4	21.5
3	02 28 44.06	-04 56 00.8	02 28 23.30	-05 04 46.0	14	130	18.5	21.5
4	02 28 55.53	-05 01 30.0	02 28 55.23	-05 01 26.6	6	-120	16.4	17.1
5	02 28 56.80	-04 54 36.8	BF			-53	16.6	17.2
7	02 29 09.06	-05 05 20.7	02 29 08.89	-05 05 21.6	3	-110	17.8	20.7
9	02 29 12.46	-05 12 35.7	02 29 12.27	-05 12 38.4	4	-134	90	17.5
11	02 29 18.16	-05 01 36.0	02 29 17.14	-05 01 33.5	15	-81	17.5	20.4
12	02 29 23.29	-05 12 20.0	BF					E
13i	02 29 24.92	-05 10 37.8	02 29 24.21	-05 10 37.6	11	-89	16.2	21.1
13ii	02 29 28.84	-04 47 12.3	02 29 24.80	-05 10 48.9	11	-171	16.7	St
13iii	02 29 31.83	-05 25 42.7	02 29 31.61	-05 25 52.4	10	-161	22.0	
15	02 30 02.90	-05 17 25.1	BF					
16a/b	02 30 03.55	-04 59 18.2	02 30 04.18	-04 59 17.9	9	88	17.8	21.0
		02 30 05.12	-04 59 21.5	24	98	>19.5	22.7	E
<i>Abell 407</i>								
1	02 57 15.56	35 35 17.5	02 57 16.24	35 35 19.9	9	74	16.5	St
			02 57 17.18	35 35 13.5	20	101	18.5	St
2	02 57 19.90	35 42 06.3	02 57 16.17	35 35 02.9	16	153	19.3	G
			BF					

Table 5. (*Continued*)

Abell 474									
2	04 04 32.62	-16 35 05.5	BF						
4	04 04 53.73	-16 59 37.5	BF						
5	04 04 56.05	-17 00 34.2	04 04 56.63	-17 00 29.0	10	58	22.0	G	
6	04 04 56.26	-16 39 17.4	04 04 55.83	-16 39 26.8	11	-147	19.5	22.3	G
7	04 05 02.49	-16 53 54.5	BF						
8	04 05 02.56	-16 45 28.1	BF						
9	04 05 04.86	-16 39 00.1	BF						
10	04 05 10.37	-17 02 06.4	04 05 11.61	-17 01 56.7	20	61	>19.5	21.5	G
11	04 05 10.71	-17 04 35.6	04 05 10.01	-17 04 45.3	14	-134	19.3	19.8	G
12	04 05 20.98	-16 54 38.3	BF						
14	04 05 33.84	-16 48 31.6	04 05 32.92	-16 48 17.3	19	-43	19.0	21.0	St
15	04 05 45.93	-16 57 06.9	04 05 34.50	-16 48 49.7	20	152	17.5	19.1	E
16	04 05 47.52	-16 41 18.7	BF						
17	04 05 47.96	-17 03 38.1	BF						
18a/b	04 05 52.09	-16 46 14.4	04 05 53.36	-16 46 23.8	21	117	18.3	20.5	G
19a/b	04 06 23.91	-16 56 39.0	04 06 23.74	-16 56 37.5	3	-58	17.1	17.6	St
Abell 496									
2	04 30 36.30	-13 11 58.3	04 30 37.15	-13 12 12.2	19	138	16.0	16.1	St
3	04 31 13.12	-13 19 08.3	BF						
5	04 31 23.91	-13 26 33.5	04 31 23.59	-13 26 36.0	5	-118	16.8	E	0.0341
6	04 31 29.33	-13 22 20.3	BF						
7	04 31 29.47	-13 15 45.3	BF						
8	04 31 36.94	-13 06 51.8	BF						
12	04 32 04.06	-13 23 06.4	BF						
13	04 32 05.59	-13 29 20.6	04 32 05.30	-13 29 28.4	9	-152	22.7	G	
			04 32 05.37	-13 29 33.4	13	-166	21.7		
Abell 514									
1	04 45 14.70	-20 32 00.2	BF						
3	04 45 48.74	-20 52 49.9	04 45 49.43	-20 52 41.2	13	48	21.2	G	
7	04 46 09.64	-20 36 30.1	04 46 08.60	-20 36 35.7	16	-111	20.8	St	
9	04 46 21.39	-20 40 00.5	BF						
11	04 46 27.10	-20 48 02.6	04 46 26.68	-20 47 59.8	7	-65	20.0	St	
12	04 46 32.91	-20 27 52.6	04 46 32.06	-20 27 44.3	15	-55	20.5	St	

13		04 46 34.40	-20 25 14.6	BF								
14		04 46 34.43	-20 38 18.8	04 46 35.81	-20 38 14.7	20	78		20.3	G		
16		04 46 52.07	-20 43 05.1	04 46 52.58	-20 43 17.4	14	150		20.6	St		
17		04 46 56.47	-20 42 51.3	04 46 55.54	-20 42 57.1	14	-114		18.5	St		
18		04 47 10.34	-20 23 56.1	BF								
20		04 47 41.28	-20 42 10.7	04 47 41.82	-20 42 20.4	12	142		20.3	E		
Abell 519												
2		04 50 22.38	00 22 43.0	04 50 21.84	+00 22 43.8	8	-84	17.5	20.1	St		
4		04 50 36.12	00 25 10.9	04 50 22.42	+00 22 48.0	5	7	18.9	22.0	G		
				04 50 35.56	+00 24 55.9	17	-151	18.2	24.2	St		
				04 50 36.01	+00 25 02.1	9	-169	17.8	21.4	E		
5		04 50 37.16	00 48 01.1	04 50 37.16	+00 25 04.0	17	114	15.5	11.1	St		
6		04 50 45.46	00 21 10.2	BF								
7 <i>i</i>		04 51 04.16	00 53 10.4	BF								
7 <i>ii</i>		04 51 22.54	00 55 29.1	BF								
7 <i>iii/a/b</i>		04 51 24.81	00 54 53.1	BF								
9		04 51 29.08	00 35 15.5	04 51 28.29	+00 35 02.9	17	-137	15.8	12.7	St		
				04 51 29.07	+00 35 14.4	1	-172	17.2	19.2	E		
10		04 51 29.78	00 30 16.2	BF								
11		04 51 38.64	00 44 18.6	BF								
12		04 52 02.84	00 36 29.9	04 52 02.97	+00 36 29.2	2	110	17.3	20.2	E		
Abell 531												
2		04 58 06.54	-03 42 12.6	04 58 06.66	-03 42 33.4	21	175		19.1	St		
3		04 58 27.19	-03 33 24.0	04 58 26.56	-03 33 35.2	15	-140	19.2	19.5	St		
				04 58 27.52	-03 33 29.3	7	137	17.5	17.5	St		
				04 58 28.32	-03 33 38.8	22	131	18.2	18.7	E		
4		04 58 34.03	-03 26 26.6	04 58 33.91	-03 26 22.8	4	-25		21.4	E		
5		04 58 38.55	-03 35 33.2	04 58 38.31	-03 35 26.2	8	-27	19.0	19.8	St		
				04 58 38.41	-03 35 31.0	3	-44	19.3	20.3	St		
				04 58 39.86	-03 35 41.4	21	113	>19.5	22.7	G		
6		04 58 40.66	-03 43 18.5	BF								
8		04 58 48.46	-03 29 09.2	BF								
9		04 58 49.67	-03 38 10.5	04 58 49.10	-03 37 55.2	18	-29	19.6	21.5	G		
10		04 58 50.10	-03 22 07.8	04 58 48.88	-03 22 04.4	19	-79	18.3	18.1	St		
				04 58 48.90	-03 22 16.8	20	-117	16.7	16.0	St		
				04 58 50.62	-03 22 03.2	9	59	19.0	20.0	G		

Table 5. (*Continued*)

Table 5. (Continued)

MCG 01-29-001 IRAS 11049+0300									
14	11 04 37.97	03 14 36.2	BF						S0
15	11 04 38.70	03 10 34.0	BF						
17	11 04 51.46	02 47 19.3	BF						
18	11 04 57.75	03 00 58.1	11 04 57.99	03 00 56.5	4	114	16.2		
19	11 04 59.52	03 14 59.2	11 04 57.53	03 00 53.1	6	-147	16.3	E	
20	11 05 01.68	03 12 07.4	BF	03 14 49.5	22	116	17.7	G	
23	11 05 28.53	03 15 41.2	BF						
24	11 05 38.22	02 54 04.9	11 05 37.04	02 54 13.0	19	-65	18.0	E	
			11 05 37.95	02 54 05.7	4	-79	16.6	St	
			11 05 38.41	02 53 57.3	8	159	19.6	St	
Abell 1189									
2ii	11 07 54.07	01 19 51.6	BF						
2iii	11 08 14.65	01 29 56.9	BF						
3	11 08 21.70	01 26 09.1	11 08 21.70	+01 26 07.2	2	180	11.9	St	
4	11 08 23.03	01 27 36.4	BF						
7	11 08 46.50	01 23 31.9	BF						
8	11 08 48.25	01 17 27.0	11 08 48.06	+01 17 21.1	7	-154	19.2	E	
9a/b	11 08 49.74	01 27 50.7	BF						
11	11 08 54.13	01 36 05.9	BF						
12i	11 08 56.74	01 25 48.8	BF						
12ii	11 08 59.15	01 36 33.6	11 08 57.95	+01 36 38.9	19	-74	22.3	G	
13ii	11 09 36.53	01 20 29.5	BF						
Abell 1238									
1	11 19 31.85	01 10 32.9	11 19 32.80	+01 10 35.5	14	80	21.6	St	
3	11 19 52.32	01 31 55.7	11 19 51.46	+01 32 09.1	19	-44	19.5	22.2	St
			11 19 52.22	+01 31 59.2	4	-23	17.7	19.4	St
4	11 19 53.97	01 20 10.5	11 19 52.83	+01 31 36.7	20	158	>19.5	21.4	St
			11 19 52.86	+01 20 12.5	17	-83	>19.5	21.6	G
6	11 19 57.44	01 12 17.4	11 19 57.55	+01 12 09.7	8	-35	19.3	20.8	St
7	11 19 57.07	01 42 00.9	11 19 57.00	+01 41 57.8	3	168		22.5	G
			11 19 57.2	+01 20 27.0	20	-161	>19.5	22.6	G
8a/b	11 19 57.38	01 22 08.2	11 19 57.45	+01 22 04.2	4	165	17.3	19.4	St
9	11 20 12.51	01 27 25.6	11 20 11.54	+01 27 33.2	16	-62	17.1	19.5	E
	11 20 15.73	01 23 18.9	11 20 15.42	+01 23 11.9	8	-146	16.3	18.0	E
			11 20 16.07	+01 23 05.5	14	159	19.2	20.0	G

10	11 20 17.76	01 28 18.4	11 20 17.76	+01 28 24.2	6	0	16.3	18.2	E
12	11 20 23.12	01 13 44.3	BF						
13	11 20 26.01	01 25 25.4	BF						
14	11 20 26.79	01 12 14.7	BF						
16	11 20 31.96	01 15 27.6	BF						
17	11 20 36.59	01 21 14.9	11 20 36.99	+01 21 03.6	13	152	17.5	19.3	E
18	11 20 38.67	01 27 02.8	BF						
19a/b/c	11 20 46.57	01 25 36.3	BF						
20	11 20 50.05	01 13 52.9	11 20 49.08	+01 14 14.6	26	-34	17.3	18.7	E
			11 20 49.94	+01 13 56.5	4	-25	2x19.0	19.7	G
21	11 20 53.44	01 13 48.0	11 20 50.77	+01 13 48.9	12	110	17.9	20.0	E
22	11 20 57.61	01 26 46.1	BF.	+01 14 08.1	22	-24	>19.5	22.3	G
23	11 20 59.83	01 37 31.2	11 20 59.29	+01 37 29.5	8	-102	19.5	21.9	G
25	11 21 06.13	01 37 53.7	BF						
26	11 21 32.71	01 25 29.2	11 21 32.55	+01 25 23.3	6	-158	17.6	19.2	E
27	11 21 33.11	01 13 29.8	11 21 33.19	+01 13 32.1	3	28	19.0	21.7	G
Abell 1273									
ii	11 25 56.29	-06 53 59.6	11 25 55.82	-06 53 44.8	16	-25		22.7	G
iii	11 26 12.24	-06 39 38.6	11 25 55.98	-06 54 13.9	15	-162		21.9	G
iiii	11 26 15.07	-06 51 15.6	11 26 11.40	-06 39 20.2	22	-34		18.0	St
			11 26 14.36	-06 51 22.7	13	-124		20.5	G
			11 26 14.77	-06 51 32.5	17	-165		20.3	G
3i/4	11 26 34.62	-06 48 03.8	11 26 15.17	-06 50 56.1	20	4		21.5	St
3ii	11 26 35.87	-06 45 43.7	11 26 35.54	-06 47 32.0	35	23		14.2	16.2
3iii	11 26 36.51	-06 34 01.0	11 26 35.86	-06 45 57.5	14	-179	18.2	20.5	G
6	11 26 44.58	-06 45 00.5	11 26 44.46	-06 45 11.5	11	-171	>19.5	22.6	G
7	11 27 00.35	-06 52 25.7	BF	-06 45 13.7	14	161	>19.5	20.0	St
8i	11 27 24.07	-06 39 38.3	BF						
8ii	11 27 31.93	-06 45 49.5	11 27 31.41	-06 45 51.6	8	-105	19.8	St	
			11 27 32.70	-06 45 36.8	17	42		22.5	G
Abell 1620									
2	12 47 18.17	-01 13 43.4	12 47 17.85	-01 13 35.5	9	-31	>19.5	20.3	E
4	12 47 36.89	-01 20 07.2	12 47 18.54	-01 13 46.5	6	119	19.2	20.2	E
			BF						

Table 5. (*Continued*)

6	12 47 57.22	-01 13 12.7	12 47 56.32	-01 13 01.2	18	-50	20.8	St
7	12 47 59.77	-01 15 30.2	12 47 57.39	-01 13 08.1	5	29	22.0	G
			12 47 58.77	-01 15 19.0	19	-53	19.8	E
			12 47 59.59	-01 15 19.4	11	-14	22.1	G
8	12 48 25.36	-01 12 42.2	12 48 00.43	-01 15 41.5	15	139	21.4	G
			12 48 25.21	-01 12 43.4	3	-118	18.9	E
			12 48 25.23	-01 13 01.3	19	-174	19.5	St
			12 48 25.42	-01 12 28.7	14	4	18.9	St
Abell 1631								
1a/b/c/d	12 49 18.79	-14 54 10.7	12 49 16.95	-14 54 10.2	27	-89	21.7	G
2ii	12 49 22.99	-14 56 23.3	12 49 17.46	-14 54 24.0	23	-125	20.9	G
			12 49 22.57	-14 56 32.2	11	-146	21.7	G
3a/b	12 49 33.12	-15 20 12.7	12 49 24.26	-14 56 01.5	28	40	18.2	St
5	12 49 39.35	-15 02 45.6	12 49 38.28	-15 02 50.9	16	-109	>19.5	G
7	12 49 54.39	-15 12 29.4	12 49 54.08	-15 12 35.1	7	-142	21.7	G
			12 49 54.38	-15 12 20.9	9	-1	21.7	St
8	12 49 56.12	-15 00 32.2	12 49 55.95	-15 00 52.1	20	-173	21.1	E
			12 49 57.35	-15 00 30.0	18	83	21.8	St
9	12 50 00.04	-14 50 02.3	12 50 02.52	-14 57 10.3	6	97	18.0	18.9
10	12 50 02.12	-14 57 09.6	12 50 02.52	-14 57 10.3	6	97	18.0	18.9
11	12 50 05.40	-15 00 17.6	BF					
12	12 50 05.26	-15 07 53.0	BF					
13	12 50 06.90	-15 11 26.1	BF					
15	12 50 12.20	-14 49 57.7	BF					
20i	12 51 05.26	-15 12 54.5	12 51 05.62	-15 12 48.2	8	40	17.6	18.4
20ii	12 51 11.61	-14 52 36.0	BF					
21	12 51 13.29	-15 13 34.7	12 51 12.34	-15 13 42.9	16	-121	20.5	E
22	12 51 15.79	-14 50 08.9	12 51 15.32	-14 50 13.4	8	-123	15.6	15.7
23a/b	12 51 17.04	-14 55 27.9	BF					
24	12 51 22.81	-14 58 17.6	12 51 21.89	-14 58 19.5	13	-98	17.5	18.6
Abell 3528								
3	12 52 23.55	-28 55 04.2	12 52 22.14	-28 55 05.1	19	-93	19.2	E
Abell 1689								
ii	13 07 50.65	-01 10 08.3	13 07 50.82	-01 10 14.8	7	159	21.4	G
2ii/a/b	13 07 53.80	-00 47 23.4	13 07 51.34	-01 10 02.0	12	59	18.3	St

3	13 08 05.53	-01 08 44.9	13 08 05.30	-01 08 47.6	4	-128	>19.5	22.3	G
4i	13 08 11.27	-00 53 17.8	13 08 06.20	-01 08 27.4	20	30	16.6	17.0	St
4ii	13 08 14.31	-00 49 36.1	13 08 11.38	-00 53 15.6	3	37	19.2	21.3	G
4iii	13 08 14.45	-01 13 14.3	BF						
5/6	13 08 21.48	-01 11 26.3	13 08 21.35	-01 11 28.4	3	-137	18.0	18.0	Q
7	13 08 40.64	-01 15 48.2	13 08 42.05	-01 15 42.7	22	75	19.0	20.3	E
8	13 08 40.67	-01 01 44.6	13 08 40.93	-01 01 41.9	5	55	19.0	20.4	G
9	13 08 41.90	-01 17 30.4	13 08 42.07	-01 17 22.4	8	18	17.1	18.5	E
10	13 08 51.51	-01 15 00.8	13 08 51.31	-01 15 20.2	20	-171	11	16.5	St
			13 08 51.68	-01 14 47.1	14	11	16.5	16.3	St
			13 08 51.80	-01 15 13.1	13	161	16.8	16.7	St
			13 08 41.61	-01 01 50.0	15	111	19.2	21.6	St
			13 08 52.69	-01 15 01.2	18	91	>19.5	22.3	G
			13 08 52.25	-01 06 06.8	12	-94	19.4	20.7	G
11	13 08 53.06	-01 06 05.9	13 08 52.82	-01 06 14.2	9	-157	19.4	20.8	G
			13 08 52.85	-01 06 23.8	18	-170	18.5	20.3	E
			13 08 53.56	-01 06 02.1	8	63	>19.5	21.5	G
12	13 08 54.79	-01 05 21.2	13 08 54.72	-01 05 22.3	2	-136	18.0	20.4	E
			13 08 55.02	-01 05 11.1	11	19	>19.5	21.5	G
			13 08 55.46	-01 05 06.3	18	34	19.4	21.3	G
			13 08 55.74	-01 05 23.3	14	98	19.5	21.3	G
			13 08 56.02	-01 05 14.8	20	71	>19.5	21.3	G
13	13 08 55.79	-01 04 33.5	13 08 55.07	-01 04 47.4	18	-142	>19.5	20.8	G
			13 08 55.20	-01 04 33.4	9	-89	17.1	18.6	E
			13 08 55.71	-01 04 47.1	14	-175	17.5	19.0	E
			13 08 55.90	-01 04 35.3	2	137	17.3	18.8	E
			13 08 56.20	-01 04 49.7	17	159	18.0	19.5	E
			13 08 56.49	-01 04 36.1	11	104	19.5	20.5	G
16	13 09 02.68	-01 18 09.4	13 08 56.91	-01 04 27.8	18	71	16.3	17.9	St
			13 09 02.53	-01 18 09.3	2	-87	20.8	21.3	G
			13 09 02.62	-01 18 28.8	19	-177	22.3	22.3	St
			13 09 03.71	-01 18 23.4	21	132			
17	13 09 03.26	-01 17 22.9	BF						
18a/b	13 09 07.96	-01 07 48.1	13 09 08.25	-01 07 31.2	17	14	16.4	18.0	St
19a/b	13 09 09.15	-01 03 32.3	13 09 09.48	-01 07 20.2	36	39	15.0	16.0	St
20	13 09 15.50	-01 12 07.5	13 09 16.47	-01 11 57.5	18	-1	17.5	19.5	E
					55	55	22.6	22.6	G

