

The Radio Properties of a Complete Sample of Bright Galaxies

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Abstract

Results are given for the radio continuum properties of an optically complete sample of 294 bright galaxies, 147 of which have been detected. Data were obtained with the 408 MHz Molonglo Radio Telescope. The radio luminosity functions for all galaxies and for spiral galaxies alone are derived and the radio emission for different galaxy types is investigated. Spectral indices of 73 galaxies which had been detected at other frequencies were derived; the mean index of a reliable subsample is $\langle\alpha\rangle = -0.71$.

1. Introduction

There have been many extensive surveys of continuum radio emission from bright galaxies. The earliest comprehensive survey of high sensitivity was that of Cameron (1971*a*, 1971*b*) using the Molonglo Cross Radio Telescope at 408 MHz. Cameron observed two optically complete samples south of $\delta = +18^\circ$ and defined the radio luminosity function with reasonable statistics at radio powers of $\sim 10^{22} \text{ W Hz}^{-1}$. In the past decade the optical properties of galaxies have been revised so that the selection of an optically complete sample is more reliable. In addition, between 1970 and 1978 the sensitivity of the 408 MHz Molonglo Cross was improved by more than a magnitude, permitting more detections and more accurate measurements of weak radio emission. Before observations at 408 MHz with the Molonglo Cross ceased in 1978, a new survey was made to improve Cameron's results and provide the best possible data base for subsequent investigations at different frequencies. Well-observed sources in Cameron's catalogue were not re-observed, although they are included in the tabulated results. Altogether, 294 galaxies are listed, of which 147 have been detected; however, 28 of these detections are shown to be uncertain because of low signal-to-noise ratios, confusion or discordant positions.

A description of the new survey and tabulation of directly measured properties appears in Section 2. Section 3 re-evaluates the radio luminosity function and discusses the relationship between galaxy types and their optical and radio properties. Section 4 derives spectral indices of 73 galaxies from the present data and previously published surveys at other frequencies.

2. Observations

(a) Sample Selection

The selection criteria were identical with those of Cameron (1971*a*). Two groups of galaxies were chosen: those brighter than total corrected optical magnitude 11.0

and south of $\delta = +18^\circ$; and those with photographic magnitudes less than 12.5 in the regions $b = -35^\circ$ to -60° , $l = 100^\circ$ to 220° and $b = +35^\circ$ to $+60^\circ$, $\delta \leq +18^\circ$. Eight galaxies were excluded from the original sample and a further 33 not selected by Cameron were added. These changes resulted from considerable revisions of optical magnitudes (de Vaucouleurs *et al.* 1976; de Vaucouleurs 1977; de Vaucouleurs and Corwin 1977; de Vaucouleurs *et al.* 1977; de Vaucouleurs and Bollinger 1977*a*, 1977*b*, 1977*c*; de Vaucouleurs and Head 1978; de Vaucouleurs *et al.* 1981; and de Vaucouleurs, personal communication 1978).

The new survey includes:

- (1) from Cameron's list 1, all detected galaxies with measured flux densities less than 500 mJy ($1 \text{ Jy} \equiv 10^{-26} \text{ W m}^{-2} \text{ Hz}^{-1}$) and all undetected galaxies except NGC 4293;
- (2) from Cameron's list 2, all detected galaxies with measured flux densities less than $500/n^{1/2}$ mJy (where n is the number of transits observed), NGC 660 and all undetected galaxies;
- (3) the 33 galaxies not previously observed.

Of 239 galaxies observed in this program, 92 were detected, 28 of these with some qualifications.

(b) Calibration

The survey was conducted in February, May and August 1978 using the Molonglo Radio Telescope at 408 MHz with a bandwidth of 2.5 MHz. The effective beam-widths were 2.86 arcmin in right ascension and 2.86 sec z arcmin in declination where z is the zenith angle.

Optical positions were taken initially from the 'Second Reference Catalogue of Bright Galaxies' (RC2) (de Vaucouleurs *et al.* 1976). However, where large discrepancies between optical and fitted radio positions occurred, new positional determinations were made using Palomar Sky Survey plates (PSS) and European Southern Observatory blue plates (ESOB). An x - y measuring machine was used to obtain positional accuracies ranging from 1 arcsec for compact images (Hunstead 1971, 1974) to about 30 arcsec for the most extended galaxies.

The pointing of the telescope and the flux density scales were calibrated by observing point sources with accurately known positions and flux densities. These were taken from Hunstead (1972). Known variable sources (McAdam 1978) were not used for the flux density calibrations. All flux densities are based on the absolute scale of Wyllie (1969*a*, 1969*b*).

There are many factors influencing the accuracy of these calibrations and individual observations. To provide useful estimates of positional and flux density errors, general terms which represent telescope pointing uncertainties, random noise and confusion have been adopted.

For point sources, the standard errors in observed positions are of the form

$$\sigma = \{a^2 + (b/Sn^{1/2})^2\}^{1/2}, \quad (1)$$

where S is the flux density in mJy and n is the number of transits observed. Empirical estimates of the constants a and b are tabulated below. Positions of extended sources (diameter $\gtrsim 3$ arcmin) are less certain. A contour map of each transit of a galaxy

was produced and mid points of the contours were used to derive a position with standard deviations of X in right ascension and $X \sec z$ in declination, where z is the zenith angle and X varies from ~ 6 arcsec for symmetric sources to ~ 10 arcsec for complex asymmetric sources. These errors were combined with the errors derived from equation (1).

Flux density uncertainties for unresolved sources are expressed as

$$\sigma_s = \{a^2 + (b/n^{\frac{1}{2}})^2 + (cS)^2\}^{\frac{1}{2}}, \quad (2)$$

where n and S have the same meanings as before. For extended sources, fitting of the beamshape was inappropriate and integrated flux densities were computed. A further uncertainty of 5% was then included because of difficulties in estimating the flux density between the zero and first contour levels. The constants used for equations (1) and (2) are:

Parameter	a	b	c
Right ascension (s)	$0.2 \sec \delta$	$100 \sec \delta$	—
Declination (")	3	1500	—
Flux density (mJy)	11	15	0.04

(c) Directly Measured Properties

A detected radio source was regarded as being identified with a galaxy if the positional discrepancy was less than 1 arcmin or 2 kpc in projected distance, whichever was the larger. It is unlikely that any chance coincidences are included with these criteria; however, some real associations may have been rejected. These would be included among the 'confusing sources' in the Notes to Table 1 (see p. 342).

The results of the 1978 survey are shown in Table 1, together with results for those galaxies detected by Cameron (1971*a*, 1971*b*) in 1968–69 and not re-observed; these are indicated by an asterisk next to the flux density measurement. The columns are:

- Column 1, line 1: NGC, IC or other identifying label. An asterisk indicates that the galaxy was not detected because of faulty observations or loss of data during computer analysis.
- Column 2, line 1: Revised morphological type of de Vaucouleurs *et al.* (RC2).
line 2: Hubble morphological type (RC2).
- Column 3, line 1: Optical right ascension in hours, minutes and seconds.
line 2: Radio right ascension and standard error in seconds of time.
- Column 4, line 1: Optical declination in degrees, minutes and seconds.
line 2: Radio declination and standard error in seconds of arc.
- Column 5, line 1: Distance in Mpc obtained, in order of preference, from
(1) de Vaucouleurs (personal communication 1981): 115 galaxies.
(2) de Vaucouleurs *et al.* (1981): 78 galaxies.
(3) de Vaucouleurs (1979*a*): 56 galaxies.
(4) de Vaucouleurs and Bollinger (1979) and the RC2: 30 galaxies.
(5) de Vaucouleurs (1979*b*): 2 galaxies.
(6) Sandage (1978), RC2 and de Vaucouleurs and Bollinger (1979): 9 galaxies.

A colon indicates either a large uncertainty in the distance or derivation of the distance from preliminary values of the modulus.

Table 1. Optical and radio properties of galaxy sample

N	Type	R.A.	Dec.	Dist. (Mpc)	MAG MABS	S (mJy) P*E18 (W/Hz)	RMAG RMABS	R408 -alpha	Note
7814	SA 2	00 00 41.4	15 52 00	12.5	10.93	< 45	> 14.9	>4.0	
	SAB				-19.5	< 837	> -15.6		
45	SA 8	00 11 31.8	-23 27 36	5.68	10.78	< 90	> 14.2	>3.4	S
	SDM				-18.0	< 336	> -14.6		
55	SB 9	00 12 24.0	-39 28 00	1.57	6.98	1300*	11.3	4.3	
	SBM	(EMISSION OVER OPTICAL EXTENT)			-18.9	3830	-14.6		
134	SX 4	00 27 54	-33 32	12.7:	10.43	398 27	12.6	2.2	
	SBC	27 54.7	31 01	9	-20.1	7690	-17.9	.1	
157	SX 4	00 32 14.4	-08 40 18	12.1	10.75	544 33	12.2	1.5	
	SBC	32 14.0	40 10	9	-19.7	9500	-18.2	0.22	.39
247	SX 7	00 44 39.6	-21 01 48	2.83	8.98	52 13	14.8	5.8	
	SD	44 39.7	01 13		-18.3	49.8	-12.5		
253	SX 5	00 45 07.8	-25 33 42	3.11	7.50	16200*	8.5	1.0	
	SC	45 06.1	33 34		-20.0	18800	-19.0	0.63	.07
300	SA 7	00 52 31.8	-37 57 18	1.74	8.39	< 180	> 13.5	>5.1	N
	SD				-17.8	< 64.1	> -12.7		
0057-33	E3P	00 57 36	-33 58	0.12:	6.8*	< 100	> 14.1	>7.3	
	DE				-13.6	< 0.17	> -6.3		
I1613	IX 10	01 02 13.2	01 51 00	0.7:	9.69	< 120	> 13.8	>4.1	
	IM				-14.5	< 6.91	> -10.4		
428	SX 9	01 10 21.7	00 42 53	10.0	11.55	85: 13	14.2	2.7	
	SM	10 20.6	43 21		-18.5	1020	-15.8		
474	LA	01 17 31.8	03 09 18	15.9:	11.74	< 95	> 14.1	>2.4	
	SO				-19.3	<2854	> -16.9		
488	SA 3	01 19 11.4	04 59 35	20.9	10.83	77 14	14.3	3.5	
	SB	19 14.5	05 00 16	16	-20.8	4020	-17.3	1.22	.38
514	SX 5	01 21 24.6	12 39 30	21.1	12.15	133 17	13.7	1.6	
	SC	21 25.9	39 57	16	-19.5	7080	-17.9	1.41	.28
524	LA	01 22 09.8	09 16 46	25.9	11.24	< 30	> 15.4	>4.1	
	SO				-20.8	<2410	> -16.7		