1.0038

19

A1689-110

0.0815

6

A1689-236

0.1840

6

A1689-227

0.1947

6

A1689-2

6,12

4,6,12

A1689-3

6

A1689-3

Table 5. (Continued)

21	13 09 26.61	-01 19 23.6	BF					
23i	13 09 30.83	-00 58 20.2	BF					
23ii	13 09 40.65	-01 03 16.4	13 09 40.25	-01 03 06.3	12	-31	22.7	G
Abell 1772								
1	13 38 17.76	-10 43 07.5	13 38 17.93	-10 43 16.2	9	164	18.7	21.9
			13 38 18.24	-10 43 27.4	21	160	>19.5	23.0
			13 38 17.00	-10 42 49.1	21	-31	19.0	19.9
2	13 38 20.41	-10 57 13.7	BF					
3	13 38 41.47	-11 05 48.6	BF					
4	13 38 44.59	-10 47 13.8	13 38 44.48	-10 47 14.4	2	-110	21.8	E
5	13 38 52.68	-10 39 44.4	13 38 52.21	-10 39 41.3	8	-66	18.2	20.5
6	13 39 05.95	-10 58 00.2	BF					
8	13 39 55.70	-10 57 15.9	BF					
9a/b	13 40 02.79	-10 54 56.7	BF					
12a/b	13 40 27.07	-10 47 42.2	BF					
Abell 1775								
1	13 38 20.38	26 26 59.4	13 38 20.86	26 26 42.6	18	159	17.2	E
2	13 38 27.92	26 30 31.2	13 38 27.53	26 30 30.0	5	-103	17.4	E
5	13 38 54.63	26 32 09.7	13 38 53.32	26 32 14.8	18	-74	16.8	St
6	13 39 07.55	26 42 36.6	BF					
8	13 39 29.39	26 24 11.0	13 39 28.34	26 23 56.3	20	-136	16.2	St
9	13 39 30.52	26 55 29.5	BF					
11a/b	13 39 31.67	26 53 22.7	13 39 30.70	26 53 36.2	19	-44	18.6	Q?
12	13 39 31.68	26 19 25.0	BF					
14a/b	13 39 44.66	26 19 04.5	13 39 49.09	26 45 47.4	2	4	17.8	G
15	13 39 49.08	26 45 45.4						
16	13 40 01.83	26 28 58.5	13 40 01.07	26 29 15.9	11	-135	19.2	St
			13 40 01.44	26 28 42.6	17	-162	18.3	E
17	13 40 08.66	26 39 18.4	13 40 10.07	26 39 24.5	20	72	19.3	G
18	13 40 09.36	26 34 37.5	13 40 07.52	26 39 19.1	15	-87	16.2	St
			13 40 08.93	26 34 35.9	6	-106	17.8	St
			13 40 07.96	26 34 23.8	23	-126	19.2	St
							36	133930.8+2653

19	13 40 17.38	26 46 06.1	BF									
Abell 1791	13 45 48.03	-25 10 54.2	13 45 47.76	-25 11 04.0	10	-159	20.0	St				
1			13 45 48.02	-25 10 54.7	1	-165	17.4	E				
Abell 1913												
1	14 23 36.55	17 01 27.5	14 23 36.77	17 01 30.2	4	49	19.5	St				
2	14 23 40.86	16 46 59.3	BF									
3i	14 23 43.06	16 58 30.2	14 23 43.27	16 58 34.3	5	36	19.5	St				
3ii	14 23 43.36	17 14 48.1	14 23 42.76	16 58 29.9	4	-94	18.0	G				
				16 58 22.3	10	143	19.6	St				
4	14 23 53.01	16 54 35.3	14 23 42.72	17 14 31.4	19	-151	19.8					
5	14 24 01.45	17 07 51.0	14 24 01.25	17 07 52.8	3	-58	17.4	E				
				17 07 46.6	15	-107	17.8	St				
7	14 24 11.43	17 04 13.8	14 24 11.40	17 04 14.8	1	-23	16.2	E				
				17 04 12.74	19	92	19.2	G				
9	14 24 15.58	16 58 25.1	14 24 16.62	16 58 40.5	21	44	19.8	G				
10	14 24 16.16	16 47 45.8	14 24 15.77	16 58 30.6	6	26	17.2	D				
11	14 24 20.41	16 52 26.0	BF									
12	14 24 23.79	16 56 04.6	14 24 22.94	16 56 13.0	15	-55	19.5	St				
				16 56 10.6	8	42	18.7	St				
13	14 24 30.31	16 48 14.6	14 24 24.17	16 56 04.8	17	89	18.0	G				
17	14 24 56.95	17 10 23.9	14 24 56.93	17 10 25.6	2	-10	16.6	E	0.0949	35	IRAS 14249+1710	
18	14 24 57.37	16 59 03.5	BF									
19	14 24 59.46	17 12 18.1	BF									
20	14 25 01.92	16 49 19.2	BF									
21	14 25 27.20	17 03 13.1	14 25 27.42	17 03 13.8	3	77	19.5	G				
23	14 25 34.76	16 54 32.2	14 25 27.29	17 02 58.9	14	174	19.6	St				
24	14 25 38.82	17 06 42.6	14 25 37.95	17 06 37.1	14	-114	18.8	St				
Abell 2009												
1	14 57 20.77	21 21 07.2	14 57 21.50	21 21 14.1	12	56	17.2	St				
				21 21 06.2	10	-96	19.3	G				
				21 21 04.1	3	-156	17.1	E				

Table 5. (Continued)

2	14 57 24.79	21 24 58.2	14 57 25.58	21 25 12.5	18	38	18.9	G
3	14 57 36.45	21 36 41.7	14 57 35.79	21 36 52.9	14	-39	17.6	E
4	14 57 36.57	21 24 42.0	14 57 36.63	21 36 50.8	9	15	16.5	St
5	14 57 39.01	21 32 38.4	BF					
6	14 57 44.60	21 41 26.5	BF					
7	14 57 48.00	21 51 06.8	14 57 48.01	21 50 50.0	17	180	18.1	G
8	14 57 49.35	21 42 16.9	14 57 49.47	21 42 19.2	3	36	18.3	G
9	14 57 49.51	21 42 55.2	BF					
11	14 58 00.84	21 45 34.8	BF					
15	14 58 07.20	21 43 12.9	BF					
17	14 58 19.43	21 44 13.2	BF					
18	14 58 40.88	21 23 10.5	14 58 39.99	21 22 56.4	19	-139	17.2	St
19	14 58 52.86	21 45 31.9	14 58 53.23	21 45 21.4	12	154	18.8	St
22	14 59 07.55	21 36 27.1	14 59 07.46	21 36 49.6	23	-3	18.6	G
23ia/b	14 59 07.66	21 19 20.8	14 59 08.42	21 19 36.8	19	34	19.2	G
			14 59 07.38	21 19 21.8	4	-76	17.2	St
23ii	14 59 09.87	21 47 12.7	14 59 09.38	21 47 20.9	11	-40	16.2	St
24	14 59 11.09	21 18 53.6	14 59 11.39	21 18 59.0	7	38	18.4	G
26	14 59 15.09	21 36 08.2	14 59 15.16	21 36 08.7	1	63	18.0	E
27	14 59 23.01	21 46 44.2	14 59 22.21	21 46 53.9	15	49	19.7	G
Abell 2029	15 08 29.71	05 55 09.5	15 08 29.47	05 55 26.4	17	-12	18.2	St
3			15 08 29.32	05 55 09.9	6	-86	18.0	18
4	15 08 31.71	06 00 35.9	15 08 31.80	06 00 38.1	3	31	19.2	G
5	15 08 37.61	05 52 41.0	15 08 37.65	05 52 40.4	1	135	16.6	St
			15 08 36.63	05 52 34.7	16	-113	18.6	G
Abell 2052	No sources with 1.5 GHz flux < 20 mJy							
Zw 1518.8	15 18 21.45	08 08 15.1	BF					
2	15 19 01.41	07 49 18.8	BF					
5	15 19 15.72	07 55 03.0	BF					
9	15 19 16.27	07 40 01.4	BF					
10								

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13ab	15 19 41.87	07 45 13.4	BF						
14	15 19 46.74	07 56 02.1	BF						
15	15 19 51.54	07 58 21.9	15 19 52.18	07 58 25.3	10	70	17.3		St
16ab	15 19 52.16	08 09 06.8	BF						
17	15 19 54.93	07 54 18.1	BF						
18	15 19 56.17	08 11 00.1	15 19 55.37	08 11 15.0	19	-39	18.4		St
20	15 19 57.04	07 48 47.3	15 19 56.87	08 11 08.7	13	50	18.4		St
22	15 20 03.55	08 03 13.4	15 19 57.25	07 48 45.9	3	114	15.7	E	
23	15 20 27.55	07 48 44.5	15 20 03.33	08 03 12.2	3	-110	15.6	E	
			BF						
Abell 2082									
1	15 28 08.78	.03 39 52.9	15 28 09.15	03 40 06.0	14	23	15.9	E	
			15 28 08.47	03 39 49.8	6	-124	15.5	E	
2	15 28 17.42	03 32 01.2	BF						
3ab	15 28 19.61	03 42 18.8	15 28 20.03	03 42 24.8	9	46	18.3	G	
			15 28 19.35	03 42 16.3	5	-123	16.0	E	
			15 28 19.17	03 42 13.6	8	-128	17.2	St	
			15 28 19.96	03 42 01.0	19	164	17.8	G	
4	15 28 30.36	03 35 06.6	BF						
5	15 28 36.46	03 49 01.8	BF						
7	15 28 49.23	03 51 32.8	15 28 48.81	03 51 20.2	14	-153	19.5	G	
9ii	15 28 56.68	03 28 00.8	BF						
			15 28 57.22	03 31 12.7	BF				
11	15 28 58.36	03 44 59.6	15 28 58.42	03 45 00.1	1	61	16.0	D	
14	15 29 19.25	03 49 09.6	15 29 18.41	03 49 18.8	16	-54	19.2	St	
			15 29 19.63	03 48 53.0	18	161	18.6	G	
15	15 29 25.15	03 39 26.4	BF						
16	15 29 29.46	03 43 29.2	BF						
17	15 29 30.77	03 39 55.6	15 29 30.64	03 40 15.2	20	-6	18.5	St	
			15 29 30.60	03 39 34.2	22	-173	17.7	St	
19ab	15 29 42.41	03 41 36.0	15 29 43.34	03 41 41.5	15	68	16.4	St	
Abell 2091									
1ia/b	15 30 40.28	10 11 17.0	15 30 41.06	10 11 18.8	12	81	17.0		
1ii/b	15 31 16.39	10 35 35.2	BF						
2	15 31 24.91	10 24 34.6	BF						
3	15 31 27.33	10 09 17.4	15 31 27.69	10 09 35.4	19	16	18.2	E	
			15 31 27.91	10 09 03.7	16	148	18.8	G	

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Table 5. (*Continued*)

4	15 31 41.85	10 08 27.2	BF								
5	15 31 43.53	10 29 27.0	15 31 44.24	10 29 08.0	22	151	19.2	G			
			15 31 44.68	10 29 17.4	19	120	19.0	St			
7a/b	15 31 57.84	10 21 52.6	15 31 57.94	10 21 53.1	2	71	16.9	E			
9	15 32 01.90	10 29 20.2	BF	10 21 42.9	16	-126	18.9	G			
10	15 32 08.28	10 11 20.2	15 32 07.99	10 11 32.5	13	-19	18.2	G			
11	15 32 12.62	10 19 48.3	BF								
12	15 32 18.09	10 27 57.8	15 32 18.14	10 27 58.0	1	75	15.1	DB			
			15 32 18.26	10 28 06.5	9	16	17.8	G			
			15 32 18.42	10 28 18.4	21	13	16.2	St			
13	15 32 24.91	10 10 52.8	BF	10 27 34.2	25	158	18.8	G			
15	15 32 37.30	10 24 03.7	BF								
16	15 32 38.43	10 31 46.5	15 32 38.64	10 31 46.6	3	88	19.4	G			
17	15 32 53.31	10 29 15.7	15 32 54.18	10 29 02.2	19	136	18.0	G			
18	15 32 55.16	10 28 31.6	BF								
19	15 32 56.87	10 28 01.1	BF								
Abell 2094											
1	15 33 00.66	-01 42 36.4	15 33 00.35	-01 42 48.5	13	-159	16.7	18.1	St		
4	15 33 41.39	-01 50 13.2	BF								
6	15 34 03.02	-01 50 03.6	15 34 03.52	-01 50 02.0	8	78	16.2	18.4	St		
7	15 34 06.20	-01 46 54.1	15 34 07.26	-01 47 03.3	18	120	19.5	21.6	G		
8	15 34 07.46	-01 38 59.3	BF	15 34 06.36	-01 46 54.1	2	90	19.0	23.0	G	
10a/b	15 34 10.49	-01 49 24.9	BF								
11	15 34 13.03	-01 45 10.5	15 34 14.50	-01 45 10.9	22	91	>19.5	22.6	G		
12a/b	15 34 17.83	-02 01 55.2	15 34 16.02	-02 02 27.1	42	-140	17.5	20.4	E		
			15 34 16.45	-02 02 02.7	22	-110	>19.5	22.7	G		
13	15 34 24.51	-02 06 34.5	15 34 25.27	-02 06 21.7	17	5	18.2	20.1	E		
14	15 34 29.49	-01 40 07.4	15 34 29.60	-01 40 10.2	3	149	15.5	16.3	S0		
15	15 34 36.42	-01 39 47.8	15 34 29.15	-01 40 15.3	9	-147	17.0	St			
16	15 34 38.32	-01 59 47.2	BF	-01 39 47.5	1	56	17.6	21.0	E		
17	15 34 40.42	-01 58 47.6	15 34 40.88	-01 58 44.2	8	64	16.1	16.5	St		

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Table 5. (Continued)

10	16 04 27.35	18 17 39.4	16 04 19.90	18 36 43.6	14	91	16.4	St
13	16 04 42.60	18 10 01.6	16 04 26.60	18 17 47.6	13	-52	19.4	G
14	16 04 51.89	18 08 16.9	16 04 51.78	18 08 19.8	3	-28	18.6	E
			BF					
15	16 04 57.23	18 22 42.4	16 04 51.57	18 08 28.6	13	-21	19.5	St
17a/b	16 05 17.32	18 05 01.9	16 05 16.28	18 04 38.6	28	-148	17.3	E
			BF					
18	16 05 24.43	18 36 39.1	16 05 24.41	18 36 43.9	5	-3	15.5	E
			BF					
Abell 2249								
1/2	17 07 23.87	34 20 10.1	BF					
3i	17 07 42.59	34 29 16.9	17 07 42.93	34 29 20.4	5	50	13.8	E
			BF					
4a/b	17 07 58.34	34 12 43.4	17 07 41.44	34 29 12.3	15	-108	20.0	St
5	17 08 10.55	34 34 21.2	17 08 10.92	34 34 21.3	5	89	16.3	E
			BF					
7	17 08 52.69	34 25 50.1	17 08 53.21	34 25 49.5	6	95	15.5	E
9	17 09 22.76	34 25 46.8	BF					
Abell 2354								
1	21 31 58.06	-15 18 54.0	BF					
2	21 32 24.06	-15 20 22.3	21 32 24.76	-15 20 39.6	20	150	18.6	19.0
3	21 32 33.77	-15 09 50.1	21 32 33.34	-15 09 48.6	6	-76	17.5	19.5
			BF					
5a/b	21 32 50.76	-15 06 40.6	21 32 34.00	-15 09 40.8	10	20	18.0	20.3
			BF					
7	21 33 00.23	-15 13 43.2	21 32 49.86	-15 06 22.3	22	-35	18.2	20.6
			BF					
10a/b	21 33 11.82	-15 14 12.4	21 33 12.52	-15 14 26.7	18	145	17.3	17.7
11a/b	21 33 13.08	-15 08 56.4	21 33 13.67	-15 08 28.2	29	17	19.5	20.6
			BF					
12	21 33 17.62	-14 59 10.9	21 33 18.13	-15 08 53.5	11	75	14.5	12.5
14	21 33 43.68	-15 20 43.1	BF	-14 59 12.0	7	98	16.0	15.2
			BF					
								GSC 05799-00563

	15	21 33 53.33	-15 10 38.4	21 33 54.59	-15 10 40.6	18	97	19 0	DB
Abell 2396									
1	21 52 46.26	12 20 40.5	BF						
2	21 52 49.84	12 19 51.5	21 52 48.86	12 19 52.2	14	-87	16.4		St
4	21 53 06.60	12 18 30.7	21 53 07.66	12 18 33.8	16	79	18.8		G
7	21 53 17.05	12 05 18.2	BF	12 18 32.9	9	-75	17.8		St
9	21 53 26.53	12 12 05.6	BF	12 18 11.7	28	-132	19.0		G
10	21 53 56.76	12 12 24.5	BF						
12	21 54 12.04	12 19 30.4	21 54 12.73	12 19 29.9	10	93	19.2		G
13	21 54 18.82	12 17 44.9	BF	12 19 22.8	9	-144	19.5		G
Abell 2399									
1/3	21 53 07.32	-08 37 30.1	21 53 05.11	-08 37 13.3	37	-63	16.3	16.4	St
2	21 53 06.28	-08 19 38.7	21 53 09.27	-08 37 28.2	3	51	>19.5	22.2	St
4	21 53 14.30	-08 34 44.1	21 53 05.51	-08 19 33.6	13	-66	16.3	16.0	St
7	21 54 05.00	-08 30 38.0	BF	-08 19 38.8	18	90	19.7		
9	21 54 17.79	-08 40 45.4	BF						
11	21 55 09.00	-08 30 05.4	21 55 08.80	-08 30 02.8	4	-49	21.7		G
Abell 2443									
1a/b	22 22 37.53	17 10 08.1	BF						
2a/b	22 22 48.24	16 59 44.9	22 22 47.66	16 59 19.1	27	-162	17.0		St
4	22 22 52.47	16 47 48.5	BF						
5	22 23 10.11	16 50 37.3	22 23 10.58	16 50 34.1	7	115	17.2		St
6	22 23 10.33	17 16 28.8	22 23 10.29	17 16 10.8	18	-178	18.1		E
8	22 23 51.00	17 03 34.8	22 23 37.19	17 03 36.2	3	63	18.0		G
10	22 23 57.97	16 57 17.9	22 23 38.52	16 57 29.6	14	34	18.0		G
13	22 23 45.02	17 20 29.7	22 23 45.06	17 20 33.8	4	8	17.8		G
14	22 23 56.32	16 54 26.5	BF						
15	22 23 59.11	17 24 47.9	22 23 59.45	17 25 09.7	22	13	16.3		St
			22 23 58.81	17 24 59.2	12	-21	15.6		St
			22 23 59.69	17 24 44.2	9	114	16.1		

Table 5. (Continued)