584	E4	01 28 50.7	-07 07 29	17.5	11.07	< 50	> 14.8	> 3.7		
	E4				-20.1	< 1830	> -16.4			
613	SB 4	01 31 58.8	-29 40 18	16.1	10.48	516	12.3	1.8		
	SBBC	01 31 59.7	8		-20.6	15900	-18.7	0.67	.10	
628	SA 5	01 34 00.6	15 31 36	8.24	9.50	162	13.5	4.0		
	SC	01 33 59.9	15		-20.1	1320	-16.1	0.62	.61	
660*	SB 1	01 40 21.0	13 23 18	10.0	10.52*					S
	SBA				-19.5					
720	E5	01 50 34.2	-13 59 06	17.4	10.92	< 40	> 15.0	> 4.1		
	E5				-20.3	< 1450	> -16.2			
772	SA 3	01 56 35.4	18 46 00	15.6	10.65	191	13.3	2.7		
	SB	01 56 34.1	46 20		-20.3	5580	-17.7	0.77	.32	
821	E6	02 05 40.8	10 45 30	18.2	11.51	< 30	> 15.4	> 3.8		
	E6				-19.8	< 1190	> -15.9			
864	SX 5	02 12 50.4	05 46 12	12.5	11.20	69	14.5	3.3		
	SC	02 12 49.9	46 26	17	-19.3	1280	-16.0	0.76	.18	
895	SA 6	02 19 06.4	-05 44 54	19.1	11.90	97	14.1	2.2		
	SCD	02 19 05.6	45 29	15	-19.5	4250	-17.3			
908	SA 5	02 20 46.2	-21 27 42	12.1	10.40	500*	12.3	1.9		
	SC	02 20 46.1	27 46		-20.0	8800	-18.1	0.69	.07	
936	LB	02 25 04.8	-01 22 42	14.5	10.78	< 60	> 14.6	> 3.8		
	SB0				-20.0	< 1530	> -16.2			
1022	SB 1	02 36 04.1	-06 53 32	15.1	11.85	< 70	> 14.4	> 2.6		C,P
	SBA				-19.0	< 1900	> -16.5			
0237-34	E0	02 37 50.4	-34 44 24	0.25:	8.84	< 310	> 12.8	> 4.0		N
	DE				-13.1	< 2.27	> -9.2			
1042	SX 6	02 37 56.4	-08 38 48	13.6	11.16	< 50	> 14.8	> 3.6		
	SCD				-19.5	< 1110	> -15.9			
1052	E4	02 38 37.2	-08 28 06	13.8:	11.26	660*	12.0	0.7		P
	E4	02 38 36.4	28 07		-19.5	15000	-18.7	0.35	.20	
1055	SB 3	02 39 11.4	00 13 42	12.2	10.81	600*	12.1	1.3		
	SB	02 39 11.7	13 40		-19.6	10700	-18.3	0.74	.12	

Table 1
(Continued)

N	Type	R.A.	Dec.	Dist. (Mpc)	MAG MABS	S (mJy) P*E18 (W/Hz)	RMAG RMABS	R408 -alpha	Note
1068	SA 3	02 40 07.2	-00 13 30	7.87	9.21	11700*	8.9	-0.3	
	SB	40 07.0	13 32		-20.3	86700	-20.6	0.61	
1073	SB 5	02 41 05.4	01 09 54	13.6	11.19	< 90	> 14.2	> 3.0	.03
	SB				-19.5	< 1980	> -16.5		
1084	SA 5	02 43 31.8	-07 47 06	18.2	10.79	540*	12.2	1.4	
	SC	43 31.3	47 31		-20.5	21400	-19.1	0.50	.01
1087	SX 5	02 43 51.6	-00 42 30	11.4	11.13	349	12.7	.1	
	SC	43 52.7	42 14	9	-19.2	5460	-17.6	0.88	.58
1090	SB 4	02 44 00.6	-00 27 24	18.1	12.03	< 30	> 15.4	> 3.3	
	SBBC				-19.3	< 1180	> -15.9		
1097	SB 3	02 44 11.4	-30 29 06	11.2	9.87	900*	11.7	1.8	
0255-54	SBBC	44 12.1	28 55		-20.4	13400	-18.5	0.66	.04
	SB 7	02 55 06	-54 48		10.99	NOT OBSERVED			
1179	SBD	03 00 21.0	-19 05 36	14.5	11.88	< 40	> 15.0	> 3.2	
	SCD				-18.9	< 999	> -15.8		
1187	SB 5	03 00 24.0	-23 03 48	15.2	10.63	167	13.5	.1	
	SBC	00 24.0	03 31	10	-20.3	4620	-17.4	2.9	.37
1201	LA	03 01 57.6	-26 15 54	12.6:	11.25	< 30	> 15.4	> 4.1	
	SO				-19.3	< 570	> -15.1		
1232	SX 5	03 07 30.0	-20 46 12	15.7:	10.19	78:	14.3	.2	
	SC	07 28.2	45 53		-20.8	2300	-16.7	4.1	
1291	SB0	03 15 28.5	-41 17 23	14	9.19	< 100	> 14.0	> 4.8	N
	SB0/A				-20.6	< 970	> -15.7		
1300	SB 4	03 17 25.2	-19 35 28	15.7	10.74	72:	14.4	.3	
	SBBC	17 22.6	35 32	17	-20.2	2120	-16.6	3.7	
1313	SB 7	03 17 39.0	-66 40 42	4.47	9.35	201	13.3	.1	
	SBD	17 44.8	40 19	11	-18.9	481	-15.0	4.0	
1302	SB0	03 17 42.6	-26 14 24	16.2	11.38*	< 30	> 15.4	0.06	
	SB0/A				-19.7	< 944	> -15.7	> 4.0	

1309	SA 4	03 19 46.9	.5	-15 34 49	20.0	11.68	181	18	13.4	.1	1.7	P
	SBC	19 47.5		34 26		-19.8	8700		-18.1		0.36	
1316	LX	03 20 46.8		-37 23 06	16.3	9.47	249000*		5.6		-3.9	
	S0	(03 20 47.6)		(-37 23 09)		-21.7	7910000		-25.5		0.65	.10
1326	LB	03 22 01.2		-36 38 24	15.9:	11.02	129	17	13.8	.2	2.8	
	SBO	22 02.5	.8	38 42	12	-20.0	3900		-17.2			
1332	L	03 24 03.9		-21 30 32	14.7	10.84	< 60		> 14.6		> 3.8	
	S0					-20.0	< 1560		> -16.2			
1344	E5	03 26 18.0		-31 14 30	17.5	11.02	< 45		> 14.9		> 3.9	
	E5					-20.2	< 1640		> -16.3			
1350	SB 2	03 29 10.2		-33 47 54	20.0:	11.03	< 30		> 15.4		> 4.4	
	SBAB					-20.5	< 1440		> -16.1			
1353	SB 3	03 29 49.8		-20 59 12	24.2	11.72	< 30		> 15.4		> 3.6	P
	SBB					-20.2	< 2100		> -16.5			
1365	SB 3	03 31 42.0		-36 18 18	8.71	9.78	1300*		11.3		1.5	
	SBB	31 41.2		18 20		-19.9	11800		-18.4		0.71	
1371*	SX 1	03 32 52.8		-25 05 54	14.5	11.50*						
	SA					-19.3	< 30		> 15.4		> 4.6	
1380	LA	03 34 31.2		-35 08 24	15.9:	10.81	< 907		> -15.6			
	S0					-20.2						
1385	SB 6	03 35 19.8		-24 39 54	17.7	11.30	340*		12.7		1.4	P
	SBCD	35 17.9		39 55		-19.9	12700		-18.5		0.46	
1395	E2	03 36 19.2		-23 11 24	15.9:	10.85	< 40		> 15.0		> 4.2	.17
	E2					-20.2	< 1210		> -16.0			
1399	E1	03 36 34.8		-35 36 42	15.9:	10.60	1400*		11.2		0.6	N
	E1	36 34.5		36 34		-20.4	42400		-19.8			
1398	SB 2	03 36 45.3		-26 29 59	15.9	10.30	35: 15		15.2	.8	4.9	
	SBAB	36 45.1	2.0	30 23	32	-20.7	1060		-15.8			
1404	E1	03 36 57.1		-35 45 21	15.9:	11.00	< 100		> 14.1		> 3.1	C,P
	E1					-20.0	< 3020		> -16.9			
1400	LA	03 37 15.6		-18 50 54	15.9:	11.80	< 40		> 15.0		> 3.2	P
	S0					-19.2	< 1210		> -16.0			
1407	E0	03 37 57.0		-18 44 24	15.9:	10.85	280*		12.9		2.1	P
	E0	37 55.8		44 20		-20.5	8420		-18.1		0.77	.46
1421	SX 4	03 40 09.0		-13 38 54	29.2	11.35	192	16	13.3	.1	2.0	P
	SBC	40 09.2	.4	38 46	8	-21.0	19600		-19.0		0.51	.13

Table 1 (Continued)

N	Type	R.A.	Dec.	Dist. (Mpc)	MAG MABS	S (mJy) P*E18 (W/Hz)	RMAG RMABS	R408 -alpha	Note
1433	SB 1	03 40 27.0	-47 22 48	22.9	10.39	< 70	> 14.5	>4.1	
	SBA				-21.4	<4130	>-17.3		
1448	SA 6	03 42 52.8	-44 48 00	11.2	10.63	286	12.9	2.3	
	SCD	42 52.7	48 09	9	-19.6	4270	-17.3	.1	
1518	SB 8	04 04 37.8	-21 18 42	15.1	11.80	< 30	> 15.4	>3.6	P
	SBDM				-19.1	< 818	>-15.5		
1532	SB 2	04 10 10.2	-33 00 06	19.5	10.98	105	14.0	3.0	
	SBAB	10 07.9	00 11	12	-20.5	4780	-17.5	.2	
1549	E0+	04 14 39.0	-55 42 54	13.8:	10.54	< 40	> 15.0	>4.5	
	E0-1				-20.2	< 911	>-15.7		
1553	LA	04 15 05.4	-55 54 08	10.5:	10.09	< 50	> 14.8	>4.7	C
	SO				-20.0	< 660	>-15.3		
1559	SB 6	04 17 01.2	-62 54 18	17.4:	10.50	700*	12.0	1.5	
	SBOD	17 01.1	54 18		-20.8	25400	-19.2		
1566	SX 4	04 18 52.8	-55 03 24	6.79:	9.88	700*	12.0	2.1	
	SBC	18 52.6	03 56		-19.3	3860	-17.2	0.72	
1617	SB 1	04 30 33.0	-54 42 24	17.4:	10.77	< 50	> 14.8	>4.0	
	SBA				-20.4	<1810	>-16.4		
1637*	SX 5	04 38 57.6	-02 57 06	6.38	11.02				
	SC				-18.0				
1672	SB 3	04 44 55.2	-59 20 12	11.3	10.62	700*	12.0	1.4	
	SBB	44 53.8	20 01		-19.7	10700	-18.3	0.69	.13
1744	SB 7	04 57 55.5	-26 05 40	8.13	11.26	< 45	> 15.0	>3.7	
	SBD				-18.3	< 359	>-14.7		
1792	SA 4	05 03 30.0	-38 02 42	10.0	10.40	600*	12.1	1.7	
	SBC	03 31.9	02 58		-19.7	7180	-17.9		
1808	SX 1	05 05 58.8	-37 34 42	7.6	10.24	1400*	11.2	1.0	
	SA	05 58.6	34 38		-19.2	9680	-18.2	0.74	.004
1964	SX 3	05 31 14.4	-21 58 54	15.2	10.91	200	13.3	2.4	
	SB	31 15.6	58 32	9	-20.0	5540	-17.6	0.72	.09

2207	SX 4	06	14	14.4	-21	21	12	19.6	10.81	1200*	11.4	0.6	C
	SBC	14	14.2		21	14			-20.7	55100	-20.1	0.88	
2217	LB	06	19	40.0	-27	12	29	15.9:	10.94	69	14	3.6	
	SBO	19	37.8				15		-20.1	2070	-16.5	.2	
2223	SX 3	06	22	30.0	-22	48	36	16.4	11.52	187:	17	1.9	
	SB	22	28.6				9		-19.6	6000	-17.7	.1	C
2427	SX 8	07	35	02.0	-47	31	31	9.04	11.24	< 70	> 14.4	>3.2	
	SDM								-18.5	< 684	> -15.4		
2442/3	SB 3	07	36	33.0	-69	25	00	14.4	10.41	900*	11.7	1.3	
	SBB	36	32.1		25	06			-20.4	22300	-19.1		
2525	SB 5	08	03	15.6	-11	17	06	12.7	11.48	86	14	2.7	C
	SBC	03	15.9				13		-19.0	1650	-16.3	.2	
2613	SA 3	08	31	10.8	-22	48	00	15.7	10.13	111	14	3.8	
	SB	31	12.4				10		-20.9	3270	-17.1	.2	
2775*	SA 2	09	07	40.8	07	14	30	9.6	10.85				
	SAB								-19.1	< 30	> 15.4	>4.7	C
2784	LA	09	10	06.0	-23	57	54	10.5:	10.68	< 396	> -14.7	3.3	
	SO								-19.4	133	16		
2835	SB 5	09	15	36.9	-22	08	37	10.5:	10.37	1740	-16.4	.2	
	SBC	15	38.1				11		-19.7				
2967	SA 5	09	39	29.9	00	33	53	15.9	12.01	259:	20	1.0	S
	SC	39	27.8				10		-19.0	7830	-18.0	.1	
2974	E4	09	40	01.8	-03	28	06	17.9	11.46	< 250	> 13.1	>1.6	
	E4								-19.8	<9540	> -18.2		
2997	SX 5	09	43	27.6	-30	57	36	7.41	9.74	700*	12.0	2.3	
	SC	43	29.2						-19.6	4600	-17.4		N
3059	SB 4	09	49	39.0	-73	41	12	9.55	10.80	600*	12.1	1.3	
	SBC	49	33.1						-19.1	6550	-17.8		
3109	SB 9	10	00	46.8	-25	54	48	2.00	9.53	< 100	> 14.0	>4.5	
	SBM								-17.0	< 47.2	> -12.5		
3115	L	10	02	44.4	-07	28	30	6.43	9.65	< 70	> 14.4	>4.8	C
	SO								-19.4	< 331	> -14.6		
3136	E4	10	04	31.2	-67	08	00	14.1	10.08	< 30	> 15.4	>5.3	
	E4								-20.7	< 717	> -15.4		
1005+12	E3	10	05	46.2	12	33	12		10.61	< 250	> 13.1	>2.5	
	E3												C

Table 1
(Continued)

N	Type	R.A.	Dec.	Dist. (Mpc)	MAG MABS	S (mJy) P+E18 (W/Hz)	RMAG RMABS	R408 -alpha	Note
3145	SB 4 SBBC	10 07 43.2 07 44.2	-12 11 18 11 38	28.2	11.88 -20.4	98 9310	14.1 -18.2	2.2	
3166	SX 0 SO/A	10 11 09.6 11 09.1	03 40 30 39 51	12.0	11.07 -19.3	123 2130	13.8 -16.6	2.7 0.73	.14
3169	SA 1 SAP	10 11 37.8 11 39.1	03 43 12 43 01	10.5	10.93 -19.2	183 2420	13.4 -16.7	2.5 0.51	.20
3223	SA 3	10 19 19.8	-34 00 48	10.2	11.13 -18.9	< 30 < 376	> 15.4 > -14.6	> 4.3	
3239	SB IB 9 IBM	10 22 23.4	17 24 48	7.9:	11.31* -18.2	< 60 < 448	> 14.6 > -14.9	> 3.3	
3256	P	10 25 42.0	-43 38 54	25.9	11.03 -21.0	1450* 117000	11.2 -20.9	0.2 0.61	.04
3261	SBB SB 3	25 42.8 10 26 53.3	38 40 -44 24 02	22.8	12.16* -19.6	232 14400	13.1 -18.7	0.9	
3338	SBB SA 5	26 53.7 10 39 28.8	23 43 14 00 36	9	11.02 -19.9	41: 14 1100	15.0 -15.9	4.0	
3346	SC SB 6	39 28.4 10 40 59.4	00 48 15 08 06	34	12.18* -19.2	< 30 < 1270	> 15.4 > -16.0	> 3.2	P
3351*	SBCD SB 3 SBB	10 41 19.2	11 58 06	8.24	10.22 -19.4				
3367*	SB 5	10 43 55.8	14 00 48	27.9	11.85 -20.4				S,P
3368	SBC SX 2	10 44 08.6	12 05 02	7.9:	9.80 -19.7	< 190 < 1420	> 13.4 > -16.1	> 3.6	
3370	SAB SA 5	10 44 23.4 44 22.4	17 32 18 32 55	11	11.94 -19.3	189 7020	13.4 -17.8	1.5 1.22	.14
3377	SC E5	10 45 03.0	14 15 00	8.7:	10.87 -18.8	< 40 < 362	> 15.0 > -14.7	> 4.2	
3379	E5 E1 E1	10 45 11.4	12 50 48	9.1	10.00 -19.8	< 45 < 446	> 14.9 > -14.9	> 4.9	

3384	LB	10 45 38.4	12 53 42	9.1	10.64 -19.2	< 30 < 297	> 15.4 > -14.4	> 4.8		
3389	SB0	10 45 49.8	12 47 54	16.9	12.06 -19.1	79 2700	14.3 -16.8	2.2 0.63	P	
3412	SC	10 45 49.6	47 59 13	7.68	-11.15 -18.3	< 40 < 282	> 15.0 > -14.4	> 3.9	.17	
3423	SB0	10 48 15.0	13 40 30	13.8	-11.34 -19.4	87 1980	14.2 -16.5	2.9	S	
3489	SA 6	10 48 38.4	06 06 18	7.2	-10.87 -18.4	< 30 < 186	> 15.4 > -13.9	> 4.5		
	SCD	48 39.1	06 27 14							
	LX	10 57 40.8	14 10 12							
	S0									
3511	SA 5	11 00 57.0	-22 49 00	10.2	11.01 -19.1	192 2400	13.3 -16.8	2.3		
3521	SC	00 57.1	48 58 10	8.43	-9.56 -20.3	2600* 22100	10.5 -19.1	0.9		
3557	SBC	11 03 15.6	13 25	19.1	-10.91 -20.5	1500* 65500	11.1 -20.3	0.98 0.2	.12	
3585	E3	11 07 36.0	16 02	12.0	-10.79 -19.6	< 60 < 1030	> 14.6 > -15.8	0.68 > 3.8	.01	P
3593	E7	11 10 49.8	-26 28 48		11.24 -18.0	194 1110	13.3 -15.9	2.1		
	SA 0	11 12 00.0	13 05 24	6.9				.1		
	S0/A	11 59.1	06 16 12							
3596	SX 5	11 12 28.8	15 03 36	15.4	11.42 -19.5	62 1750	14.6 -16.3	3.2		
3607	SC	12 29.4	03 20 24	18.2	-10.76 -20.5	< 30 < 1190	> 15.4 > -15.9	> 4.6		
3608*	LA	11 14 16.8	18 19 42							
3621	S0	11 14 21.0	18 25 36	20.0	-11.70 -19.8					
3621	E2	11 15 50.4	-32 32 24	5.75	9.51 -19.3	500* 1980	12.3 -16.5	2.8 0.67		
3623	SA 7	15 51.7	32 47	7.2	-9.66 -19.6	< 55 < 343	> 14.7 > -14.6	> 5.0		
	SD	11 16 18.6	13 21 54							
	SX 1									
	SA									
3626	LA	11 17 26.4	18 37 48	14.5	11.41 -19.4	< 30 < 755	> 15.4 > -15.4	> 4.0		
3627	S0	11 17 38.4	13 15 48	6.85	-9.30 -19.9	700* 3930	11.9 -17.3	2.6 0.54		
3628	SB	17 37.8	15 40						.17	
	S 3	11 17 39.6	13 52 06	7.91	9.63 -20.0	900* 6740	11.7 -17.8	2.1 0.49		
	SB	17 39.2	52 15					.12		