16	22 24 01.44	17 19 46.8	BF	17 11 43.0	12	144	16.8	St
17	22 24 06.48	17 11 52.5	22 24 06.97	17 11 42.7	12	-145	15.5	St
			22 24 06.00	17 11 51.5	3	112	18.2	G
18	22 24 09.45	17 21 21.5	BF	17 00 12.7	17	-58	19.7	St
19	22 24 11.53	17 00 03.7	22 24 10.53	16 59 49.8	15	160	19.6	St
20	22 24 11.80	16 47 45.3	BF	17 03 24.7	13	-93	17.5	St
21	22 24 16.78	17 17 28.7	BF	17 03 06.1	20	163	16.5	St
22	22 24 21.10	16 58 23.0	BF					
23	22 24 31.41	17 03 25.4	22 24 30.48	17 03 24.7				
			22 24 31.82	17 03 06.1				
Abell 2456								
1	22 31 20.30	-15 29 18.3	22 31 19.63	-15 29 22.0	10	-111	17.7	20.8
2	22 31 28.93	-15 29 02.3	22 31 28.55	-15 29 01.3	6	-80	>19.5	20.9
3	22 31 32.43	-15 19 24.3	22 31 32.02	-15 19 21.2	7	-62	18.8	22.3
4	22 31 38.64	-15 29 56.2	22 31 39.82	-15 30 01.8	18	108	17.3	19.5
5	22 31 55.54	-15 24 08.9	22 31 54.84	-15 24 25.5	19	-149	18.0	19.7
6a/b	22 32 05.27	-15 39 31.8	BF					
7	22 32 10.98	-15 37 28.7	22 32 10.67	-15 37 19.3	10	-25	18.0	21.7
8	22 32 18.14	-15 27 15.5	22 32 16.91	-15 27 07.0	20	-64	17.5	19.0
			22 32 18.57	-15 27 03.0	14	26	19.6	21.2
9	22 32 18.54	-15 42 18.5	BF					
10	22 32 19.21	-15 34 33.6	22 32 18.05	-15 34 41.9	19	-116	>19.6	21.1
			22 32 19.91	-15 34 33.5	10	89	16.1	16.5
11	22 32 20.68	-15 46 37.8	BF					
12	22 32 21.71	-15 43 55.6	BF					
13iii/b	22 32 32.83	-15 20 08.2	22 32 33.05	-15 20 20.2	12	165	18.4	St
14i	22 32 33.41	-15 51 02.7	22 32 34.54	-15 50 52.0	19	57	15.0	St
15	22 32 37.13	-15 51 28.5	BF					GSC 06386-01177
17	22 32 54.92	-15 28 12.3	22 32 54.95	-15 28 12.6	1	125	13.6	14.7
19	22 33 17.73	-15 45 08.4	BF					D 0.0217
20	22 33 19.35	-15 20 05.5	22 33 18.94	-15 20 10.9	8	-132	20.1	E
21	22 33 27.83	-15 21 25.4	22 33 27.54	-15 21 33.4	9	-152	16.5	St
Abell 2457								
1ia/b	22 33 12.60	01 16 16.6	22 33 10.94	01 16 26.9	27	-68	14.7	St
			22 33 11.87	01 16 00.4	20	-146	19.8	St

Abell 2575		Abell 2593	
ii	22 33 12.66 22 33 33.39	01 12 45.5 01 17 57.2	22 33 11.94 22 33 32.25
ii	22 33 52.12 22 34 00.08	01 05 03.2 00 55 34.2	22 33 33.67 22 33 50.91
ii	22 34 07.71 22 34 15.91	01 07 44.1 01 03 59.3	BF BF
ii	22 34 19.28	01 14 00.4	22 34 19.27 BF
			01 14 00.8
		0	21.8
		E	
Abell 2575			
ii	23 16 19.85 23 16 24.08	-22 06 59.9 -22 20 48.6	BF BF
ii/a/b	23 16 28.69	-22 08 37.1	23 16 28.12 23 16 28.40
ii			-22 08 18.4 -22 08 31.5
ii	23 16 54.19 23 17 03.17	-22 07 52.2 -22 19 23.1	23 16 30.03 23 17 04.73
ii			-22 08 42.3 -22 08 42.3
ii	23 17 32.71 23 17 35.51	-22 36 58.7 -22 23 32.0	BF BF
ii	23 17 43.69	-22 39 03.9	23 17 42.80 23 17 43.43
ii			-22 39 16.0 -22 39 16.7
ii	23 18 01.92 23 18 04.23	-22 24 04.9 -22 15 19.8	23 18 01.25 23 18 04.78
ii	23 18 28.30	-22 12 31.6	23 18 28.60
ii	23 18 31.25	-22 13 31.5	23 18 32.23
			-22 13 44.2
			19
			133
			20.1
			St
Abell 2593			
ii	23 21 00.60 23 21 03.96	14 03 32.1 14 17 02.9	23 21 00.62 23 21 02.82
ii			14 16 54.0 14 16 46.0
ii	23 21 40.08	14 12 41.0	23 21 41.21 23 21 40.52
ii	23 21 49.09	14 22 20.4	23 21 49.39 14 22 21.4
ii			4
			77
			13.5
			D
			0.0419
			16,21,28
			NGC 7649

Table 5. (Continued)

		23 21 49.51	14 12 48.3	23 21 49.39	14 22 02.7	18	166	16.1	St
4ii	5	23 21 52.60	14 19 07.4	BF					
6	6	23 21 56.09	14 23 24.8	BF					
7a/b	7	23 22 00.87	14 35 28.5	BF					
8ii	8	23 22 03.55	14 29 31.1	23 22 03.46	14 29 13.5	18	-176	19.4	St
9ii	9	23 22 08.10	14 34 19.8	BF					
10ii	10	23 22 08.16	14 28 12.5	23 22 07.74	14 28 25.9	15	-24	16.2	St
11ii	11	23 22 25.52	14 39 23.2	BF	23 22 07.26	14 28 01.6	17	-130	15.0
11iii	12	23 22 29.84	14 15 25.2	23 22 29.27	14 15 34.0	12	-43	17.6	E
12i	13	23 22 43.80	14 35 38.9	23 22 28.63	14 15 32.0	19	-69	16.3	St
12ii	14	23 22 45.93	14 20 11.6	23 22 30.48	14 15 13.4	15	142	17.6	E
13	15	23 22 49.66	14 09 33.5	23 22 43.20	14 35 51.6	13	-5	17.5	St
				BF	23 22 43.20	14 35 22.4	19	-152	18.3
				BF					St
Abell 2622									
2	2	23 31 28.24	27 05 47.0	23 31 27.79	27 05 46.3	6	-97	17.8	E
3	3	23 31 28.55	27 06 47.9	23 31 28.94	27 06 48.9	5	79	18.6	E
4	4	23 31 39.42	27 15 25.1	BF					
5	5	23 32 21.32	27 07 17.1	BF					
6	6	23 32 21.91	27 06 14.7	23 32 22.59	27 06 19.8	10	61	17.5	St
7	7	23 32 24.04	27 04 34.0	23 32 22.09	27 06 06.9	8	163	18.5	G
8	8	23 32 31.46	27 09 23.4	23 32 23.92	27 04 32.7	2	-129	15.7	S0
11a/b	12	23 32 33.44	27 16 49.5	BF	23 32 23.54	27 04 26.6	10	-138	16.6
14a/b	13	23 32 45.29	27 11 12.6	23 32 46.57	27 10 58.2	22	130	19.4	St
				BF	23 32 44.99	27 10 56.4	17	-106	18.3
				BF	23 32 44.10	27 10 56.2	23	-136	19.5
15	15	23 32 47.22	27 20 47.0	23 32 46.41	27 20 57.4	15	-46	17.4	St
16	16	23 32 54.65	27 16 26.6	23 32 48.03	27 20 53.4	13	59	18.3	E
17	17	23 32 59.22	26 48 29.8	23 33 00.21	27 16 22.9	17	-103	18.0	St
18	18	23 33 16.64	26 56 13.0	BF	26 48 27.6	13	99	15.9	St
19	19	23 33 19.48	27 07 44.9	BF					

GSC 02253-0307

Zw331.214

20		23 33 21.26	27 06 48.2									
21		23 33 30.13	27 04 46.5									
				BF								
					BF							
Abell 2626	1	23 32 41.17	20 46 26.0									
	2	23 32 51.00	20 51 38.7	BF								
	3	23 33 22.83	21 04 15.8	23 33 22.08								
	4	23 33 23.38	20 48 12.6	BF								
	8	23 33 45.27	20 49 38.1	23 33 45.26	20 49 45.3	7	-1	17.5				
	9	23 33 47.77	21 02 07.0	BF								
	10	23 33 54.70	20 52 33.7	23 33 54.03	20 52 25.2	13	-132	14.5				
	13	23 34 06.08	20 46 11.2	BF.								
	14	23 34 08.63	20 49 31.0	23 34 08.68	20 49 29.7	1	152	14.0	E	0.0589	31	Zw455.028
Abell 2657	16	23 34 33.45	20 55 04.3	23 34 07.96	20 49 13.2	20	-152	19.0	G			
	18	23 34 48.82	20 35 49.2	BF	23 34 33.02	20 55 15.3	12	-29	18.8	G		
	1	23 43 25.62	08 29 29.3	23 43 26.31	08 29 30.2	10	85	17.5	E			
	2a/b	23 43 26.68	08 27 50.0	BF								
	6	23 44 08.63	08 41 35.6	BF								
	7	23 44 16.62	08 35 16.3	23 44 16.42	08 35 15.7	3	-101	16.3	St			
				23 44 16.29	08 35 11.2	7	-136	18.0	E			
Abell 4038	2	23 44 12.51	-28 32 00.5	23 44 12.26	-28 32 07.6	8	-155	17.5	St			
	3	23 44 22.84	-28 07 58.9	BF								
	5	23 44 35.72	-28 17 03.8	BF								
	6i	23 44 40.58	-28 26 22.5	23 44 39.42	-28 26 27.0	16	-106	19.1	St			
	6ii	23 44 40.69	-28 08 10.8	23 44 40.43	-28 26 06.2	16	-7	19.7	St			
	6iii	23 44 40.74	-28 34 04.8	23 44 40.91	-28 08 04.3	7	24	21.1	St			
				23 44 41.34	-28 08 20.5	13	139	21.0	St			
				23 44 40.41	-28 33 47.1	18	-14	20.5	G			
				23 44 40.57	-28 34 13.2	9	-165	19.1	E			
				23 44 40.66	-28 34 07.6	3	-159	20.0	E			
				23 44 41.07	-28 34 22.1	18	166	20.8	G			
				23 44 41.30	-28 34 00.6	8	60	20.8	G			

Table 5. (Continued)

7	23 44 52.42	-28 24 52.1	23 44 41.84	-28 33 56.6	17	60		21.5	G								
			23 44 52.42	-28 24 52.1	0			14.5	eD								
10	23 45 07.34	-28 24 13.1	23 44 52.62	-28 25 07.4	15	170		18.0	E								
			23 45 07.27	-28 24 04.8	8			20.8	G								
12	23 45 20.00	-28 10 22.7	23 45 06.25	-28 24 13.6	14	-92		15.6	E								
			BF					0.0278								10,11	
13a/b	23 45 21.59	-28 16 41.4	23 45 21.77	-28 16 42.2	3			109									
			23 45 23.83	-28 16 48.4	30	103		18.6	St								
14	23 45 35.96	-28 15 53.3	BF														
15	23 45 37.48	-28 09 48.1	23 45 36.42	-28 09 48.2	14			-90									
			23 45 37.88	-28 09 32.4	17			17								21.2	G
16a/b	23 45 43.27	-28 30 20.5	23 45 42.77	-28 30 29.7	11			19								20.8	G
			23 45 44.68	-28 30 36.3	24	130		-144								19.1	E
17i	23 45 54.94	-28 13 35.7	BF													0.0275	1,7,11
17ii	23 46 01.96	-28 41 13.6	BF														
19	23 46 20.12	-28 39 25.4	BF														
Abell 2670																	
i	23 49 17.41	-11 09 01.6	23 49 16.85	-11 09 12.1	13			-142								20.3	E
			23 49 17.50	-11 09 22.0	20			176								19.2	E
ii	23 49 28.78	-10 51 10.4	23 49 28.83	-10 51 23.7	13			177								21.1	G
2	23 49 36.49	-11 03 33.0	BF														
3	23 49 43.39	-10 48 05.9	23 49 43.49	-10 48 15.0	9			171									
4	23 50 02.61	-10 50 55.8	BF														
5	23 50 07.85	-10 55 18.8	BF														
6	23 50 21.92	-10 45 18.8	BF														
8	23 50 27.20	-10 45 10.7	BF														
9	23 50 31.35	-11 04 47.8	23 50 31.93	-11 04 48.7	9			96								17.8	E
10	23 50 33.23	-11 10 21.6	BF													19.4	
12	23 50 34.59	-11 00 55.8	23 50 34.50	-11 00 58.4	3			-153								16.8	E
			23 50 34.90	-11 01 07.5	13			159								17.9	
13	23 50 40.03	-10 57 46.6	23 50 39.93	-10 57 48.4	2			-141								18.8	E
14	23 51 08.96	-10 56 26.2	BF													19.4	
15	23 51 37.05	-10 46 48.1	23 51 36.14	-10 46 32.8	20	-41										17.7	E
															0.0748	33	

Column Headings

- Column
 1 The cluster field and source number as listed by SPS89. See Section 2a for explanation of Roman numerals.
 2,3 The B1950 right ascension and declination of the source centroid at 1.5 GHz.
 4,5 The B1950 right ascensions and declinations of nearby optical objects.
 7,8 The angular separation and position angle (positive from north through east) of the optical object relative to the 1.5 GHz position.
 9,10 Our estimates of apparent magnitude from the Palomar red plate and SERC J-plate respectively.
 11 Our estimate of the morphological class of the optical object. Refer to Section 3 for the meanings of abbreviations.
 12 The average redshift obtained from the references in column 13.
 13 References for redshifts.
 14 Other catalogue names.

References for redshift

1. Green, Godwin and Peach (1988)
2. Malumuth et al. (1992)
3. Proust et al. (1987)
4. Schneider, Gunn and Hoesel (1983)
5. Beers et al. (1991)
6. Teague, Carter and Gray (1990)
7. Lucey and Carter (1988)
8. Dressler and Shectman (1988)
9. Merrifield and Kent (1991)
10. Maccacaro et al. (1977)
11. Chincarini et al. (1978)
12. Valentijn and Casertano (1988)
13. Quintana and Ramirez (1990)
14. Quintana et al. (1985)
15. Tarenghi et al. (1979)
16. Bothun and Schombert (1990)
17. Beers et al. (1983)
18. Bower et al. (1988)
19. Hewett et al. (1991)
20. Coziol et al. (1993)
21. Colless et al. (1993)
22. Zabludoff, Huchra and Geller (1990)
23. Owen, Ledlow and Keel (1995)
24. Hanway (1988)
25. Reynolds (1986)
26. Wegner et al. (1993)
27. Strauss et al. (1992)
28. Postman and Lauer (1995)
29. Scodellario et al. (1995)
30. Giovanelli and Haynes (1993)
31. Tago (1995)
32. Lauberts and Valentijn (1989)
33. Sharples et al. (1988)
34. de Vaucouleurs et al. (1991)
35. Huchra et al. (1995)
36. Crampton et al. (1988)

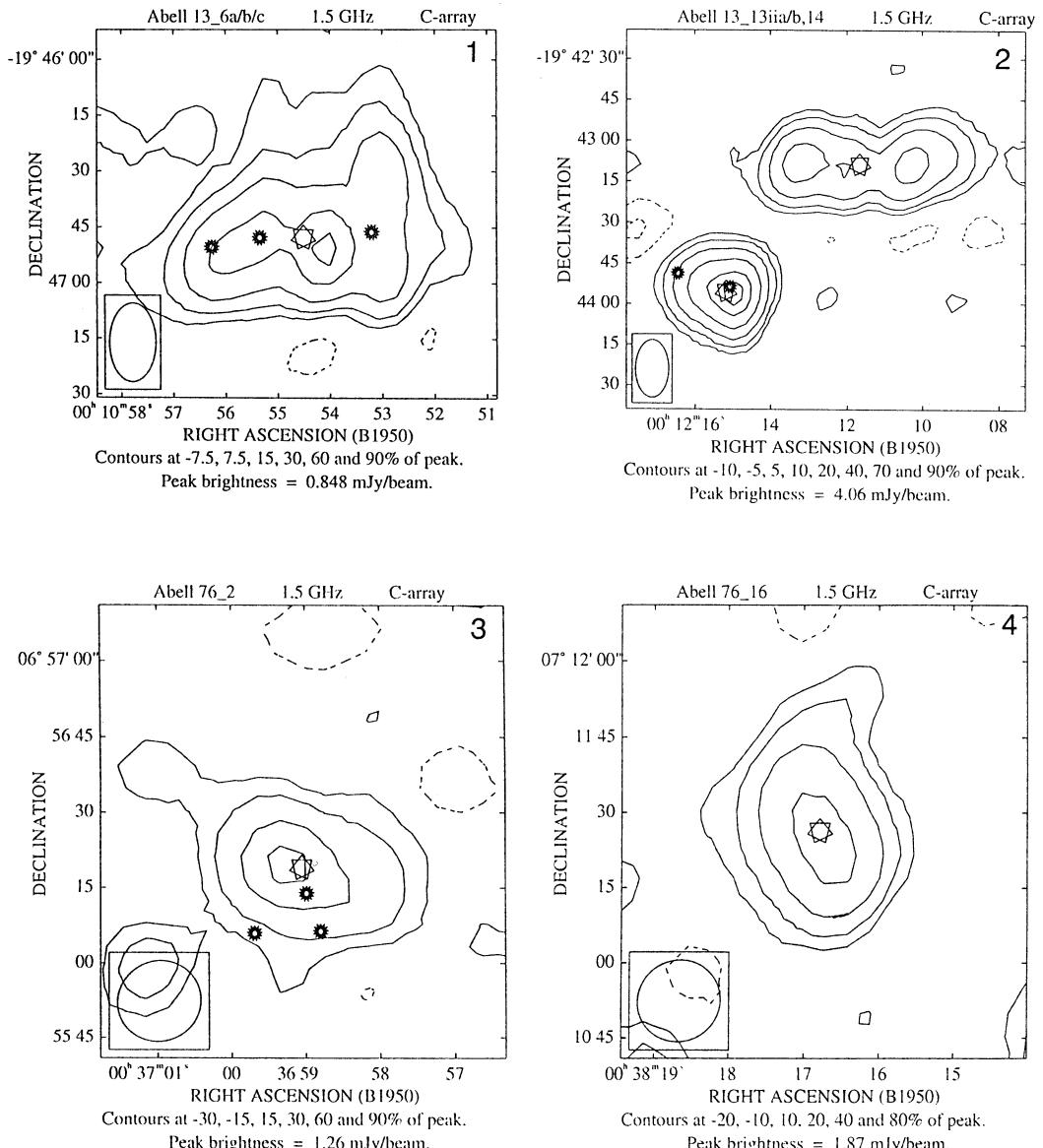
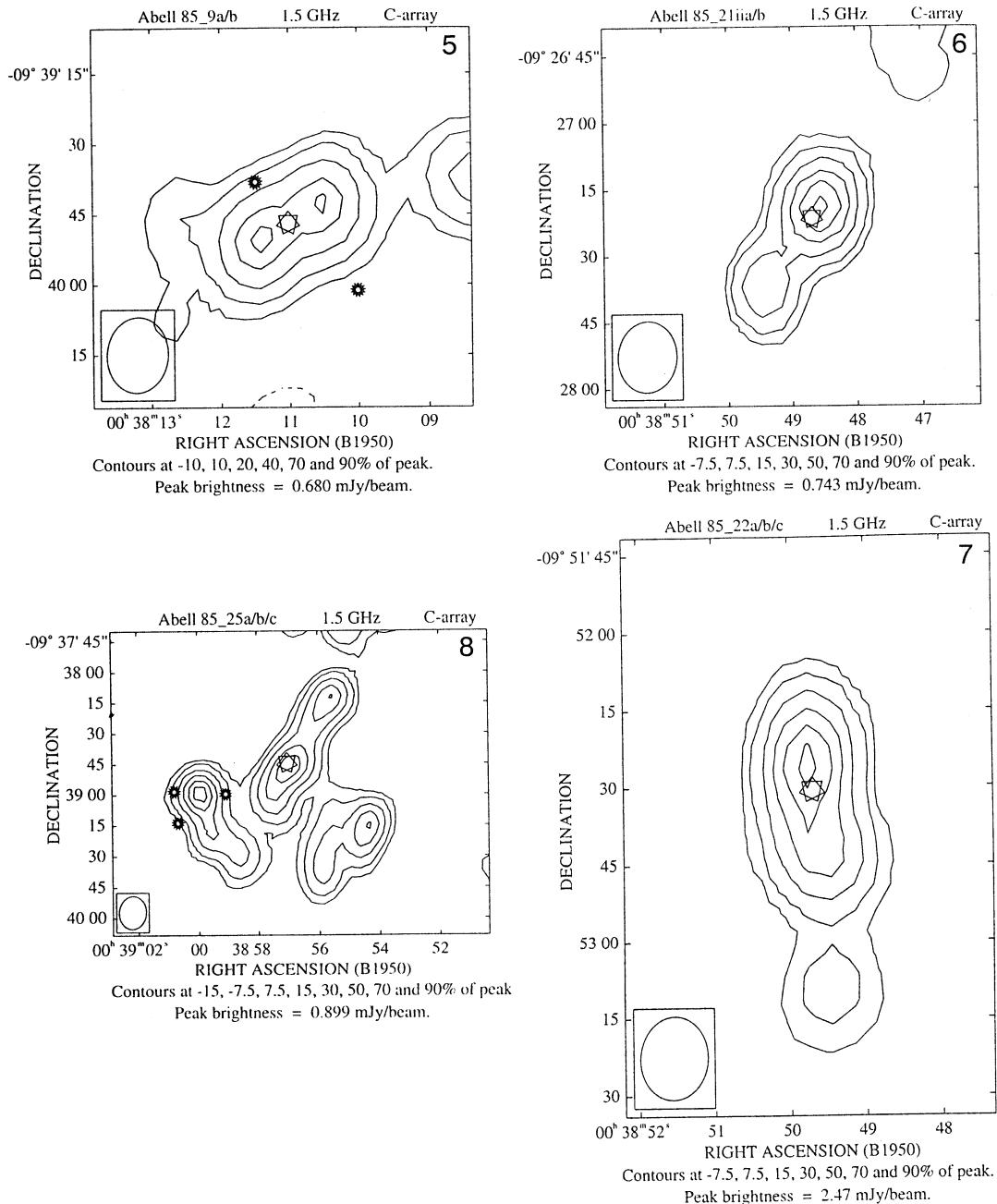


Fig. 1. Contour maps of the more extended sources in the sample. The number in the upper right corner cross-references the map to its derived parameters in Tables 2, 3 and 4. The source number (see Tables 2, 3 and 4), observing frequency and VLA configuration appear at the top of the map. The synthesised beam (FWHP) is shown in the box at the lower left corner. The rms noise level applicable to each map may be obtained from columns 7 and 8 in Table 1. Radio positions (Table 5) are shown with open 7-pointed stars and optical positions of potential identifications (Table 5) with smaller, partly filled 13-pointed stars.