Table 1
(Continued)

N	Type	R.A.	Dec.	Dist. (Mpc)	MAG MABS	S (mJy) P×E18 (W/Hz)	RMAG RMABS	R408 -alpha	Note
3640	E3	11 18 32.4	03 30 36	13.2:	11.01	125:	13.8	.2	2.8
	E3	11 18 35.3	30 18		-19.6	2610	-16.8		
3672	SA 5	11 22 30.6	-09 31 12	18.2	11.23	163	13.5	.1	2.3
	SC	22 30.5	31 17	10	-20.1	6460	-17.8		
3686	SB 4	11 25 07.3	17 30 00	14.3	11.76	35:	15.2	.6	3.5
	SBBC	25 06.9	30 42	43	-19.0	859	-15.6		
3705	SX 2	11 27 32.0	09 33 10	11.7	11.77*	46	14.9	.4	
	SAB	27 22.6	34 04	28	-18.5	753	-15.4		.35
3810	SA 5	11 38 24.0	11 44 54	12.5	11.06	340*	12.7		1.6
	SC	38 21.8	47 47		-19.4	6330	-17.8		0.91
3887	SB 4	11 44 32.4	-16 34 38	16.0	11.25	68	14.5	.2	3.3
	SBBC	44 32.1	34 21	13	-19.8	2080	-16.5		
3923	E4	11 48 30.0	-28 31 42	15.9	10.79	< 35	> 15.2		>4.4
	E4-5				-20.2	<1060	> -15.8		
3962	E1	11 52 06.6	-13 41 48	16.0	11.27	< 30	> 15.4		>4.1
	E1				-19.8	< 919	> -15.6		
3976	SX 3	11 53 23.4	07 01 42	23.6	11.74	< 50	> 14.8		>3.1
	SB 8	11 56 56.4	-18 59 24	8.91:	-20.1	<3320	> -17.1		
4027	SBDM	56 56.8	59 02	8	11.30	210	13.2	.1	1.9
	SBDM				-18.5	2000	-16.6		
4030	SA 4	11 57 49.8	-00 49 24	16.0	10.76	330*	12.7		1.9
	SB	57 49.6	48 36		-20.3	10100	-18.3		0.69
4038/9	P	11 59 19.2	-18 35 06	13.2:	10.21	1300*	11.3		1.1
	IM	59 19.8	35 38		-20.4	27100	-19.3		0.88
4050	SB 2	12 00 20.4	-16 05 36	28.3	12.25*	< 30	> 15.4		>3.1
	SBAB				-20.0	<2880	> -16.9		
4116	SB 8	12 05 03.6	02 58 12	12.9	12.01	< 40	> 15.0		>3.0
	SBDM				-18.5	< 794	> -15.5		
4123*	SB 5	12 05 37.8	03 09 24	12.0	11.53				
	SB				-18.9				

I 764	SA 5	12 07 39.0	-29 27 30	10.1	12.35*	< 50	> 14.8	> 2.5	
4179	SC	12 10 18.6	01 37 42	12.3	-17.7	< 609	> -15.2	> 3.5	
4192	SO	12 11 15.6	15 10 48	11.5	-19.1	< 905	> -15.6	2.7	
4216	SAB	11 14.3	11 08	12	-20.0	3640	-13.1	.1	
4254	SX 3	12 13 21.4	13 25 46	14.6	-20.32	< 90	> -17.2	> 3.9	C
	SB	12 16 17.4	14 41 42	12.8	-20.5	< 2320	> -16.7	0.7	
	SC	16 15.6	42 13		-20.3	1800*	> -10.9	1.14	.19
						35100	-19.6		
4261	E2	12 16 50.4	06 06 06	26.3	11.09	35300*	7.7	-3.4	
4273	E2-3	(LARGE DOUBLE)	05 37 18	19.9	-21.0	2920000	-24.4	0.73	.06
4281	SB 5	12 17 22.8	05 39 54	31.6:	-12.04	< 50	> 14.8	> 2.8	P
4303	SBC	12 17 48.6	05 39 54	12.9	-19.4	< 2360	> -16.7	> 3.6	P
4321	SO	12 19 21.6	04 45 06	12.1	11.78	< 30	> 15.4	1.5	S
	SX 4	19 22.0	45 27		-20.7	< 3580	> -17.1	1.01	
	SBC	12 20 22.8	16 06 00		-20.6	1200*	-11.4	2.0	
	SX 4	20 23.4	06 04		9.88	24000	-19.2	0.99	.18
	SBC				-20.5	700*	11.9		
4365	E3	12 21 55.6	07 35 37	14.5	10.29	12300	-18.5	> 3.9	C
4374	E3	12 22 31.2	13 09 48	14.5	-20.5	< 90	> 14.2	-1.3	
4378	E1	22 32.5	09 38	30.8	-20.7	< 2250	> -16.6	0.62	.02
4382	SA 1	12 22 45.0	05 12 06	11.0:	-20.28*	307000	8.8	> 3.1	
4406	SA	12 22 52.4	18 28 00	11.5:	-20.2	< 30	> 15.4	4.6	
	LA	22 50.4	28 33		9.81	< 3400	> -17.0	.3	
	SO	12 23 39.6	13 13 24		-20.4	73: 16	14.4	> 3.7	
	E3				9.89	1060	-15.8		
	E3				-20.4	< 150	> 13.6		
						< 2420	> -16.7		
4429	L	12 24 54.0	11 23 06	12.6:	10.74	< 45	> 14.9	> 4.2	
4438	SO	12 25 13.8	13 17 06	7.94:	-19.8	< 855	> -15.6	1.5	
4442	SA 0			14.5:	10.45	700*	11.9	1.08	.14
	SO/A				-19.1	5280	-17.6	> 3.6	
	LB	12 25 31.8	10 04 42		-11.04	< 60	> 14.6		
	SBO				-19.8	< 1510	> -16.2		

Table 1
(Continued)

N	Type	R.A.	Dec.	Dist. (Mpc)	MAG MABS	S (mJy) P×E18 (W/Hz)	RMAG RMABS	R408 -alpha	Note
4450	SA 2	12 25 58.2	17 21 42	11.5:	10.61	< 70	> 14.4	>3.8	
4457*	SAB	12 26 25.8	03 50 48	6.46	-19.7	<1110	>-15.9		
	S0/A				11.38				
4472	E2	12 27 14.4	08 16 42	11.5	9.09	700*	11.9	2.8	
4473*	E2	27 11.7	16 43		-21.2	11000	-18.4	0.73	.20
	E5	12 27 17.4	13 42 19	12.0:	10.85				
	E5				-19.5				
4486	E+0	12 28 17.4	12 40 06	14.5:	9.35	580000*	4.6	-4.8	
	E0-1	28 17.6	40 22		-21.5	14500000	-26.2	0.77	.03
4487	SX 6	12 28 29.4	-07 46 42	11.2	11.34	< 40	> 15.0	>3.7	
4496A	SCD	12 29 06.6	04 12 54	9.73	-18.9	< 602	>-15.2		
	SB 9				11.43	103	14.0	2.6	
4501	SBM	29 07.8	13 08	14	-18.5	1170	-15.9		
	SA 3	12 29 27.6	14 14 42	15.0	9.86	1200*	11.3	1.4	
	SB				-21.0	32300	-19.6	1.22	.07
4504	SA 6	12 29 42.4	-07 17 14	13.1	11.59	41:	15.0	3.4	
4517	SCD	29 41.1	16 39	42	-19.0	837	-15.6		
	SA 6	12 30 12.0	00 23 18	7.48	10.41	< 250	> 13.0	>2.6	
	SCD				-19.0	<1670	>-16.4		
4526	LX	12 31 30.6	07 58 30	15.9:	10.21	< 75	> 14.4	>4.2	C
4527	S0	12 31 35.4	02 55 42	11.8	-20.8	<2170	>-16.6		
	SX 4				10.77	539	12.2	1.4	
4532	SBC	31 34.6	55 55	10	-19.6	8980	-18.2	0.78	.08
	IB 9	12 31 46.8	06 44 42	8.51	11.75	290*	12.9	1.2	
	IBM	31 46.7	44 24		-17.9	2510	-16.8		
4535	SX 5	12 31 48.0	06 28 36	9.68	10.22	209	13.3	3.1	
	SC	31 49.6	28 41	12	-19.7	2340	-16.6	0.88	.44
	SX 4	12 31 54.0	02 27 42	9.55	10.54	800*	11.8	1.3	
4536	SBC	31 52.4	27 33		-19.4	8730	-18.1	1.04	.15

4546	LB	12 32 55.2	-03 31 06	33.1	11.09	< 30	> 15.4	> 4.3	
4548	SB0	12 32 55.2	14 46 24	10.5	-21.5	< 3930	> -17.2		
4552*	SBB	12 33 08.5	12 49 50	15.1	-19.4		NOT OBSERVED		
4569	E0	12 34 19.3	13 26 20	6.9	-20.3	454	12.4	.1	C
4570	SX 2	34 18.3	25 26	11	-9.82	2590	-16.8		
	SAB	12 34 21.0	07 31 24	11.5	-11.27	< 40	> 15.0	> 3.8	
	L				-19.0	< 633	> -15.3		
	S0								
4579	SX 3	12 35 12.0	12 05 36	14.5	10.28	500*	12.3	2.0	
4592	SB	35 11.9	04 52		-20.5	12500	-18.5	0.83	.14
	SA 8	12 36 44.4	-00 15 24	11.3	12.16*	< 50	> 14.8	> 2.6	
	SDM				-18.1	< 767	> -15.5		
4593*	SB 3	12 37 04.8	-05 04 12	21.0	11.39				S
	SBB				-20.2				
4594	SA 1	12 37 23.8	-11 20 51	9.77	8.76	107	16	5.2	
	SA	37 21.2	20 35	14	-21.2	1220	-16.0	0.06	.40
4602*	SX 4	12 38 01.8	-04 51 30	22.7	11.78				
	SBC				-20.0				
4621	E5	12 39 31.2	11 55 12	12.6	10.60	< 45	> 14.9	> 4.3	
4632	E5				-19.9	< 855	> -15.6		
	SA 5	12 39 58.2	00 11 24	19.2	11.77	63	16	.3	P
	SC	39 59.8	11 31	16	-19.6	2790	-16.8		
4636	E0	12 40 17.4	02 57 42	11.5	10.27	222	20	.1	
	E0-1	40 16.5	57 57	11	-20.0	3500	-17.1	2.9	.39
4643	SB0	12 40 47.4	02 15 06	15.9:	11.25	< 100	> 14.1	> 2.8	
	SB0/A				-19.8	< 3020	> -16.9		
4649	E2	12 41 09.3	11 49 37	15.1	9.61	41	19	.7	5.4
	E2	41 07.3	50 10	55	-21.3	1120	-15.9		
4651	SA 5	12 41 12.6	16 40 06	19.2	11.03		NOT OBSERVED		
4658	SC				-20.4				
	SB 4	12 42 02.4	-09 48 42	22.1	12.74*	93	18	.3	P
	SBBC	42 02.7	48 31	13	-19.0	5430	-17.6		
4665	SB0	12 42 27.0	03 19 48	15.1	11.43*	< 30	> 15.4	> 3.9	
	SB0/A				-19.5	< 818	> -15.5		

Table 1 (Continued)

N	Type	R.A.	Dec.	Dist. (Mpc)	MAG MABS	S (mJy) P*E18 (W/Hz)	RMAG RMABS	R408 -alpha	Note
4666	SX 5	12 42 34.8	-00 11 12	18.3	10.98	730*	11.9	0.9	
	SC	42 34.5	11 05		-20.3	29200	-19.4	0.52	
4684	LB	12 44 43.3	-02 27 13	18.8	12.27*	< 50	> 14.8	>2.5	.08
	SB0				-19.1	<2110	> -16.6		S,P
4697*	E6	12 46 00.6	-05 31 42	10.0:	9.96				
	E6				-20.0				
4696	E1	12 46 03.0	-41 02 18	31.6	11.22	12000*	8.8	-2.4	
	E1	46 03.1	02 22		-21.3	1440000	-23.7		
4699	SX 3	12 46 26.4	-08 23 36	14.1	10.15	52: 16	14.8	4.6	S
	SB	46 27.0 1.3	23 14 24		-20.6	1240	-16.0		
4713	SX 7	12 47 25.2	05 35 00	10.3	11.88	116 16	13.9	2.0	P
	SD	47 25.8	34 47 10		-18.2	1470	-16.2	0.70	.11
4731*	SB 6	12 48 25.8	-06 07 18	8.17	11.14				
	SB0				-18.4				
4742	E4	12 49 12.0	-10 11 00	11.7	11.85	< 40	> 15.0	>3.2	P
	E4				-18.5	< 654	> -15.3		
4753	I0	12 49 48.0	-00 55 42	11.4	10.40	< 30	> 15.4	>5.0	
	I0				-19.9	< 465	> -14.9		
4762	LB	12 50 25.4	11 30 09	9.1:	10.68	< 68	> 14.5	>3.8	
	SB0				-19.1	< 675	> -15.3		
4772	SA 1	12 50 55.9	02 26 21	12.6	12.40*	< 50	> 14.8	>2.4	P
	SA				-18.1	< 950	> -15.7		
4775	SA 7	12 51 10.8	-06 21 12	12.2	11.49	79 18	14.3	2.8	P
	SD	51 09.4	21 27 15		-18.9	1410	-16.1		
4781*	SB 7	12 51 46.8	-10 15 54	11.6	11.26				
	SB0				-19.1				
4818	SX 2	12 54 12.6	-08 15 12	9.9	11.89*	72 15	14.4	2.5	
	SAB	54 12.6	15 30 16		-18.1	844	-15.6		
4845	SA 2	12 55 28.1	01 50 48	14.5	12.17*	193 19	13.3	1.1	S
	SAB	55 27.4 .5	51 37 12		-18.6	4830	-17.5	0.98	.25

4856	SB0	12 56 42.0	-14 46 18	14.1:	10.89 -19.9	< 30 < 717	> 15.4 > -15.4	> 4.5	
4900	SB0/A	12 58 06.0	02 46 08	16.4	11.84	72	18	2.6	P
4902	SBC	58 07.0	46 31	30.3	-19.2	2310	19	0.46	.18
4941	SB3	12 58 21.7	-14 14 41	10	-19.56	207	13.3	1.7	
4939*	SBB	58 23.3	15 14	9.20	-20.9	22800	19.1	> 3.5	
	SX 2	13 01 37.5	-05 16 58	15.9:	11.59	< 40	> 15.0		
	SAB	13 01 37.8	-10 04 24		-18.2	< 405	> -14.8		
	SA 4				-11.56*				
	SBC				-19.4				
4945	SB 6	13 02 31.8	-49 12 00	3.89:	8.25	12600*	8.8	0.6	
4958	SBCD	02 33.1	11 53	15.2	-19.7	22800	-19.2	0.46	.05
4976	LB	13 03 12.0	-07 45 06	11.4	10.96	< 30	> 15.4	> 4.4	
4981	SB0	13 05 42.0	-49 14 30	19.1	-19.9	< 829	> -15.5	> 4.6	
4984	E4	13 06 13.2	-06 30 48	11.0	10.48	< 40	> 15.0	> 2.8	P
	E4				-19.9	< 622	> -15.4		
	SX 4				11.52	< 80	> 14.3		
	SBC				-19.9	< 3470	> -17.1		P
	LX	13 06 18.4	-15 14 58		11.84*	90	14.1	2.3	
	S0	06 17.7	14 25 12		-18.3	1300	-16.1	0.47	.21
4995	SX 3	13 07 04.2	-07 34 00	15.6	11.54	< 60	> 14.6	> 3.1	P
5018	SB	13 10 19.8	-19 15 12	31.3	-19.4	< 1750	> -16.4	> 3.9	P
5044*	E3	13 12 43.8	-16 07 18	25.0	11.49	< 30	> 15.4		P
5054	E0	13 14 18.0	-16 22 18	14.5	-21.0	< 3520	> -17.1		P
5061	SA 4	14 17.4	22 22 10	19.7	11.88*				
	SBC	13 15 20.4	-26 34 24		-20.4	164	17	2.5	
	E0				11.04	4100	13.5	0.42	.18
					-19.8	< 60	-17.3	> 3.0	P
					11.61*	< 2790	> 14.6		
					-19.9		> -16.9		
5068	SX 6	13 16 16.8	-20 46 36	5.55	10.21	< 165	> 13.6	> 3.3	
5085	SCD	13 17 34.2	-24 10 42	15.1	-18.5	< 607	> -15.1		S
5084	SA 5	17 31.8	10 51 16	15.4	11.94*	74:	18	2.4	
	SC	13 17 34.3	-21 33 54		-19.0	2010	-16.5		S
	L	17 35.6	33 44 28		11.97*	41:	15	3.0	
	S0				-19.0	1160	-15.9		

Table 1
(Continued)

N	Type	R.A.	Dec.	Dist. (Mpc)	MAG MABS	S (mJy) P×E18 (W/Hz)	RMAG RMABS	R408 -alpha	Note
5087	LA	13 17 42.6	-20 20 54	16.4	11.67	56: 18	14.7	.4	P
5102	SO	17 41.1	20 37		-19.4	1800	-16.4		
	LA	13 19 07.2	-36 22 06	2.7	9.81	< 195	> 13.4	> 3.6	
	SO				-17.3	< 170	> -13.8		
5128	L	13 22 31.8	-42 45 30	3.28	7.27	274000*	3.0	-4.3	
	SO		A		-20.2	353000	-24.6		
5161	SA 5	13 26 24.0	-32 54 54	9.55	11.34	65	14.5	.3	
	SC	26 23.1	54 50	14	-18.6	709	-15.4		
5170	SA 5	13 27 07.2	-17 42 24	14.0	11.97*	< 30	> 15.4	> 3.4	S
	SC				-18.8	< 704	> -15.3		
5236	SX 5	13 34 10.2	-29 36 48	4.21	7.84	6200*	9.6	1.8	
	SC	34 10.5	36 26		-20.3	13200	-18.5	0.92	.09
5248	SX 4	13 35 03.0	09 08 30	9.95	10.36	700*	11.9	1.5	
	SBC	35 03.2	09 39		-19.6	8290	-18.1	1.25	.16
5247	SA 4	13 35 20.6	-17 37 49	15.6	10.80	168	13.5	.1	
	SBC	35 20.8	37 07	10	-20.2	4870	-17.5		
5253	IO	13 37 05.4	-31 23 24	2.16	10.44	128	13.8	.1	
	IO	37 05.5	23 14	11	-16.2	71.5	-13.0		
5266	LA	13 39 54	-47 56	29.2	12.25*	< 40	> 15.0	> 2.8	
	SO				-20.1	< 4080	> -17.2		
5300*	SX 5	13 45 44.4	04 11 54	16.2	11.93*				
	SC				-19.1				
5334	SB 5	13 50 20.4	-00 52 06	8.79	11.90*	< 30	> 15.4	> 3.5	
	SBC				-17.8	< 277	> -14.3		
5363*	IO	13 53 36.6	05 30 00	14.8	10.80				
	IO				-20.1				
5364	SA 4	13 53 41.4	05 15 36	10.7	10.70	66: 14	14.5	.3	
	SBC	53 39.7	15 29	20	-19.5	907	-15.7		
5427	SA 5	14 00 48.6	-05 47 30	26.7	11.79	250	13.1	.1	P
	SC	00 50.4	47 44	8	-20.3	21300	-19.0	1.3	