**Fig. 1. (Continued)**

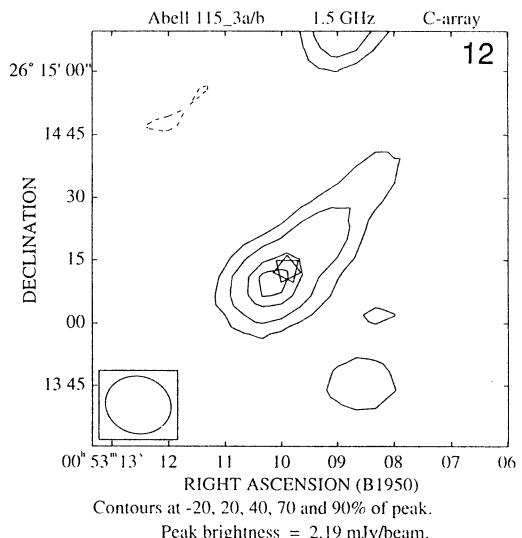
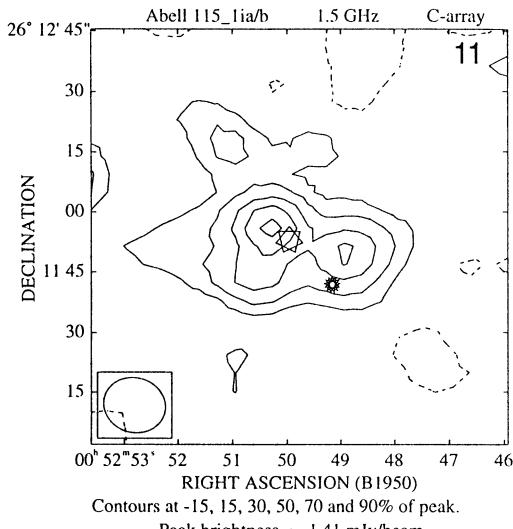
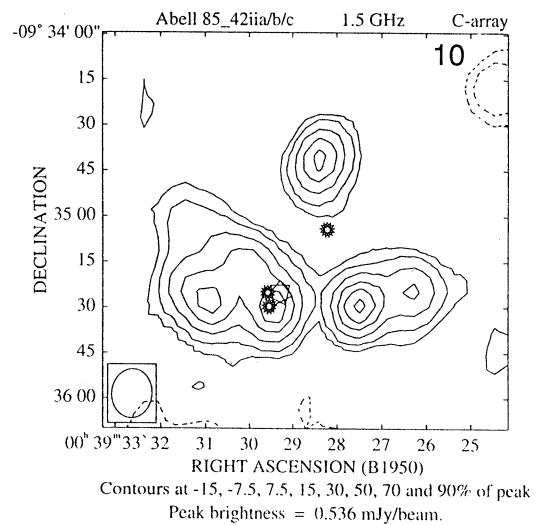
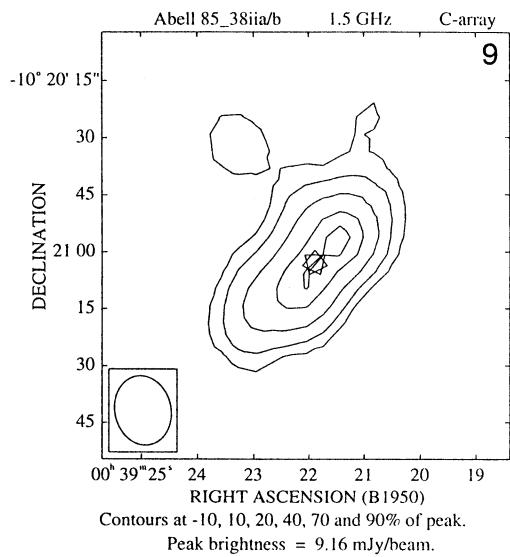
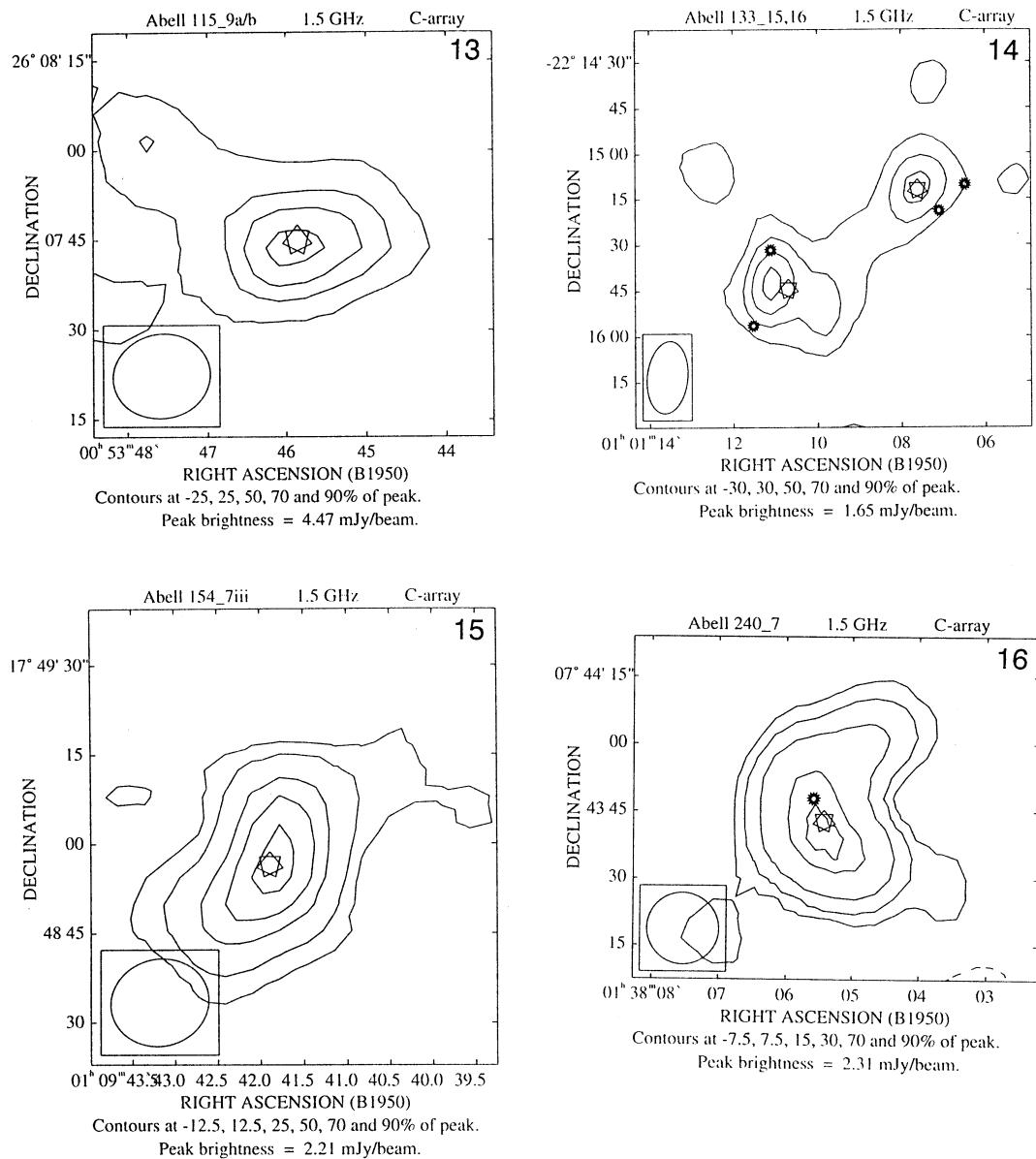
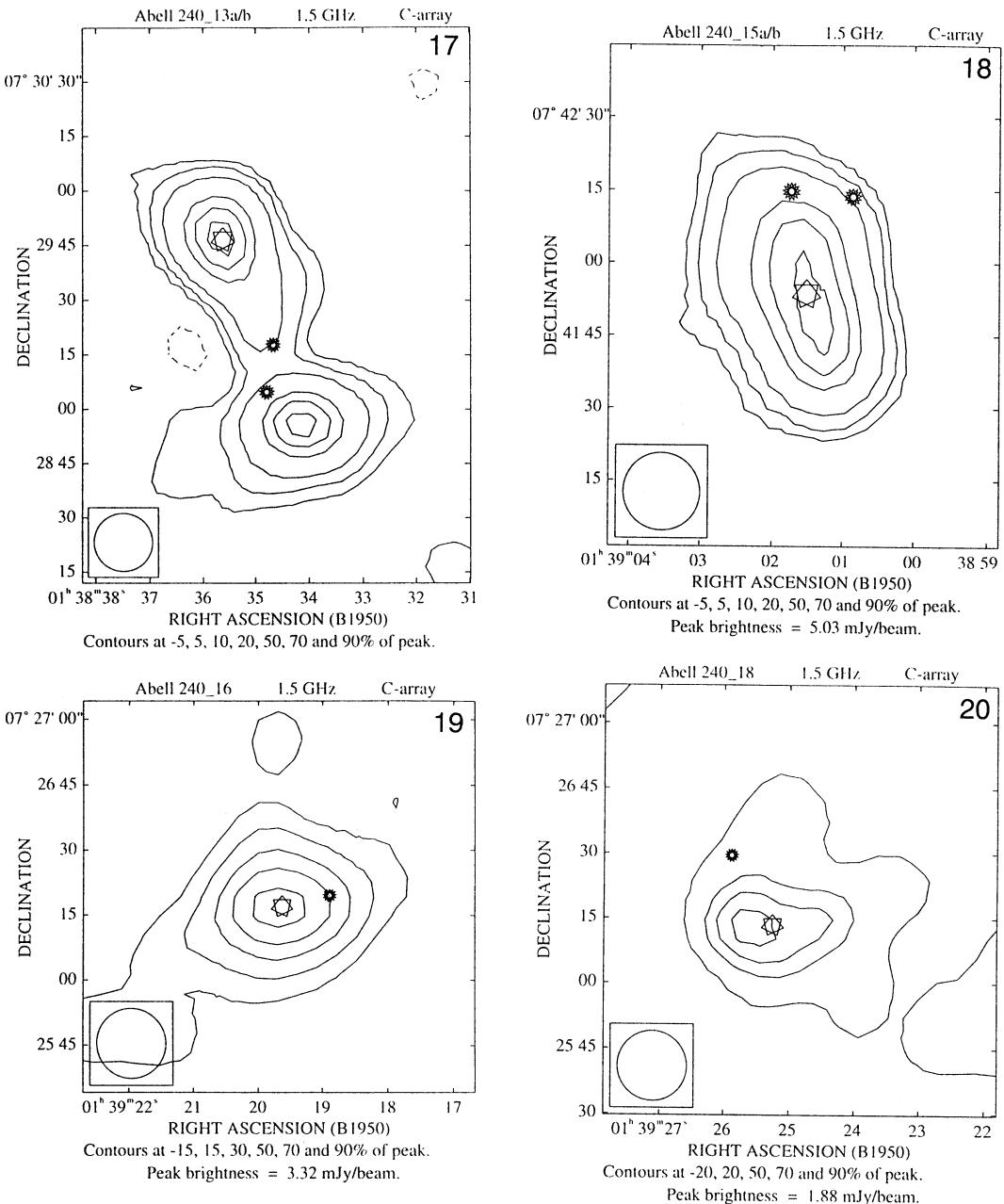
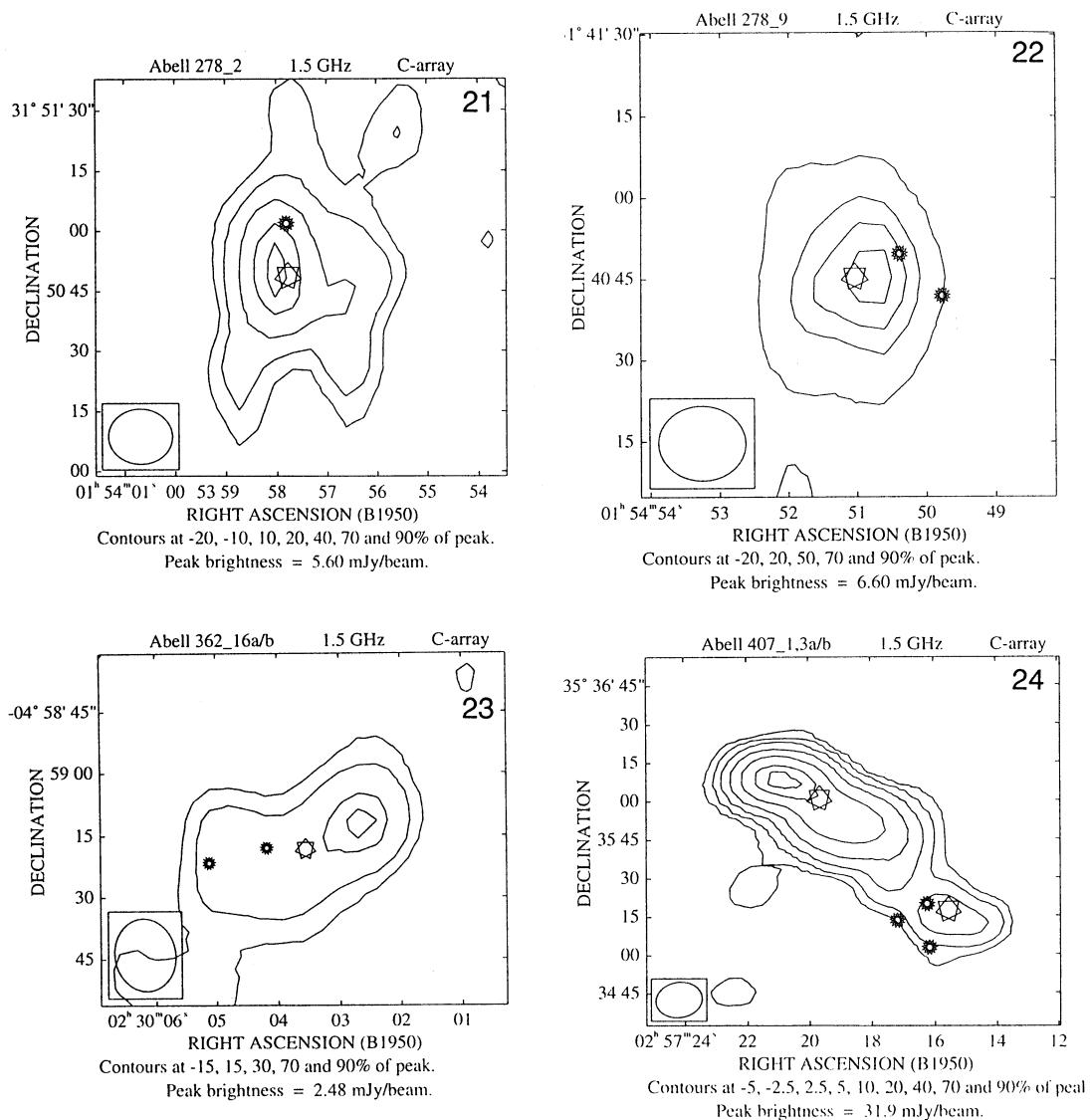
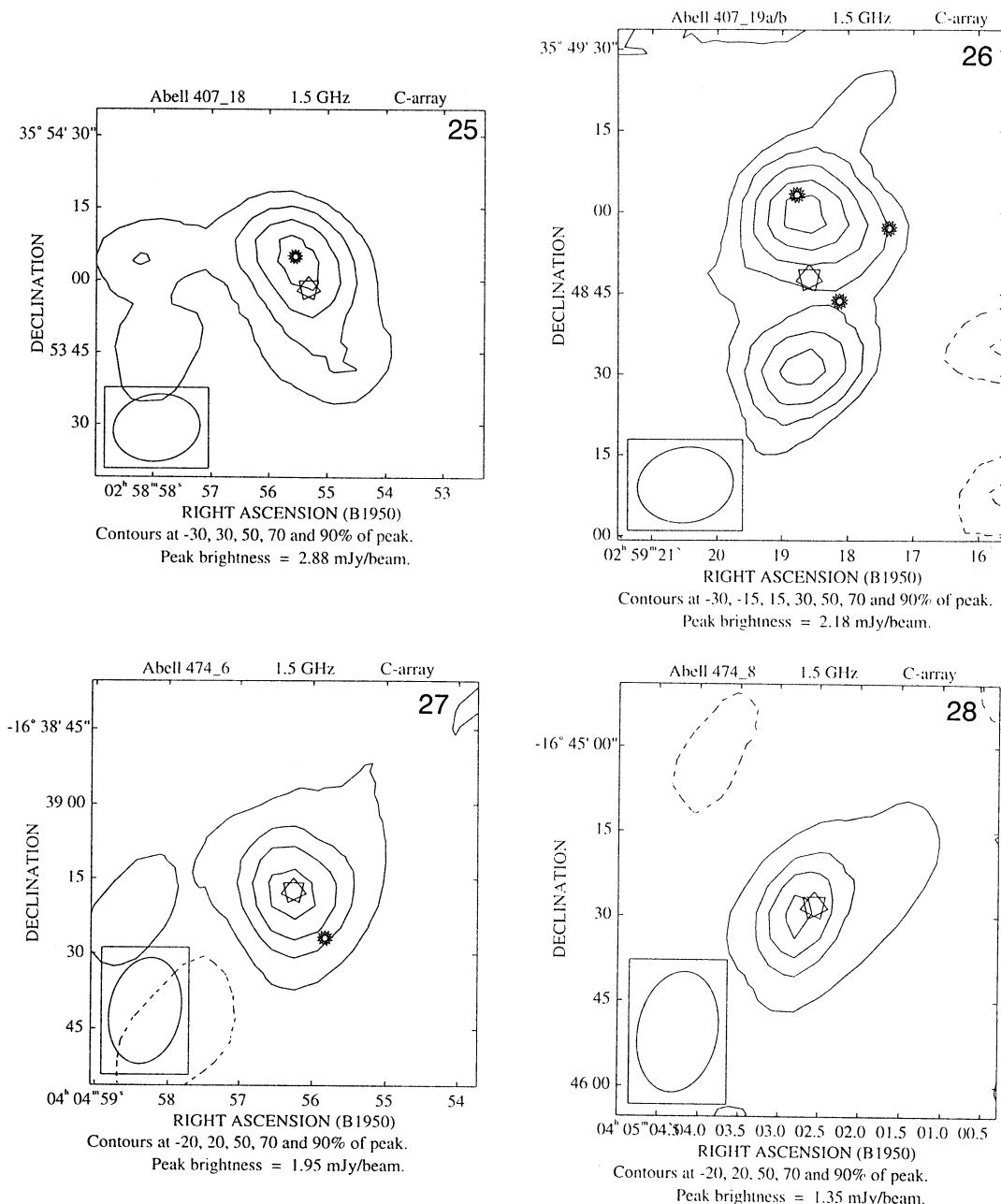


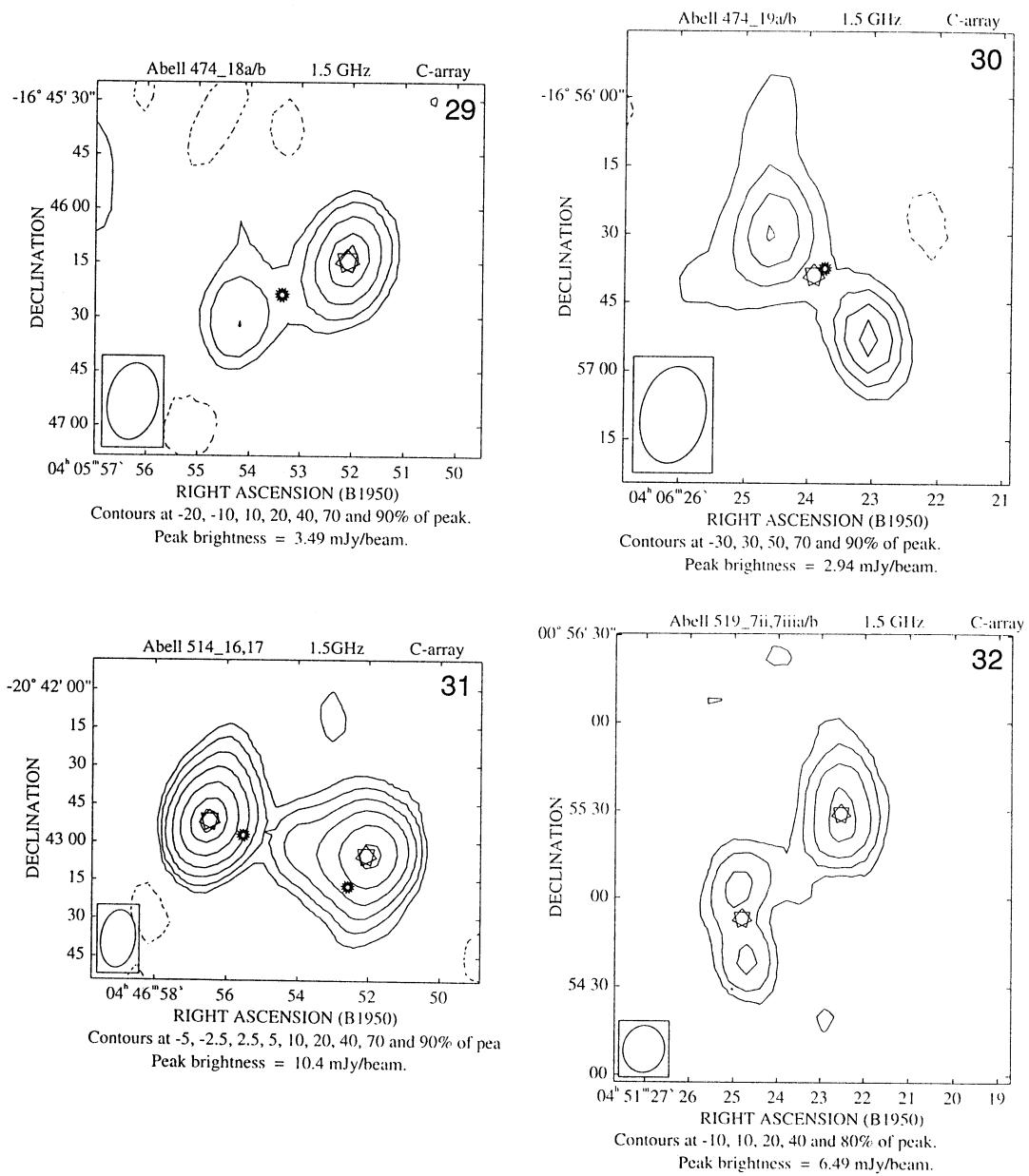
Fig. 1. (Continued)

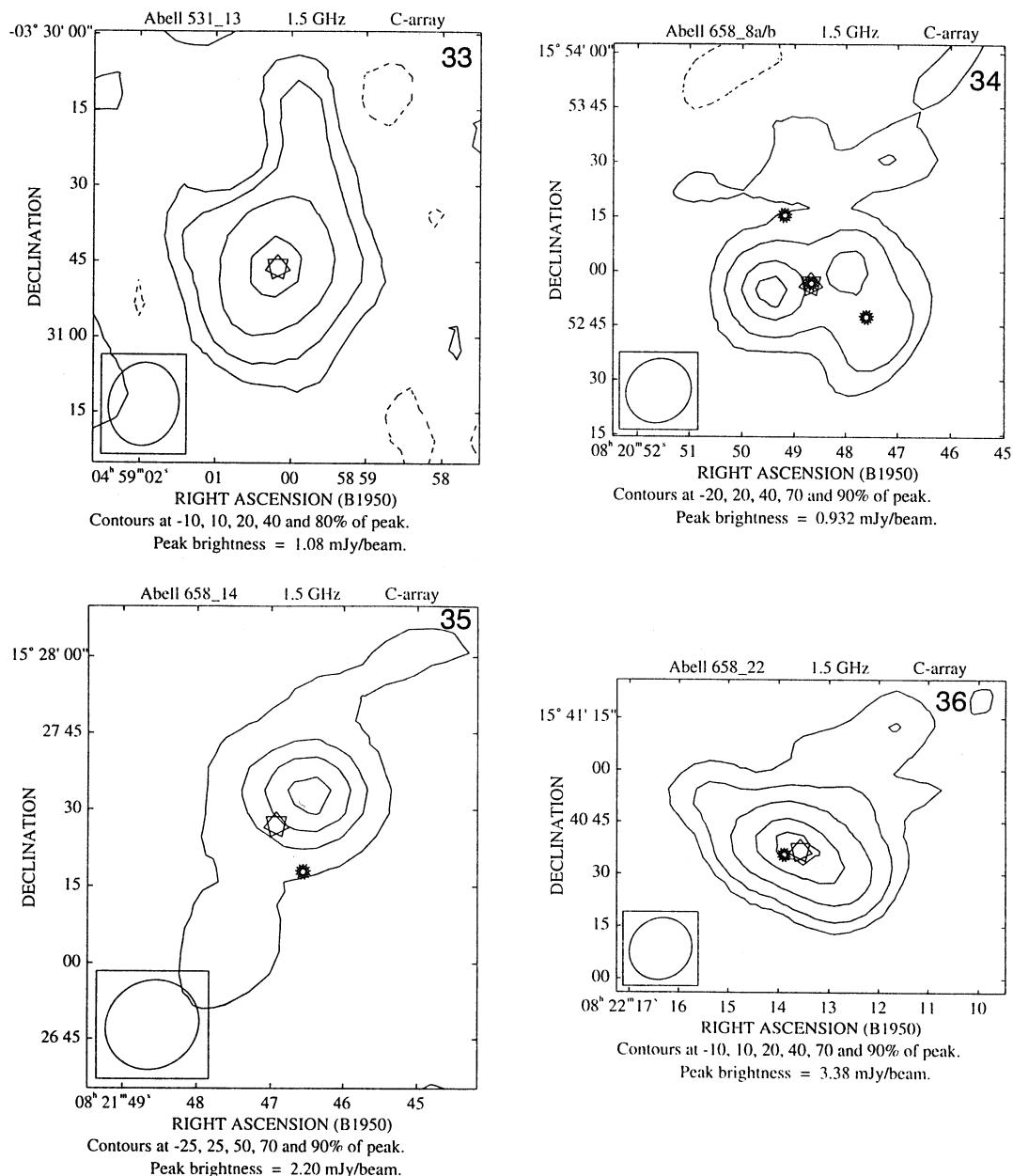
**Fig. 1. (Continued)**

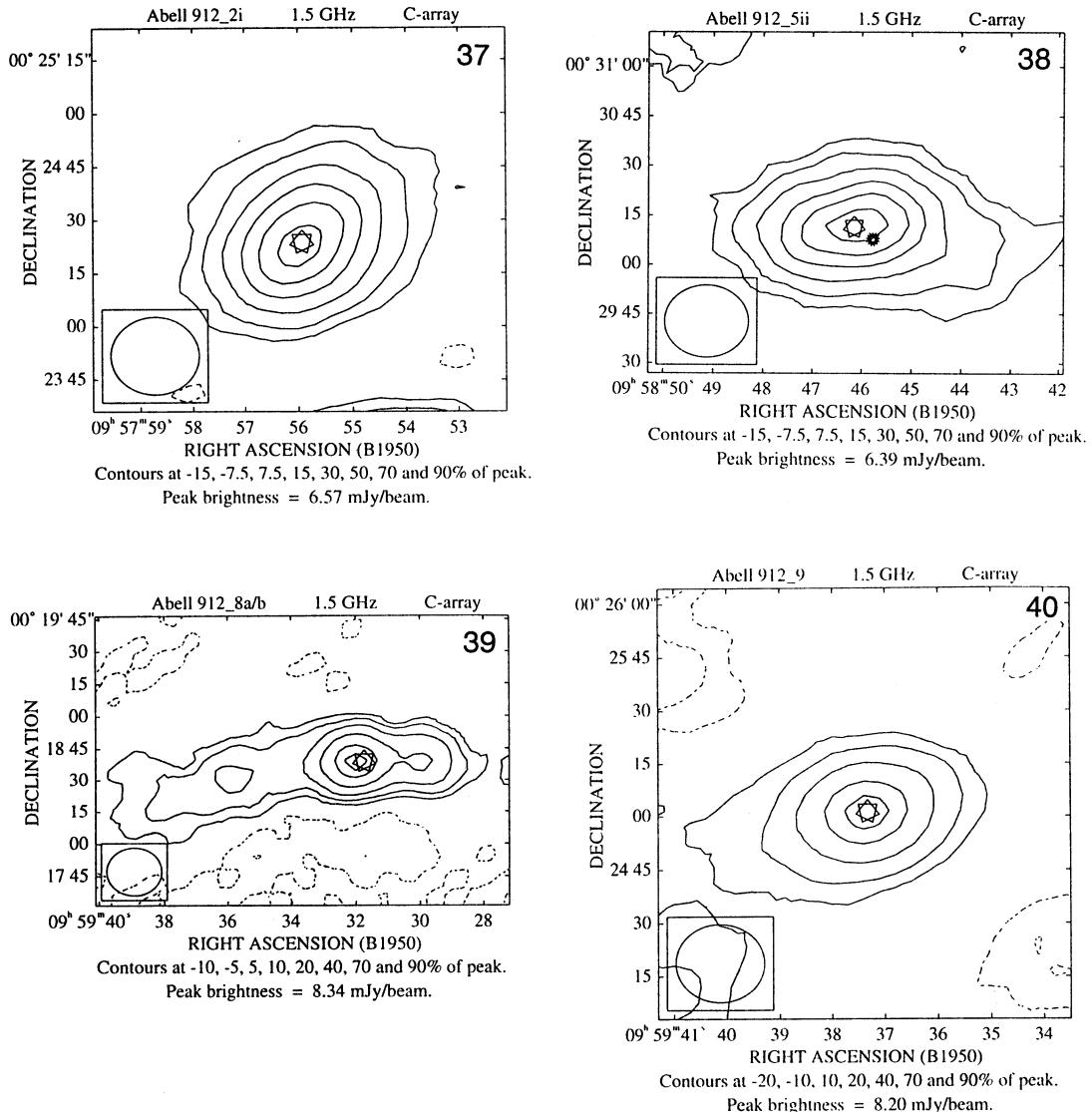
**Fig. 1. (Continued)**

Fig. 1. (*Continued*)

**Fig. 1. (Continued)**

**Fig. 1. (Continued)**

**Fig. 1. (Continued)**

**Fig. 1. (Continued)**

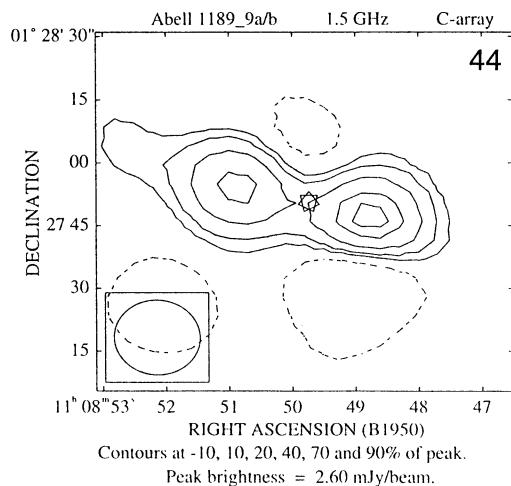
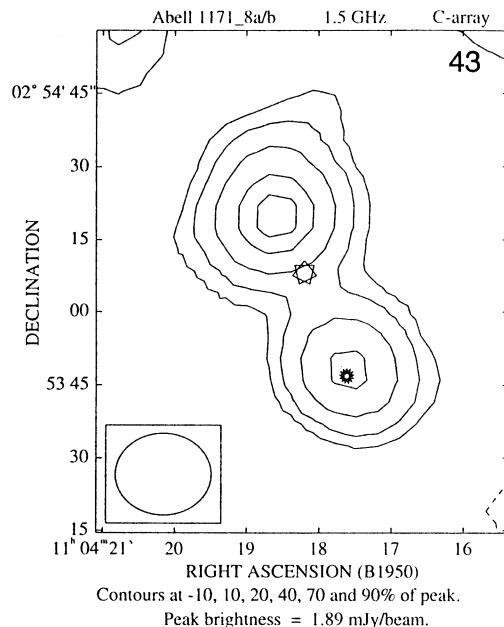
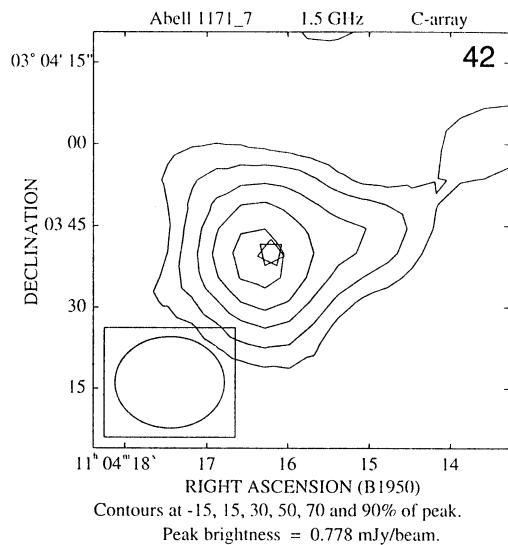
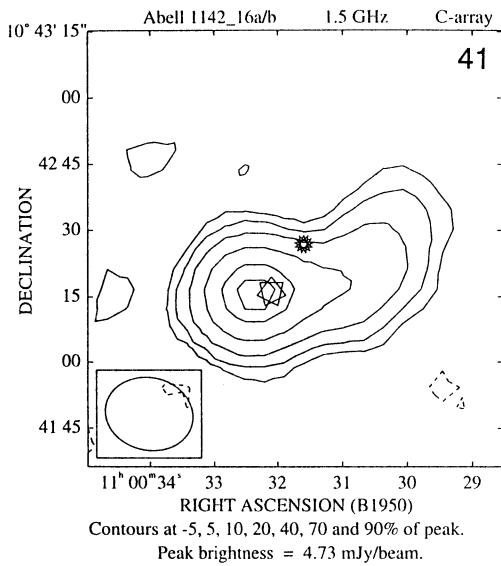
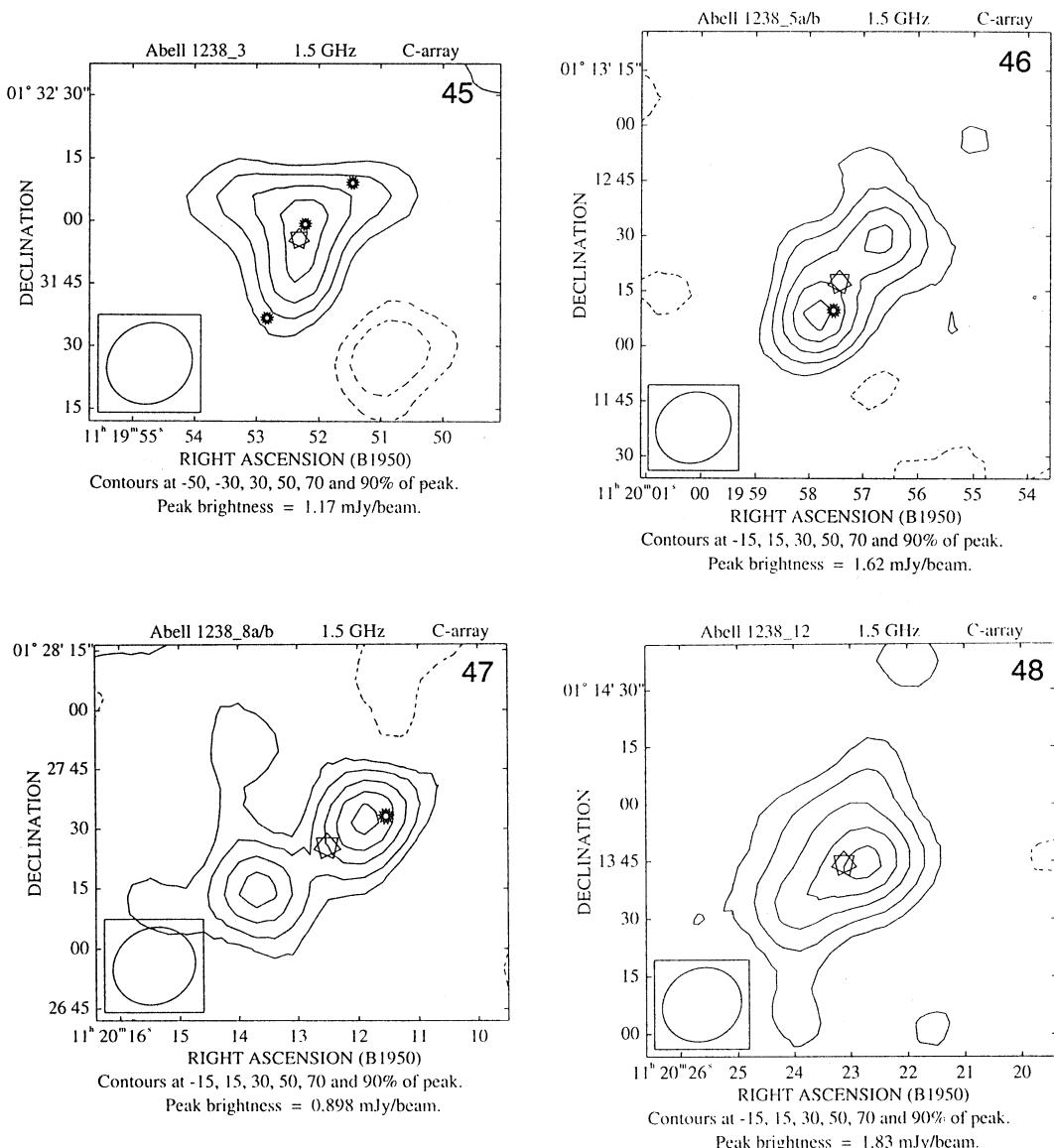
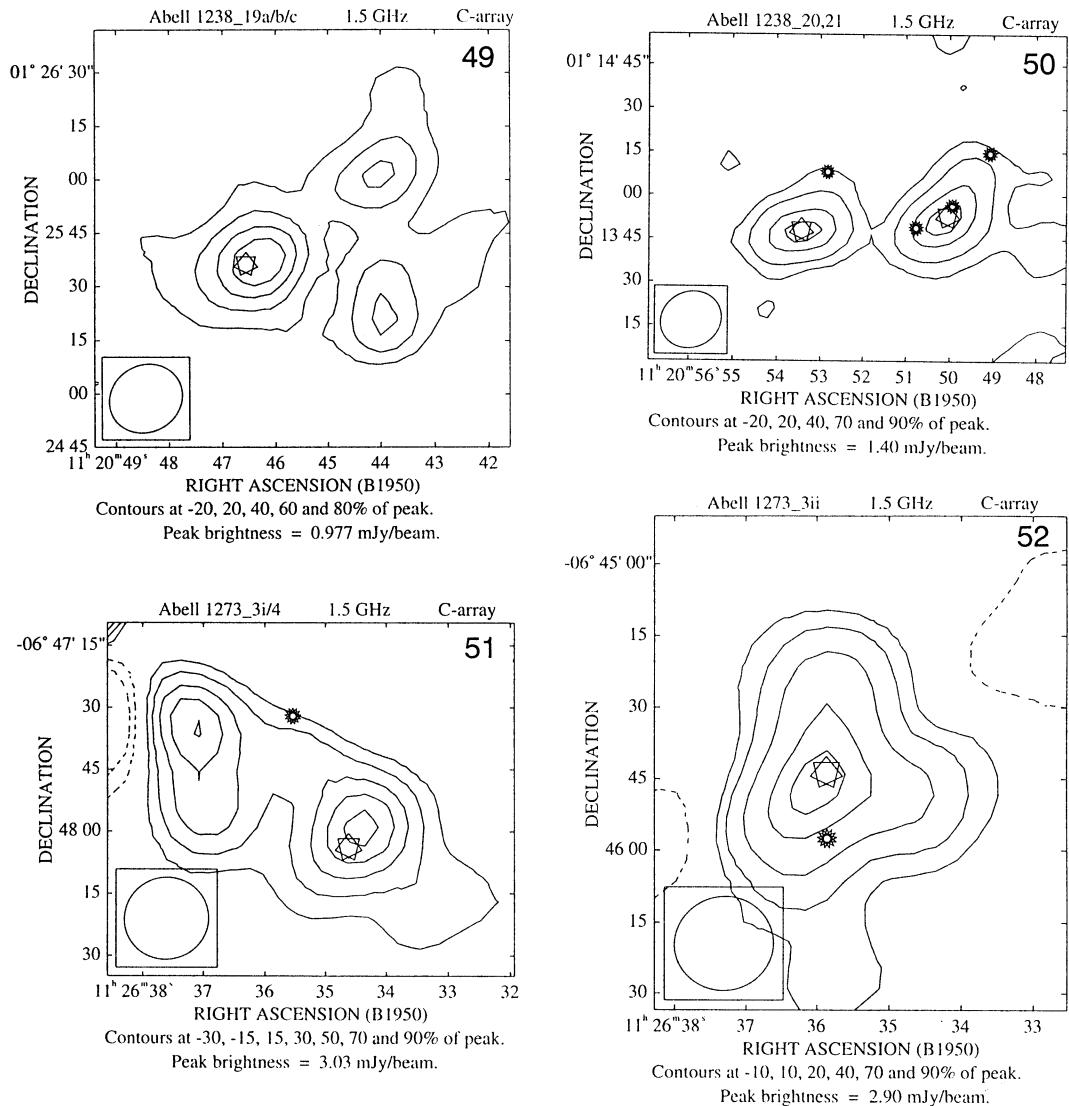
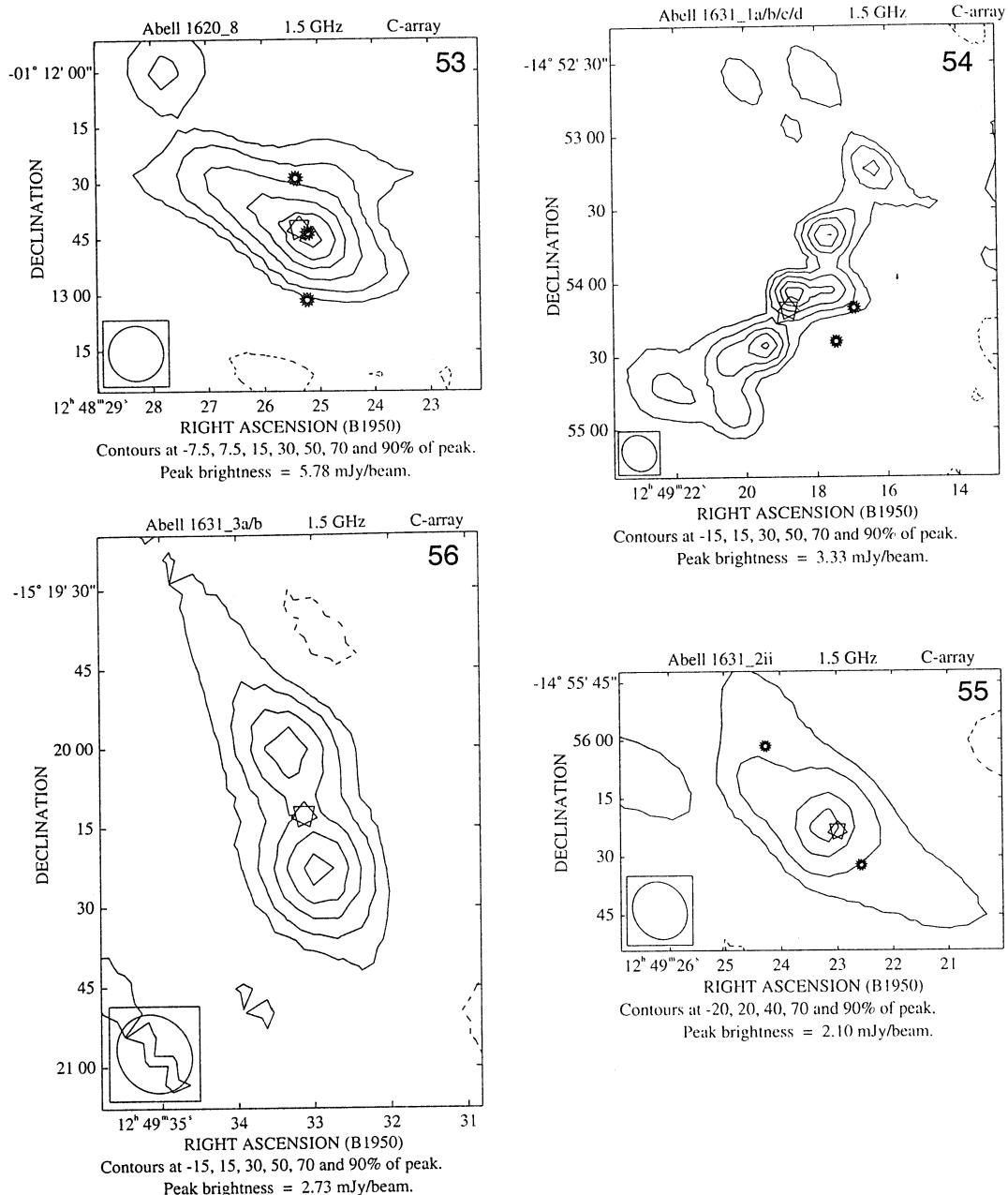