5468	SX 6	14 03 57.6	-05 12 48	19.1	11.96	< 40	> 15.0	> 3.0	P
	SCD				-19.4	<1750	>-16.4		
5483	SA 5	14 07 19.2	-43 05 12	16.9	11.46	< 60	> 14.6	> 3.1	
	SC				-19.7	<2050	>-16.5		
1409-65*	SA 3	14 09 18	-65 06	2.56	8.62				
	SB				-18.4				
5530	SA 4	14 15 18.0	-43 09 42	11.9	11.19	50: 16	14.8 .4	3.6	S
	SBC	15 17.4	09 12 23		-19.2	841	-15.6		
5566	SB 2	14 17 49.3	04 09 51	15.2	10.81	< 50	> 14.8	> 4.0	C
	SBAB				-20.1	<1380	>-16.1		
5576	E3	14 18 32.4	03 29 54	14.5	11.47	< 50	> 14.8	> 3.3	
	E3				-19.3	<1260	>-16.0		
5584	SX 6	14 19 50.2	-00 09 39	13.6	11.60	< 40	> 14.8	> 3.2	
	SCD				-19.1	< 879	>-15.9		
5643	SX 5	14 29 28.2	-43 57 12	7.55	10.12	600*	12.1	2.0	
	SC	29 28.6	57 06		-19.3	4090	-17.3		
5669	SX 6	14 30 17.5	10 06 40	11.8	11.65	< 30	> 15.4	> 3.7	
	SCD				-18.7	< 500	>-15.0		
5668	SA 7	14 30 54.0	04 40 12	18.7	11.84	31: 14	15.3 .7	3.5	S
	SD	30 52.5	40 17 38		-19.5	1300	-16.1		
5701	SB0	14 36 41.4	05 34 48	15.1:	11.93*	< 40	> 15.0	> 3.1	
	SB0/A				-19.0	<1090	>-15.9		
5713	SX 4	14 37 37.8	-00 04 30	16.6:	11.66	358 24	12.7 .1	1.0	P
	SBC	37 37.6	04 31		-19.4	11800	-18.4	0.57 .10	
5728	SX 1	14 39 36.6	-17 02 24	28.2	12.39*	138 15	13.7 .1	1.3	P
	SA	39 37.2	02 26		-19.9	13200	-18.6	0.26 .58	
5746	SX 3	14 42 23.3	02 09 56	19.1:	10.72	< 90	> 14.2	> 3.5	C
	SB				-20.7	<3790	>-17.2		
5775	SB 5	14 51 27.0	03 44 48	15.6	11.49	520*	12.3	0.8	
	SBC	51 25.3	45 16		-19.5	15200	-18.7	0.72 .05	
5792	SB 3	14 55 48.0	-00 53 24	14.3	11.05	152: 20	13.6 .2	2.5	
	SB8	55 46.5	53 13		-19.7	3730	-17.2		
5813	E1	14 58 39.0	01 53 54	15.1:	11.30	< 50	> 14.8	> 3.5	
	E1				-19.6	<1360	>-16.1		
5838	LA	15 02 54.0	02 17 36	17.4	11.37	< 40	> 15.0	> 3.7	
	SO				-19.8	<1440	>-16.2		

Table 1 (Continued)

N	Type	R.A.	Dec.	Dist. (Mpc)	MAG MABS	S (mJy) P*E18 (W/Hz)	RMAG RMABS	R408 -alpha	Note
5846	E0	15 03 56.4	01 47 48	15.9	10.84	45: 14	14.9	4.1	
	E0-1	03 56.9	48 01	26	-20.2	1360	-16.1		
5850*	SB 3	15 04 35.4	01 44 12	25.0	11.34				
	SBB				-20.6				
5861*	SX 5	15 06 33.0	-11 08 00	18.7	11.77				P
	SC				-19.6				
5885	SX 5	15 12 21.6	-09 54 00	9.95	11.96*	34: 14	15.2	.6	
	SC	12 21.1	53 55	29	-18.0	403	-14.8	3.2	
5921	SB 4	15 19 27.4	05 14 53	9.59	11.07	< 50	> 14.8	> 3.7	C
	SBBC				-18.8	< 550	> -15.1		
5962	SA 5	15 34 14.4	16 46 24	25.1	11.69	184	13.4	1.7	P
	SC	34 14.5	46 43	9	-20.3	13900	-18.6	0.63	.07
5970	SB 5	15 36 08.4	12 21 00	21.0	11.73	123	13.8	2.1	P
	SBC	36 06.6	20 41	11	-19.9	6480	-17.8	1.32	.33
6215	SA 5	16 46 48.0	-58 54 18	9.08	9.97	800*	11.8	1.8	P
	SC	46 45.0	54 18		-19.8	7890	-18.0		
6221	SB 5	16 48 25.2	-59 08 00	9.59	9.73	800*	11.8	2.1	
	SBC	48 26.5	08 06		-20.2	8800	-18.1		
6300	SB 3	17 12 18.6	-62 45 54	8.63	9.87	219	13.2	3.3	
	SBB	12 19.8	46 19	10	-19.8	1950	-16.5	.1	
6384	SX 4	17 29 58.8	07 05 43	13.6	10.50	77	14.3	.3	
	SBC	29 58.7	06 28	21	-20.2	1690	-16.4	3.8	.49
14662	IB 10	17 42 12.0	-64 37 18	2.5	10.79	62: 16	14.6	.3	P
	IM	42 13.9	37 29	16	-16.2	46.4	-12.4		
6684	LB	18 44 03.0	-65 13 54	8.06	10.69	< 50	> 14.8	> 4.1	S
	SBO				-18.8	< 389	> -14.8		
6744	SX 4	19 05 01.8	-63 56 18	4.37	8.54	< 425	> 12.5	> 4.0	
	SBC				-19.7	< 969	> -15.7		
6753	SA 3	19 07 12.0	-57 08 00	27.8	11.13	600*	12.1	1.0	P
	SB	07 11.6	07 54		-21.0	55500	-20.1		

6814	SX 4	19 39 55.2	-10 26 36	21.5	11.08	104 14	14.0	.2	2.9	
	SBC	39 56.0	26 37	12	-20.6	5740	-17.7			
6822	IB 9	19 42 07.2	-14 55 42	1.49	8.49	< 130	> 13.8		>5.3	
	IM				-17.4	< 33.9	> -12.1			
7090	SB 5	21 32 59.0	-54 46 51	6.34	10.61	< 80	> 14.3		>3.7	
	SBC				-18.4	< 385	> -14.7			
7184	SB5	21 59 53.4	-21 03 18	23.2	11.33	90: 19	14.2	.2	2.9	
	SBC	59 56.4	03 01	19	-20.5	5860	-17.6			
7205*	SA 4	22 05 06	-57 40	14.5	-11.06					
	SBC				-19.7					
7213	SA 1	22 06 12.0	-47 25 00	17.5	11.08	< 90	> 14.2		>3.1	C.P
	SA				-20.1	<3300	> -17.0			
15201	SB 6	22 18 18	-46 19	8.05	10.99	< 105	> 14.0		>3.0	
	SBCD				-18.5	< 809	> -15.5			
7410	SB 1	22 52 10.8	-39 55 42	16.7	10.78	< 80	> 14.3		>3.5	S
	SBA				-20.3	<2670	> -16.8			
15267	LA	22 54 22.4	-43 39 44	17.2	11.02	< 30	> 15.4		>4.3	
	S0				-20.1	<1060	> -15.7			
111459	E3	22 54 22.8	-36 43 48	16.7	10.70	508 32	12.3	.1	1.6	
	E3	54 22.9	43 43	8	-20.4	16900	-18.8			
7424	SX 6	22 54 28.4	-41 20 18	9.08	10.69	< 55	> 14.8		>4.1	
	SCD				-19.1	< 525	> -15.0			
7552	SB 2	23 13 25.2	-42 51 30	16.7	11.04	600*	12.1		1.1	
	SBAB	13 24.1	51 44		-20.1	20000	-19.0		0.83	.19
7582	SB 2	23 15 38.4	-42 38 42	14.9	10.95	637 39	12.0	.1	1.1	
	SBAB	15 39.0	38 33	8	-19.9	16800	-18.9			
7606	SA 3	23 16 29.4	-08 45 36	22.6	11.04	< 60	> 14.6		>3.6	
	SB				-20.7	<3660	> -17.2			
15332	SA 7	23 31 48.0	-36 22 41		10.92	< 80	> 14.3		>3.4	
	SD									
7793	SA 8	23 55 15.6	-32 52 06	2.96	9.30	107 15	14.0	.1	4.7	
	SDM	55 17.6	51 50		-18.1	112	-13.4			
2359-15	IB 9	23 59 24.0	-15 44 36	11	10.66					NOT OBSERVED
	IM									

Notes to Table 1

Confused sources

Galaxies are listed in RA order with confusing sources and their flux densities S in mJy

NGC 1022	02 36 04.1	-06 53 32	S	NGC 4365	12 21 55.6	07 35 37	S
source	02 36 11.0	-06 54 48	122	source	12 21 59.0	07 34 03	66
NGC 1073	02 41 05.4	01 09 54		NGC 4526	12 31 30.6	07 58 30	
source	02 41 22.5	01 09 53	130	source	12 31 55.8	07 58 48	66
NGC 1404	03 36 57.1	-35 45 21		NGC 4569	12 34 19.3	13 26 20	
source	03 36 51.5	-35 44 56	232	source	12 34 06.4	13 15 19	1450
NGC 1553	04 15 05.4	-55 54 08		NGC 5566	14 17 49.3	04 09 51	
source	04 14 58.8	-55 52 19	249	source	14 17 43.6	04 08 26	163
NGC 2427	07 35 02.0	-47 31 31		NGC 5746	14 42 23.3	02 09 56	
source	07 35 20.5	-47 36 01	593	source	14 42 25.9	02 13 06	139
1005+12	10 05 46.2	12 33 12		NGC 5921	15 19 27.4	05 14 53	
source	10 05 33.0	12 27 08	180	source	15 19 24.2	05 15 47	93
NGC 3976	11 53 23.4	07 01 42		NGC 7090	21 32 59.0	-54 46 51	
source	11 53 13.3	07 01 19	157	source	21 32 50.5	-54 46 25	112
NGC 4216	12 13 21.4	13 25 46		NGC 7213	22 06 12.0	-47 25 00	
source	12 13 16.5	13 22 33	80	source	22 06 07.4	-47 24 26	209
source	12 13 24.4	13 27 07	67				

Other galaxies

NGC 300:	A nearby galaxy with diameter 19.5 arcmin. There is a 730 mJy source at 00 51 41.9, -38 02 48 (Large <i>et al.</i> 1981). Nucleus has a flux density of less than 30 mJy.	NGC 1399:	There is a nearby strong source which is probably unassociated with NGC 1399, at 03 36 51.7, -35 32 29 (Schilizzi and McAdam 1975).
0237-34:	(Fornax). This nearby dwarf galaxy has a diameter of 20.0 arcmin. The radio observations did not include the whole region.	NGC 3109:	The diameter of this close galaxy is 10.7 arcmin. The nucleus has a flux density < 40 mJy.
NGC 1291:	The diameter of this galaxy is 11.0 arcmin. There is a point source of ~600 mJy at 03 15 19.0, -41 21 37.	NGC 6822:	A nearby galaxy of diameter 11.0 arcmin. A point source of ~500 mJy is at 19 42 22.5, -14 59 17.

Column 6, line 1: Optical magnitude (MAG) in the B_T^0 system where available, obtained from

- (1) de Vaucouleurs *et al.* (1981): 89 galaxies.
- (2) de Vaucouleurs (1979a): 31 galaxies.
- (3) de Vaucouleurs (personal communication 1978): 105 galaxies.
- (4) B_T^0 in RC2: 38 galaxies.
- (5) m_c , the revised and corrected magnitude on the Harvard scale: 28 galaxies.
- (6) Cameron (1971a): 3 galaxies.

The m_c magnitudes and those taken from Cameron are shown with an asterisk.

line 2: The absolute optical magnitude, MABS.

Column 7, line 1: The 408 MHz flux density S (in mJy) and the standard error where available. An asterisk indicates that the data are from

Cameron (1971*a*). A colon indicates an uncertain association and an upper limit shows that the galaxy was not detected.

line 2: The radio luminosity P in $\text{W Hz}^{-1} \times 10^{18}$.

Column 8, line 1: The radio magnitude m_{408} (RMAG) defined by $m_{408} = -53.45 - 2.5 \log S_{408}$ and standard error.

line 2: The absolute radio magnitude RMABS.

Column 9, line 1: The radio index $R_{408} = m_{408} - B_T^0$ ($R_{408} = \text{RMAG} - \text{MAG}$).

line 2: The radio spectral index and standard error as explained in Section 4.

Column 10, line 1: *Notes*: The code letters are as follows: C, a confusing source was detected in the neighbourhood (details are given in Notes to Table 1, p. 342; N, see Notes to Table 1; P, sources which are unresolved ($\lesssim 3$ arcmin diameter); S, sidelobe interference hindered measurements of flux density and position.

3. Analysis of Data and Results

(a) Radio luminosity function

Complete samples of galaxies are necessary for the derivation of the radio luminosity function. The V_0/V_m method was used to test completeness (Hummel 1981, and references therein); the mean value of V_0/V_m should be 0.5 and each value between 0 and 1 should have equal probability of occurring. For the group of galaxies in Cameron's list 1, we have $\langle V_0/V_m \rangle = 0.49 \pm 0.02$, when the limiting magnitude is $B_T^0 = 11.0$.

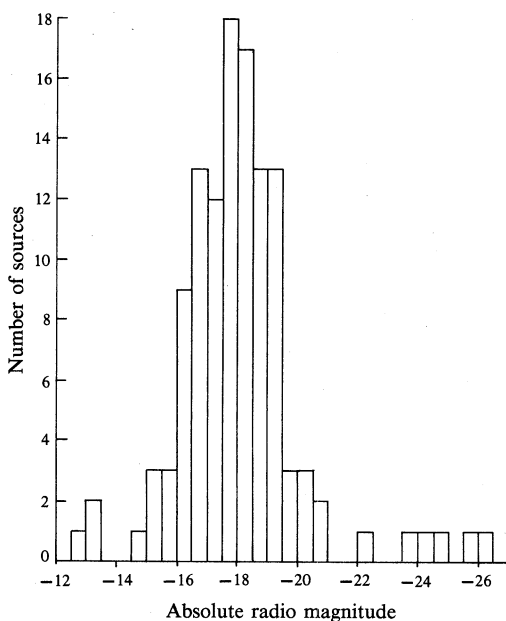


Fig. 1. Distribution of absolute radio magnitudes at 408 MHz for all detected galaxies. The weakest source is NGC 247 (Sd), the strongest NGC 4486 (E+0).

Although Cameron selected his second group of galaxies to a limiting photographic magnitude of 12.5, it was complete to $B_T^0 = 12.0$, with $\langle V_0/V_m \rangle = 0.52 \pm 0.02$. For $B_T^0 = 12.5$, we have $\langle V_0/V_m \rangle = 0.35 \pm 0.02$; the low value is reasonable as the original selection was made from the 'Reference Catalogue of Bright Galaxies' (de

Vaucouleurs and de Vaucouleurs 1964) which is known to become incomplete at $\sim B(0) = 12.5$ (Crane 1977). Also, the RC2, which together with further work (de Vaucouleurs, personal communication 1978), was used to update the sample, becomes appreciably incomplete at $B_T^0 = 12.0$. Using the derived limiting magnitudes, we excluded eight galaxies: one from list 1 ($B_T^0 > 11.0$) and seven from list 2 ($B_T^0 = 12.0$).

The distribution of absolute radio magnitudes at 408 MHz is presented in Fig. 1. The most luminous sources are the radio galaxies measured by Cameron, whereas NGC 247 (Sd), NGC 5253 (I0) and NGC 7793 (Sdm) detected in 1978 are the faintest. The radio power of Cameron's weakest source NGC 5885 was $1.4 \times 10^{20} \text{ W Hz}^{-1}$. The lower limit has now been reduced to $5.0 \times 10^{19} \text{ W Hz}^{-1}$ (NGC 247), with the majority of galaxies grouped around $10^{22} \text{ W Hz}^{-1}$.

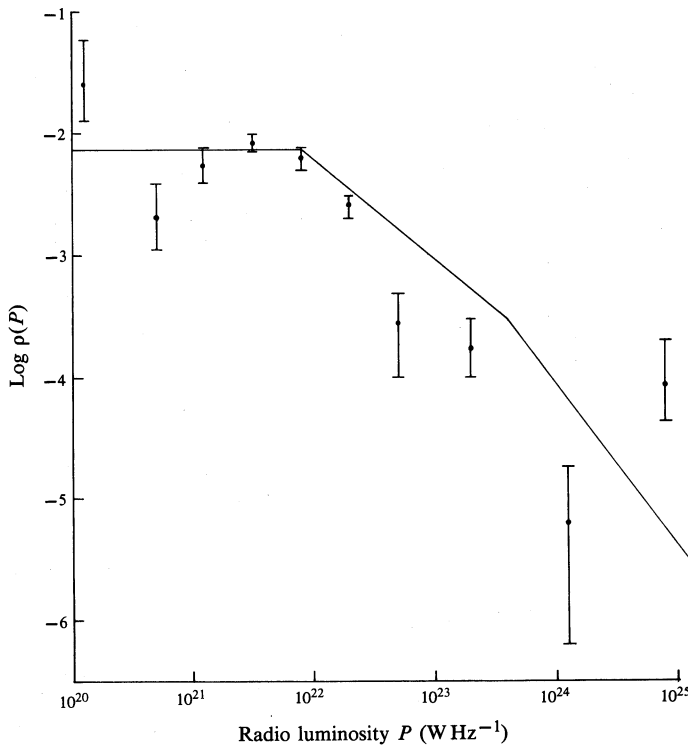


Fig. 2. Radio luminosity function $\rho(P)$ for all detected galaxies in unit magnitude steps. The standard piecewise linear fit is from Robertson (1978).