Fig. 1. (Continued)

**Fig. 1. (Continued)**

Fig. 1. (*Continued*)

**Fig. 1. (Continued)**

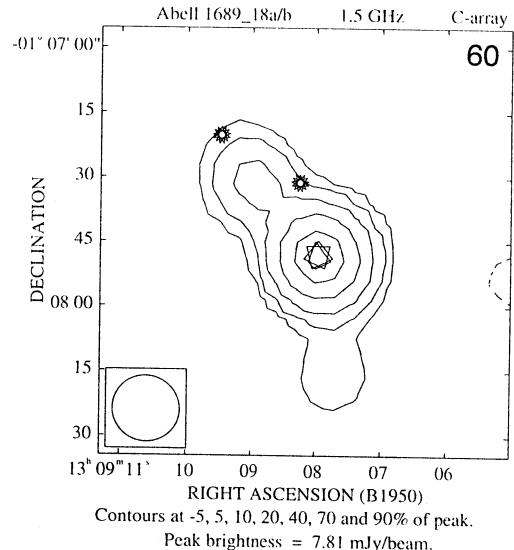
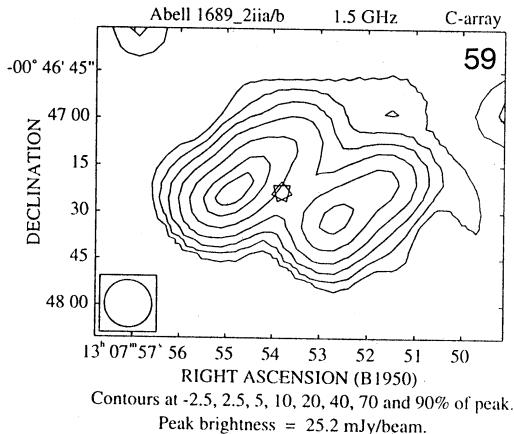
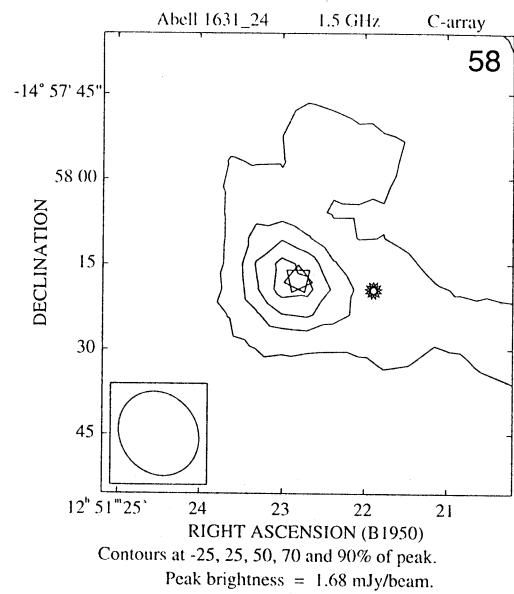
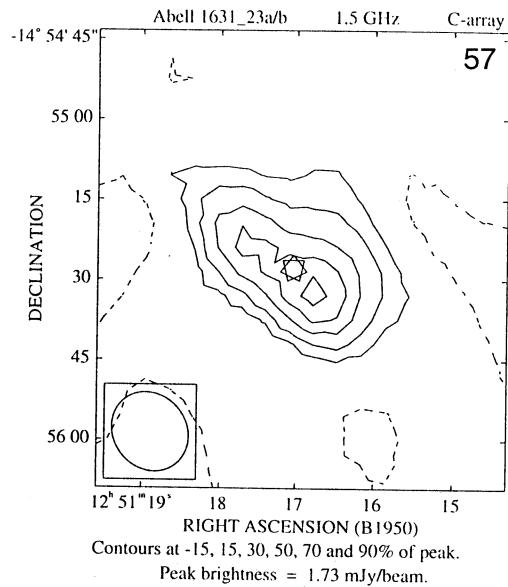
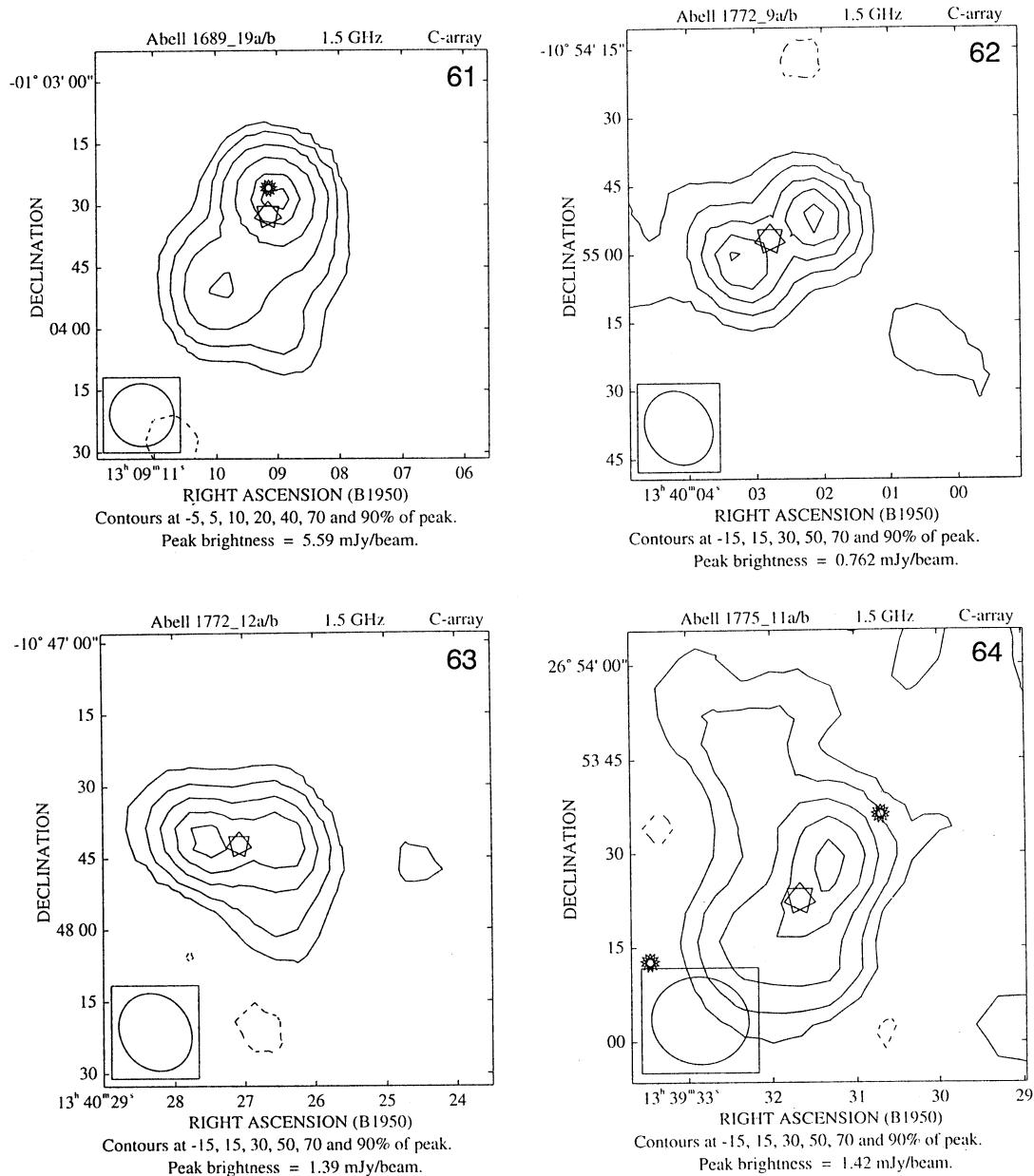


Fig. 1. (Continued)

**Fig. 1. (Continued)**

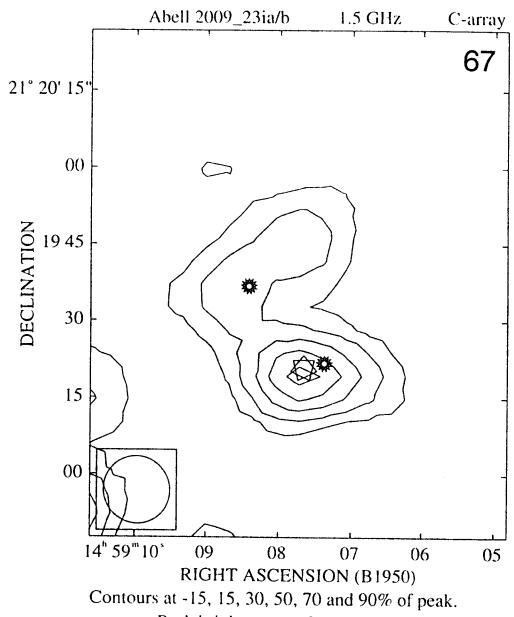
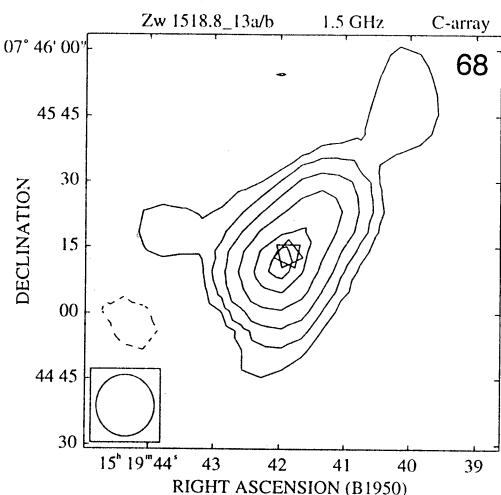
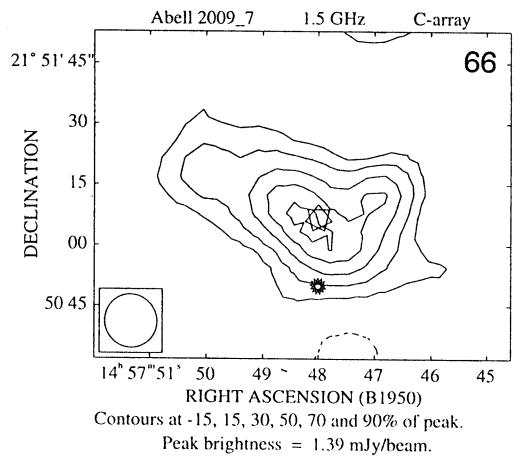
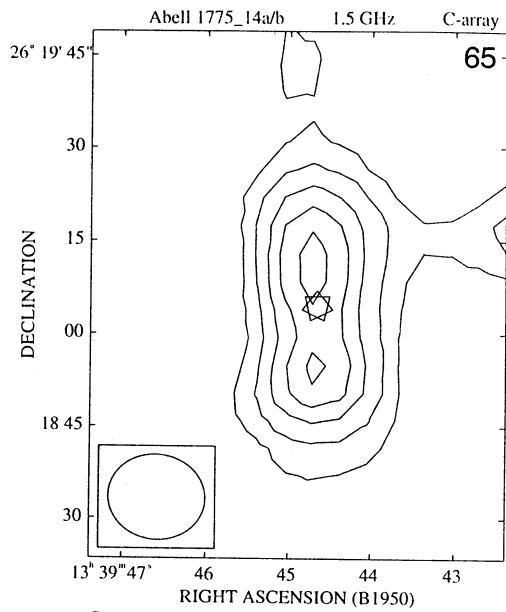


Fig. 1. (*Continued*)

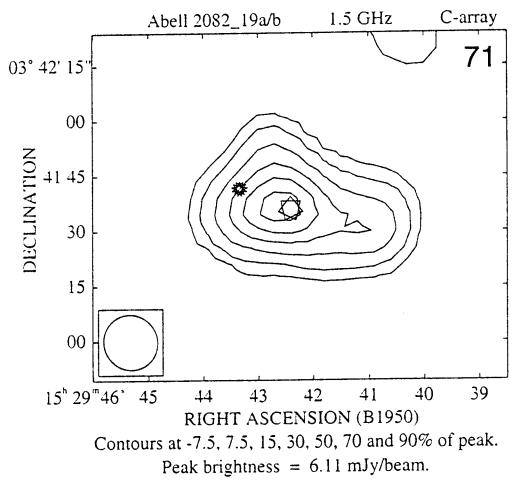
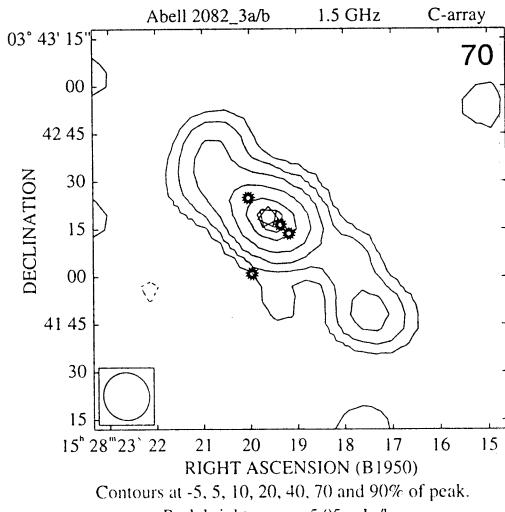
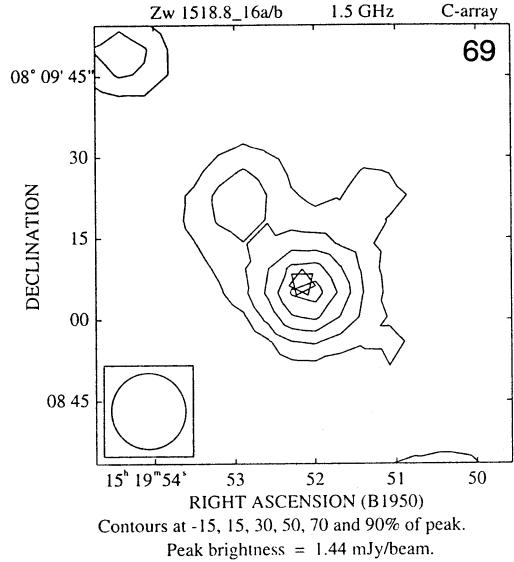
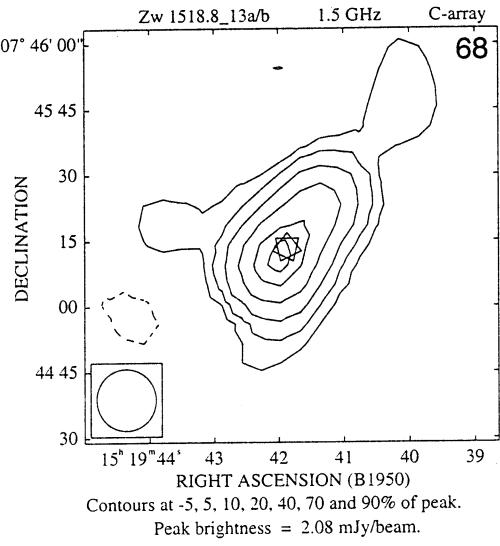


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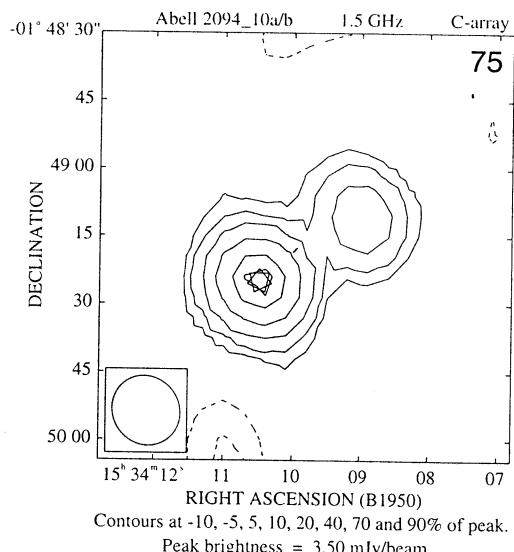
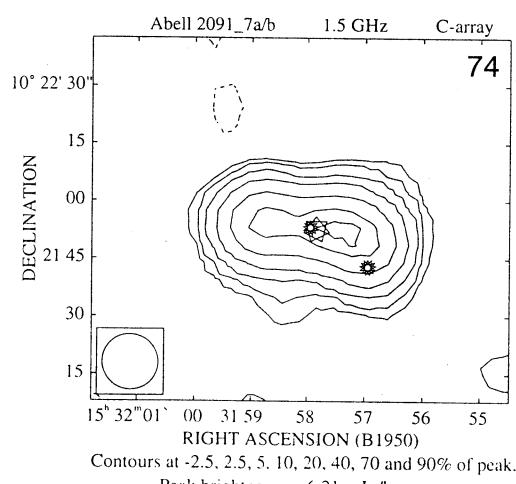
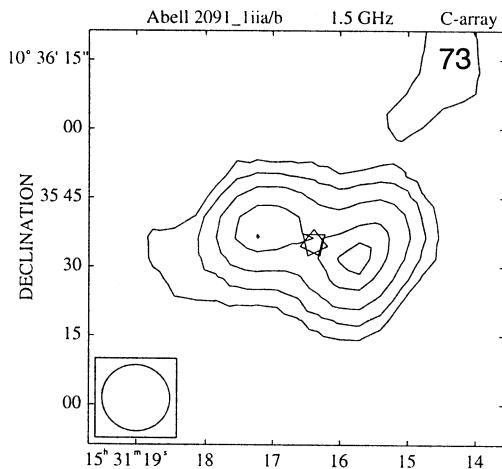
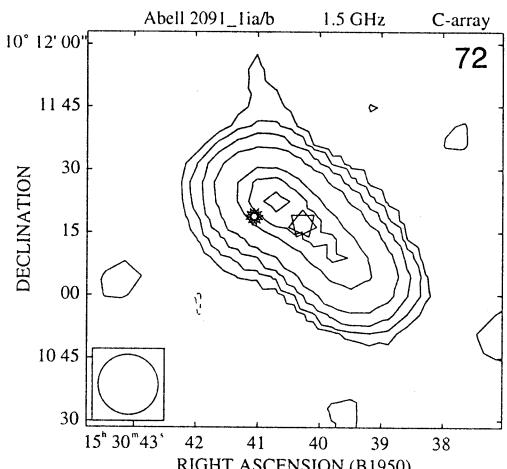
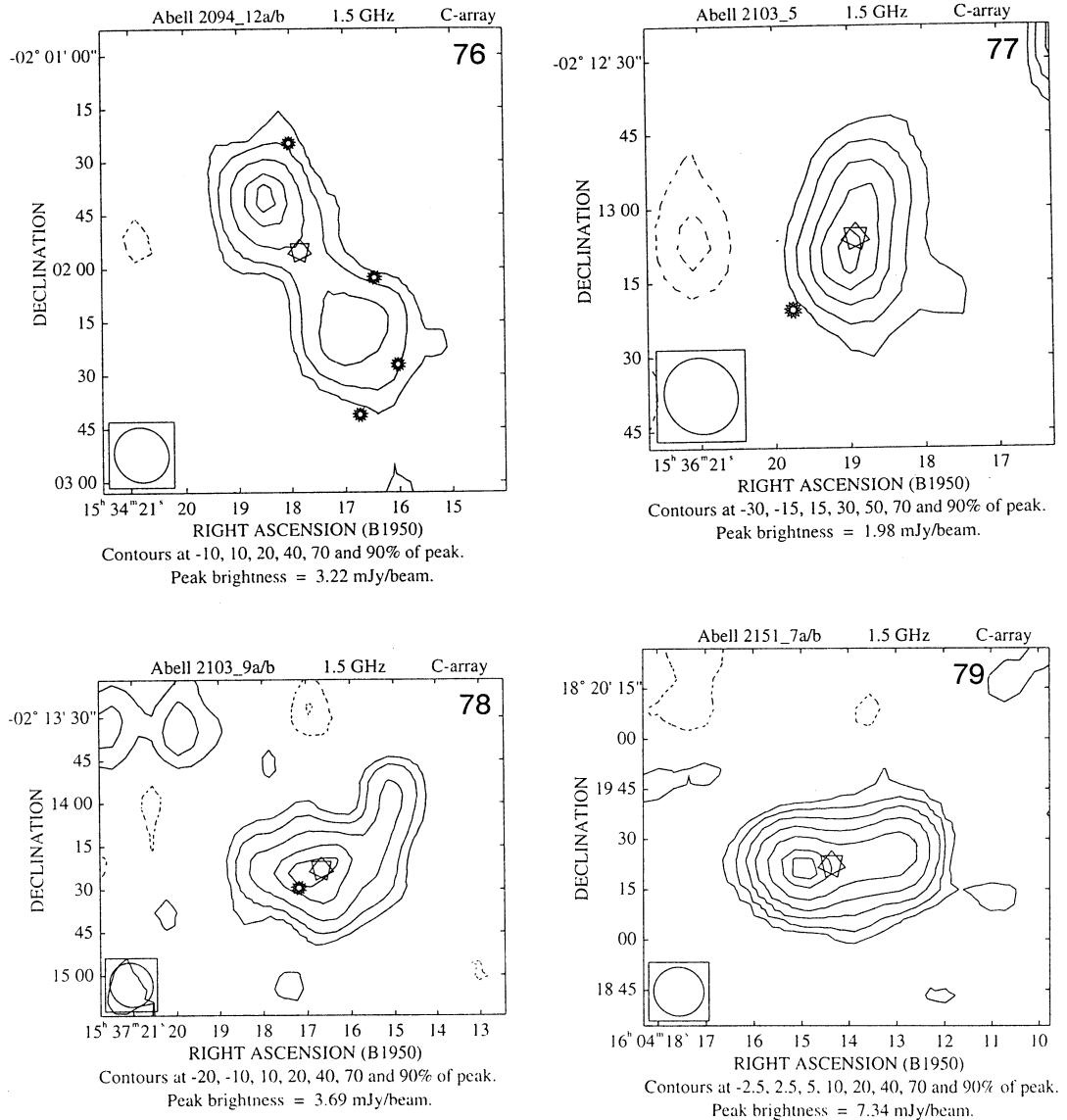
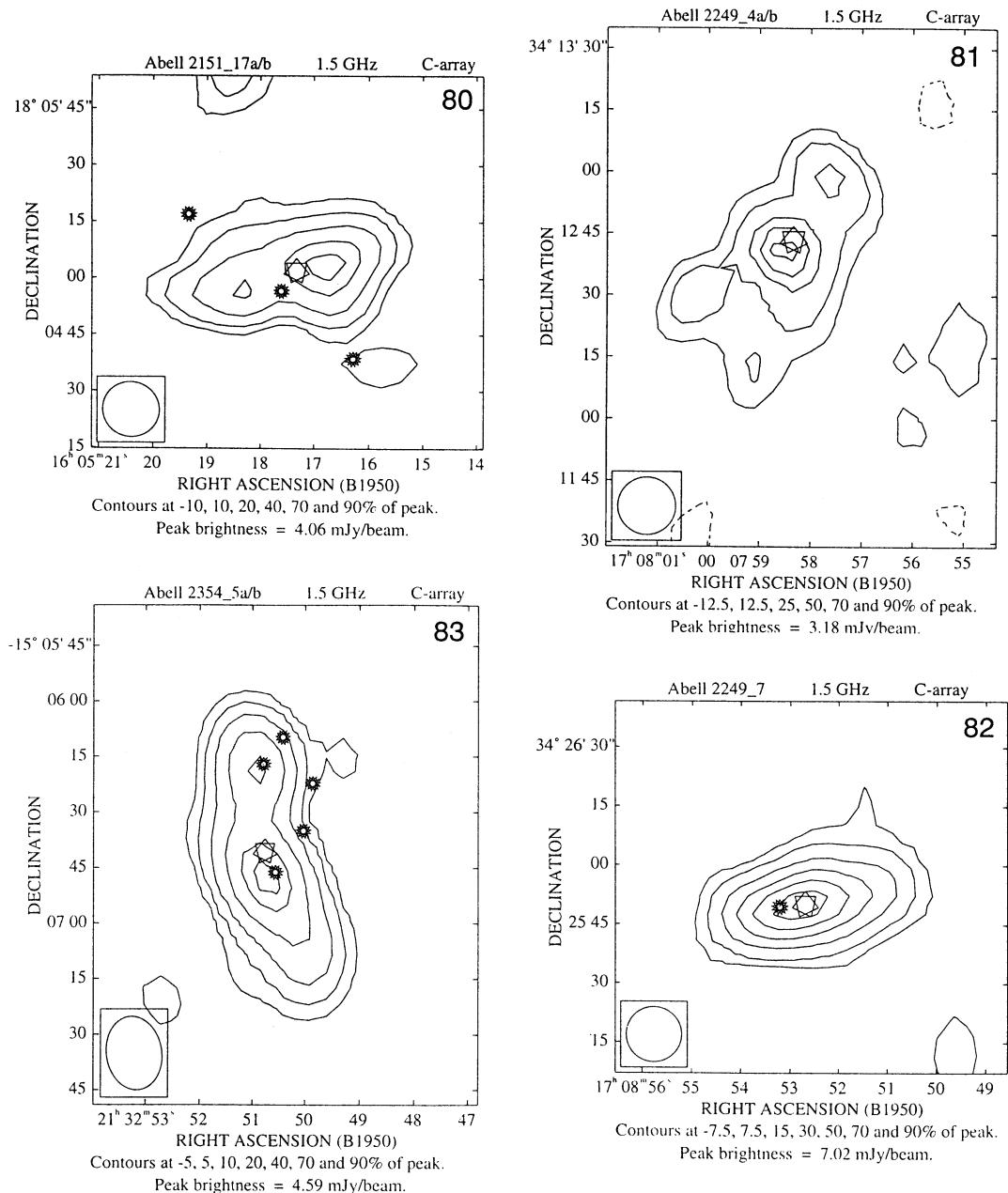
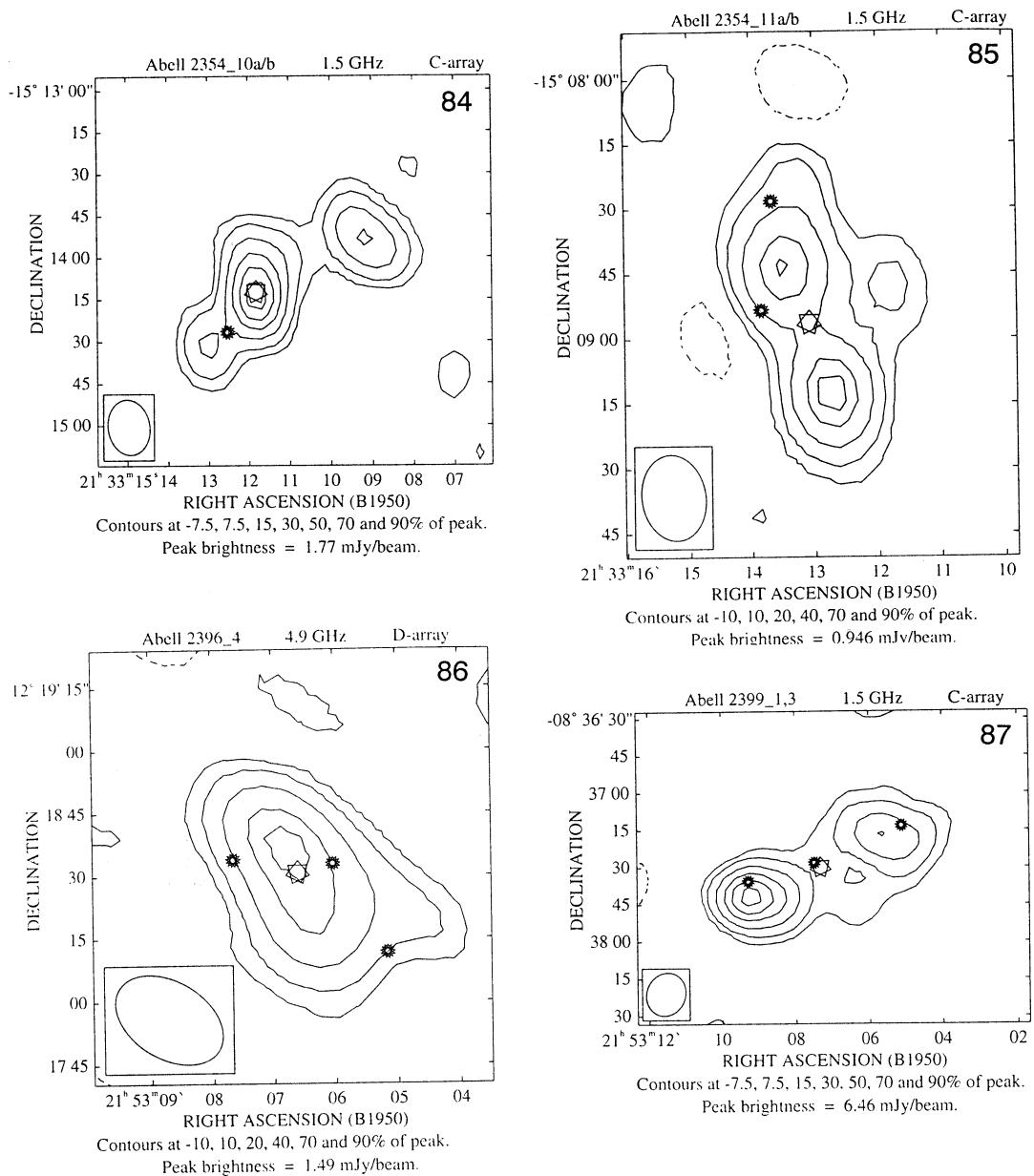
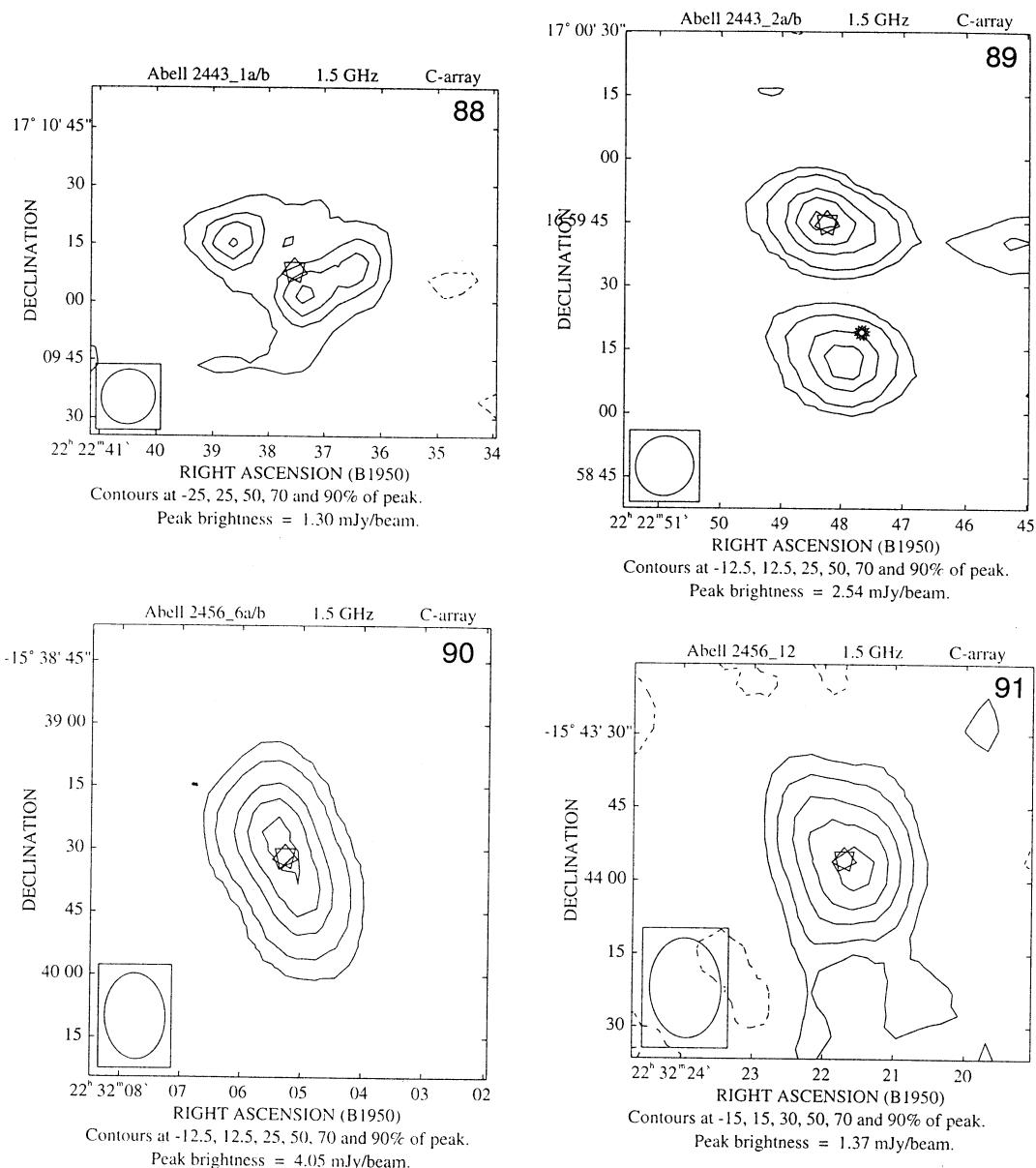


Fig. 1. (Continued)

**Fig. 1. (Continued)**

**Fig. 1. (Continued)**

**Fig. 1. (Continued)**

**Fig. 1. (Continued)**

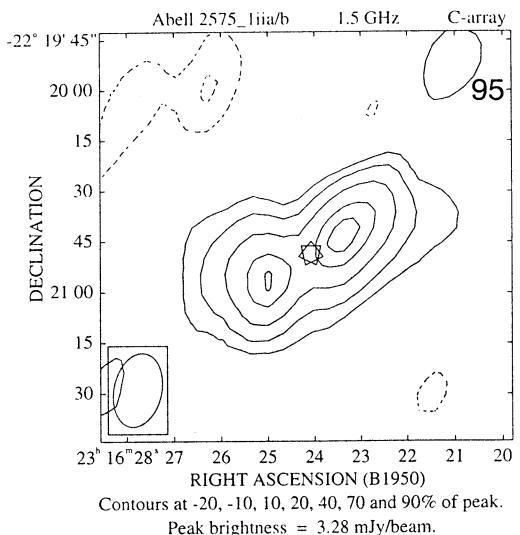
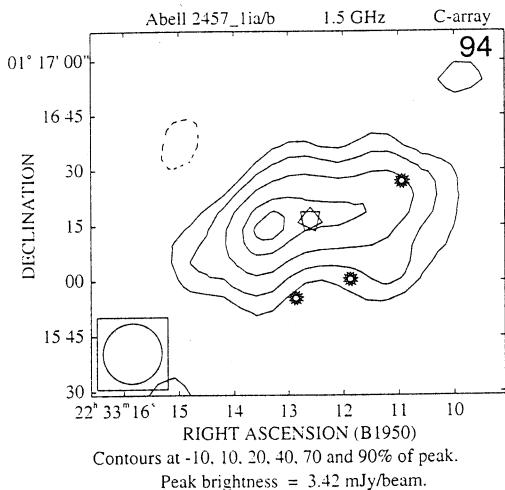
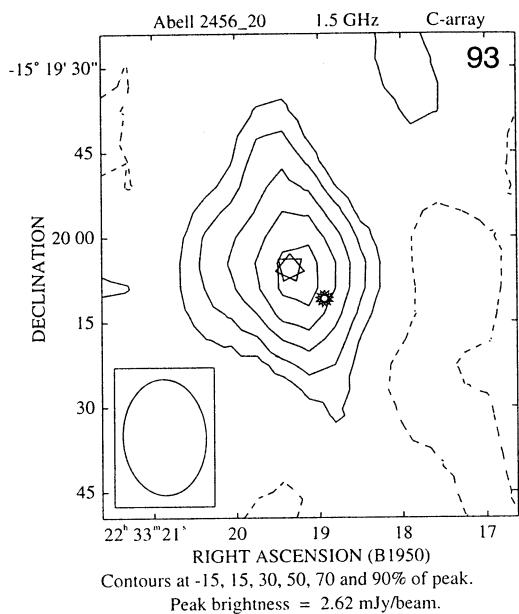
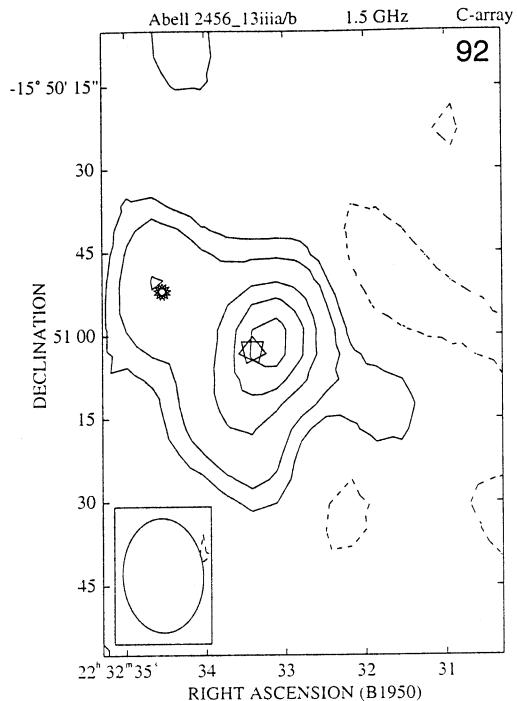


Fig. 1. (Continued)

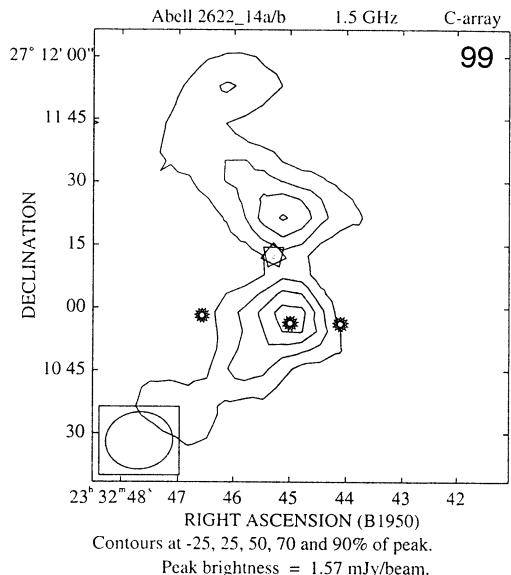
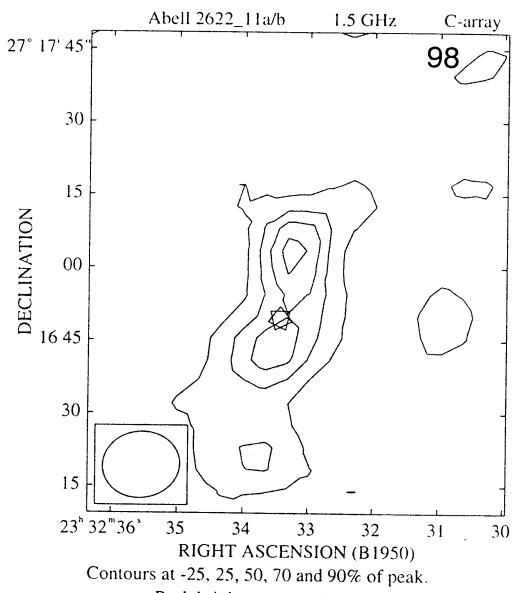
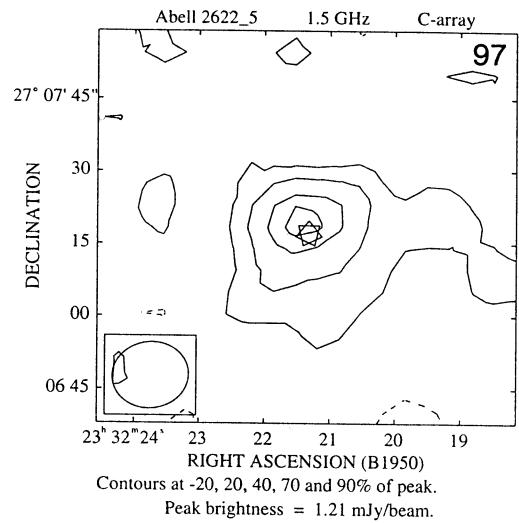
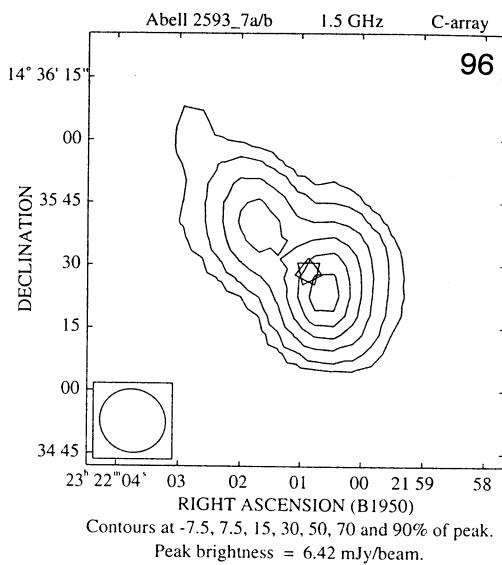


Fig. 1. (Continued)

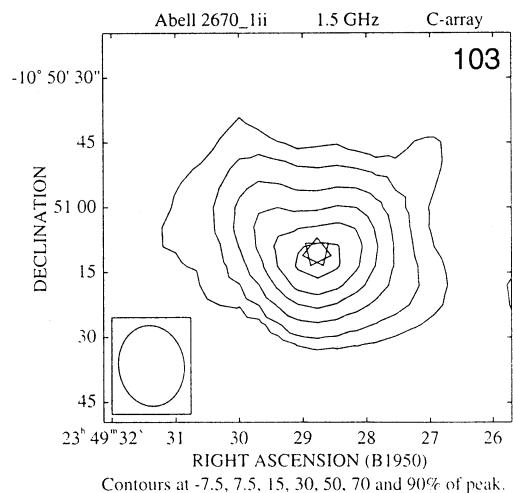
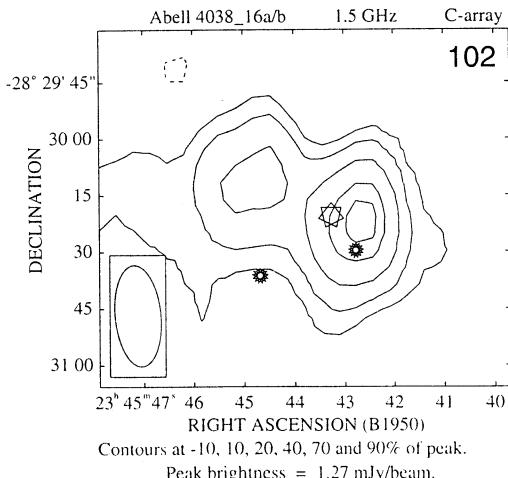
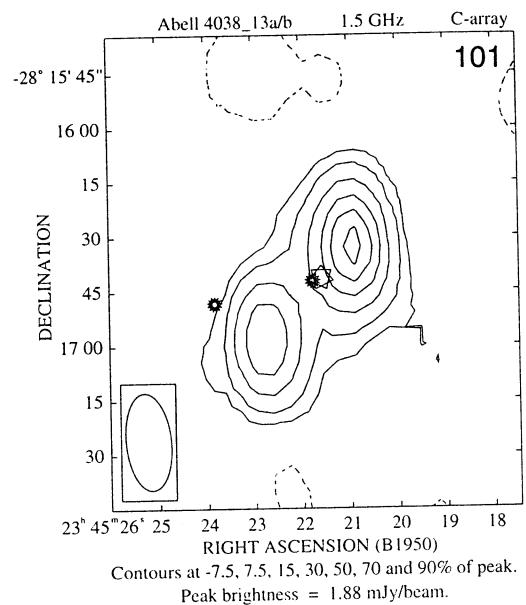
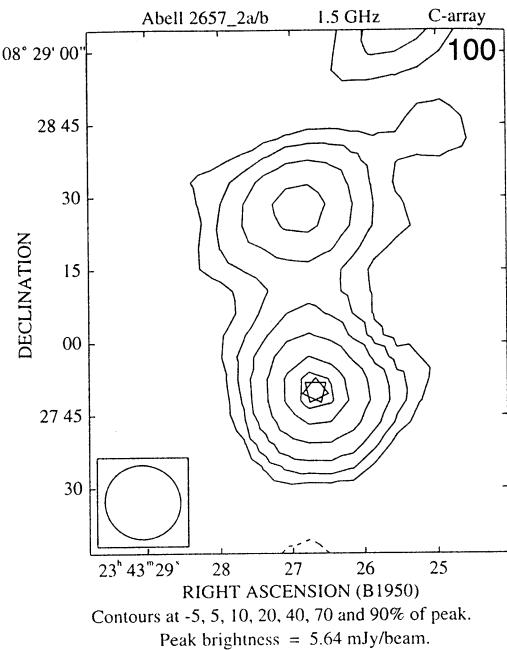


Fig. 1. (Continued)

accompanied by daggers in Tables 2 and 3 are those for which the source centroid position was ≥ 7.0 arcmin from the delay and phase centre, so that the smearing was ≥ 7 arcsec in the radial direction. The resulting image distortion depends upon the true angular dimensions of the source and on the position angle of the major axis of the restoring beam with respect to the radial direction from the map centre. Naturally, sources with angular dimensions appreciably greater than the smeared beam will not be particularly distorted. The parameters of the fitted Gaussians in Tables 2 and 3 have been corrected for the smearing.

Unlike Paper II, very few of these sources could be mapped at 4.9 GHz so that Fig. 1 contains only 1.5-GHz maps. The radio positions (mainly centroids) are depicted in Fig. 1 as large, open, 7-pointed stars on the maps, while the smaller, filled, 13-pointed stars show the positions of optical objects within the radio contours. The radio and optical positions are listed in Table 5, together with the morphologies of the optical objects.

(2e) Errors in the Parameters of Table 2

Errors in the flux density, spectral index and the Gaussian-fitted parameters result from a number of causes, the effects of which we estimate here. Flux density measurements are affected by:

- (i) A systematic multiplicative error in the flux density of our primary flux calibrator (3C 48). Baars *et al.* (1977) gave this as $<3\text{--}4\%$. We adopt an error of 3%.
- (ii) Flux bootstrapping from the primary to the secondary calibrators contributes a random multiplicative error of $\sim 4\%$.
- (iii) Pointing errors of 10 arcsec rms can generate a random multiplicative error of up to $\sim 1\%$ for sources out near the half-power points in the primary beam.
- (iv) Deconvolution in the mapping process can contribute a random multiplicative error of $\sim 3\%$.
- (v) Error from map noise and side lobes was estimated using the AIPS task IMEAN with a number of enclosing boxes with various areas and centre-offsets from the source. The values of rms map noise (Table 1) should be increased by the reciprocal of the primary beam attenuation.

The resulting 1σ random additive error was ~ 2 times the map rms (given in Table 1). In deriving errors in parameters such as spectral index and emitted radio power from the flux densities in this paper, one adds in quadrature the errors from (i) to (iv) to obtain a total multiplicative error of 6%, to which one adds in quadrature the random additive error in (v). As an example, a source with $S_{1.5} = 9.0$ mJy, $S_{4.9} = 3.0$ mJy from maps with $\text{rms} = 78 \mu\text{Jy beam}^{-1}$ has a spectral index $\alpha = -0.93 \pm 0.12$. The errors in the Gaussian-fitted parameters were found from a statistical analysis of fit-errors from 83 sources drawn from 1.5 GHz maps having a wide range of map rms. First, simple power-law regressions were made between fit-error and the several parameters that could possibly influence the error. We found that errors in the major and minor axes depended mainly on flux density/rms and ellipse area. The error in the position angle of the major axis depended on flux density/rms and axial ratio. Secondly, multiple regressions were then made to obtain the following best-fit, power-law equations:

$$\Delta \text{Maj.} = 0.36(S/N)^{-0.52}(\text{Maj.} * \text{Min.})^{+0.56}, \quad (1)$$

$$\Delta \text{Min.} = 5.08(S/N)^{-0.56}(\text{Maj.} * \text{Min.})^{+0.12}, \quad (2)$$

$$\Delta \text{PA} = 117.2(S/N)^{-0.61}(\text{AR})^{-1.07}, \quad (3)$$

where $\Delta \text{Maj.}$ is the error (arcsec) in the major axis (Maj.); $\Delta \text{Min.}$, the error (arcsec) in the minor axis (Min.); ΔPA , the error (degrees) in the position angle; AR the axial ratio of the fitted ellipse (Maj./Min.); and S/N , the flux density/rms.

As an example, we compute the 1σ errors in the Gaussian-fitted parameters for a source with $S = 5.0$ mJy from a map with $\text{rms} = 78 \mu\text{Jy beam}^{-1}$ and with $\text{Maj.} * \text{Min.} = 20 * 10 \text{ arcsec}^2$. Substituting in equations (1) to (3) we find

$$\Delta \text{Maj.} = 0.80 \text{ arcsec}, \quad \Delta \text{Min.} = 0.93 \text{ arcsec}, \quad \Delta \text{PA} = 4.4^\circ.$$

3. Optical Identifications

We examined the Palomar and SERC sky survey plates for optical counterparts to the sources in Table 2. The optical fields surrounding $\sim 95\%$ of the sources had been checked on the plates in connection with the preparation of Papers I and II, and Polaroid copies had been made if any optical object appeared within ~ 20 arcsec of the radio position. The remaining 5% of the sources were checked for optical counterparts on the COSMOS (Drinkwater *et al.* 1995) or APM (Irwin *et al.* 1994) digital versions of the surveys. We used both the catalogues and digital images on CD-ROM.

A detailed account of our optical position measurements and magnitude estimates is given in Paper II. An important difference in our treatment of these results is that the coordinates of optical objects within 20 arcsec of the radio position were obtained from the digitised surveys. We believe that these yield about the same accuracy (~ 1 arcsec) in either coordinate as we obtained with the Bolton machine for the identifications in Paper II. One advantage of the digitised SERC survey lay in our ability to make use of the SERC plates for radio sources with declinations as far north as $+2^\circ$ (copies of the SERC Equatorial Survey were not available in Sydney). In 95% of the sources we were able to check from Polaroid prints that the digital parameters gave a true description of the optical morphology and whether the digital position was affected by image blends; for those fields in the SERC Equatorial Survey, we checked the images on CD-ROM. If blending did occur, we estimated positions by offsetting from well-positioned sources on the Polaroids, whose scale of $3.4 \text{ arcsec mm}^{-1}$ was accurately known. The morphologies of faint objects are difficult to assess, both from the Polaroids and the digital surveys. It is very difficult to distinguish between galaxies and stars when the images are near the plate limit and so our classifications in such cases are subjective and should be treated with appropriate caution.

Table 5 presents the radio source positions and the parameters of all optical objects detected on the sky survey plates within ~ 20 arcsec of the radio position. The column headings are explained at the foot of the table.

The magnitudes of the objects listed in Table 5 were estimated in the same way as used in Paper II, supplemented by the digital estimates from COSMOS and APM. Our primary magnitude estimates are based on visual estimates from the Polaroids, using a 'fly-spanker' constructed for Paper II. In the southern section of our radio survey, we sometimes had Polaroids from both the SERC and Palomar I plates, enabling us to make independent brightness estimates of the same object. We estimate that the 'fly-spanker' estimates are accurate to about 0.5 mag, based on our tests outlined in Paper II. In summary, we think that the radio and optical positions in Table 5 are accurate to about 1 arcsec and the magnitude estimates to about 0.5 mag.

For each radio source Table 5 lists between zero (Blank Field) and seven optical candidates. We tried in Paper II to outline detailed identification criteria, but in Paper III we accepted any optical object within 10 arcsec of an unresolved radio source (i.e. <10 arcsec in major axis) as a possible identification. In the case of some of the more extended sources such as those shown in Fig. 1, we accepted optical objects further from the radio position as possible identifications. These likely identifications are printed in bold type. From past experience, galaxies rather than star-like images are much more likely to be associated with radio sources, but the low flux-density limit of the present survey means that it is possible to detect more true stellar emission than was likely in the stronger sources of Paper II. In addition, the lower flux-density limit of the present list may enable us to detect the so-called radio-quiet QSOs, so that coincidences with star-like images may be more frequent; one could only distinguish between stars and QSOs from their optical spectra.

Morphologies for 95% of the optical objects in Table 5 were estimated from the polaroid copies, the remaining 5 per cent being digital estimates from COSMOS or APM. We used the following criteria for the Polaroid estimates:

- (i) galaxies which were visibly extended, being surrounded by a diffuse structureless halo with an axial ratio less than ~ 2 , were classified as elliptical (E);
- (ii) galaxies satisfying the above definition but which were several times larger than all neighbouring galaxies were classified as 'cD' if near the cluster centre, or 'D' if well away from the cluster centre;
- (iii) images showing two barely resolved ellipticals were classed as 'DB'.
- (iv) a galaxy which satisfied the definition of an elliptical, except that the axial ratio was greater than ~ 2 , was classified as 'S0';
- (v) a galaxy with considerable structure in the halo was classified as a spiral (Sp).
- (vi) an image that was diffuse but too faint to assign to the above galaxy classes was called 'G';
- (vii) an image with a sharp circular boundary and sometimes showing diffraction spikes was classified as stellar (St). Some of these could, of course, be very compact ellipticals or QSOs. It should be noted that very faint images are difficult to assign to the G or St categories and often the choice is rather arbitrary.

4. Conclusion

We have listed the parameters of 737 sources detected in 60 VLA fields, which were located near 58 Abell clusters; 715 of the sources have flux densities <20 mJy at 1.5 GHz.

The measurements in this paper (Paper III) and in Paper II constitute a large database from which we can assemble a complete flux limited sample of radio sources in or near rich clusters of galaxies. In a forthcoming paper, we will use such a sample to explore the complex relationships between the radio, optical and X-ray measurements.

Acknowledgments

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Note added in proof

Electronic versions of the data tables presented in Papers II and III are available through the EINSTEIN On-line Service (EOLS) at the Center for Astrophysics (telnet einline.harvard.edu, login as einline), as well as from the NASA Astronomical Data Center (ADC) and the Centre de Donnees Astronomique Strasbourg (CDS).

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