Many authors such as Colla *et al.* (1975), Auriemma *et al.* (1977), Feretti and Giovannini (1980) and Hummel (1981) have used the bivariate form of the radio luminosity function. Because of the correlation between radio and optical magnitudes (cf. Fig. 4) and the poor statistics of presently available radio luminosity functions, there is little additional information contained in the bivariate form. Therefore Fig. 2 presents the radio luminosity function for all detected galaxies in unit magnitude steps, calculated essentially as described by Cameron (1971*b*). These calculations take into account the different limiting magnitudes of the two groups of galaxies. The standard piecewise form of the radio luminosity function was calculated by Robertson

(1978) using the derivation of Fomalont *et al.* (1974) and data from von Hoerner (1973). As a result of the improved data, the errors and scatter are less than in Cameron's original curve, but the agreement is close. Fanti *et al.* (1973) investigated the radio luminosity function for a complete sample of northern spiral galaxies with the 408 MHz Bologna Radio Telescope. Fig. 3 presents their results adjusted by a factor of $1 \cdot 10$ (Fanti *et al.* 1981) to the Wyllie (1969*a*, 1969*b*) scale, along with the Molonglo data; again the agreement is good.

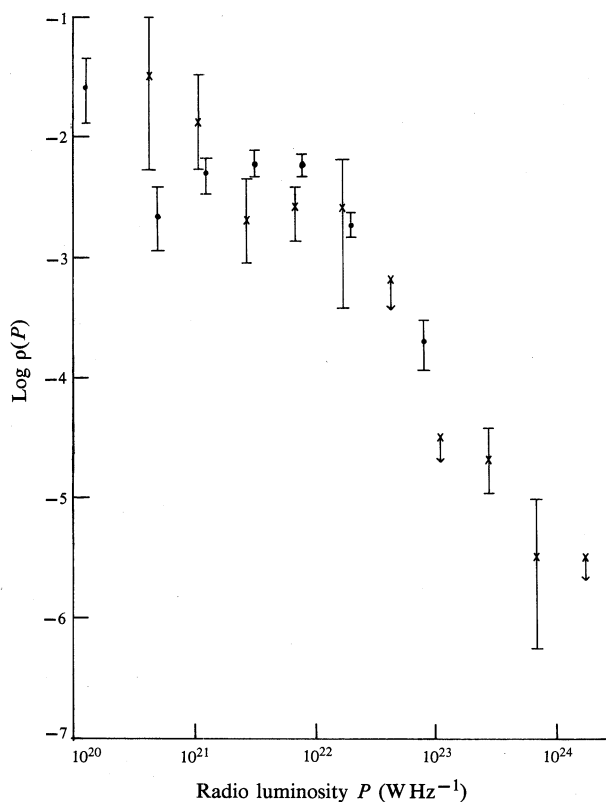


Fig. 3. Radio luminosity function $\rho(P)$ for spiral galaxies plotted for data from this paper (dots) and from the Bologna group of Fanti *et al.* (1973) (crosses).

Error bars were calculated on the basis of the number of galaxies observed, assuming Poisson statistics. For a large number n of detected galaxies, the error is $\pm n^{-1/2}$, whereas for $n < 4$ the Poisson tables are used to obtain 1σ values. The same method was used to estimate errors for the Bologna data. For bins containing small numbers of galaxies, the interval size is extended to two magnitudes.

(b) Correlation between radio and optical properties

Radio index and galaxy types. Previous surveys (Cameron 1971*a*; Hummel 1981) have compared radio observations of galaxies with their optical properties and different classification schemes, for example, Hubble and DDO types. In these surveys, as in

the present one, no more than half the galaxies were detected, making direct inter-comparisons between galaxy types impossible. This means that indirect statistical methods are necessary. Whereas Hummel (1981) used fractional luminosity functions for his analysis, the present paper uses a calculated detection probability for each galaxy based on its optical magnitude, following the method of Cameron (1971*a*). The sum of the detection probabilities may then be compared with the number of detections for different classification schemes.

The method relies on the assumption of a model for the relationship between radio and optical luminosity. The exact form of the model is not critical for relative comparisons; in this case it is based on the detected spiral galaxies because they form the most complete and best defined group. Their mean radio emission is stronger than the mean of the whole sample, and therefore the calculated number of 'expected' detections in general exceeds the actual number of detections.

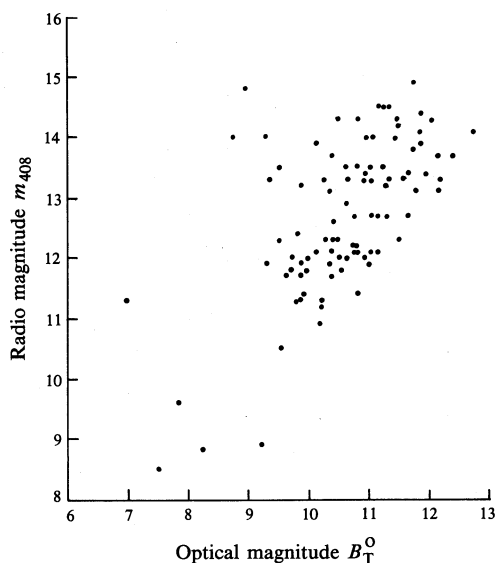


Fig. 4. Radio magnitude m_{408} plotted against optical magnitude B_T^0 for all detected spiral galaxies from Sa to Sm.

Least squares analysis of the radio and optical magnitudes of 96 detected spiral galaxies verified a linear relationship with the regression equation

$$m_{408} = 4.65 + 0.76 B_T^0 \pm 1.06 \pm 0.10. \quad (3)$$

The correlation coefficient is 0.7 and there is a vertical r.m.s. scatter of $1^m.0$. The results are also presented graphically in Fig. 4. The departure of the slope from the expected value of 1.0 is probably the result of selection effects caused by the sensitivity limit of the telescope.

The galaxies were grouped according to the revised Hubble/de Vaucouleurs type, the DDO (van den Bergh) classification, the Byurakan nuclear type and the Yerkes

(Morgan) type. Only the Hubble/de Vaucouleurs classification scheme is complete for the sample and gives meaningful results. Table 2 compares the number of galaxies detected with those 'expected'. Equation (3) has been used to define the model and a gaussian distribution for the scatter in m_{408} is assumed. Fig. 5 shows a plot of radio index R_{408} for detected galaxies against galaxy type. These results together establish that the radio emission of intermediate type spirals is well described by equation (3). In contrast, ellipticals and lenticulars combine a low average detectability with a high dispersion in radio index. Apparently their radio emission is normally low unless they display the activity of 'radio galaxies'. The SO galaxies are the least detectable; they share the normal low emission of ellipticals, but in the present sample there are no examples of radio galaxies.

Table 2. Comparison of detected galaxies with 'expected' detections

	E	L	S0	S1	S2	S3	S4	S5	S6	S7	S8	S9	I
Total detected	14	8	3	4	9	22	28	37	7	6	2	3	4
Uncertain	3	3	0	0	1	3	4	8	3	1	0	1	1
Expected	40.8	34.7	9.1	12.1	15.4	31.4	30.9	42.9	16.1	10.0	5.7	3.8	6.2
Ratio A (%) ^A	27	14	33	33	52	61	78	68	25	50	35	53	65
Ratio B (%) ^B	34	23	33	33	58	70	91	86	43	60	35	79	65

^A Ratio A is the number of well-detected galaxies, excluding uncertainties, divided by the expected number of detections.

^B Ratio B is the number of detections, including uncertainties, divided by the expected number of detections.

Distribution of radio index. The distribution of radio index for all galaxies, detected, uncertain and undetected, is shown in Fig. 6. For this complete sample the mean radio index is greater than $2^m.8$. The active radio galaxies are responsible for the low index tail to the distribution; if these are excluded, the mean radio index is greater than $3^m.0$. If undetected galaxies are also excluded, the mean radio index of the 'normal' detected galaxies is $2^m.4$ with an r.m.s. scatter of $1^m.1$. This lower value is a result of observational selection because of the radio detection limit.

4. Spectral Indices

The spectral indices and standard errors of 73 detected galaxies are listed in Table 1. In conjunction with the 408 MHz data, the surveys of Pfeiderer (1977), Dressel and Condon (1978), Pfeiderer *et al.* (1980), Hummel (1980) and the Parkes and MSH Catalogues summarized in Bolton *et al.* (1979) were used to obtain data for the following frequencies: 80, 85, 1400, 1415, 2380, 2700 and 5000 MHz. Data were initially fitted to a power law $S = \kappa \nu^\alpha$, where S is the radio flux density and ν the frequency. The regression coefficient was less than 0.8 for eight cases, so these were rejected. In most cases it was not clear whether the poor fit was caused by confusion and resolution errors or real departure of the spectrum from a power law.

For further analysis a subsample of 50 galaxies was selected, the criteria being that errors in flux density measurements were available and the standard error in the spectral index was ≤ 0.2 . Fig. 7 indicates the distribution of spectral indices for the subsample and the other galaxies. The distribution is compact, and for the subsample

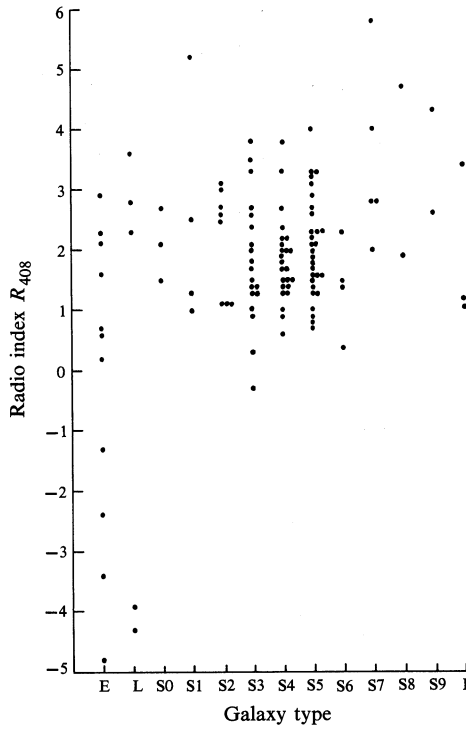


Fig. 5. Radio index R_{408} plotted against galaxy type in the Hubble/de Vaucouleurs classification scheme.

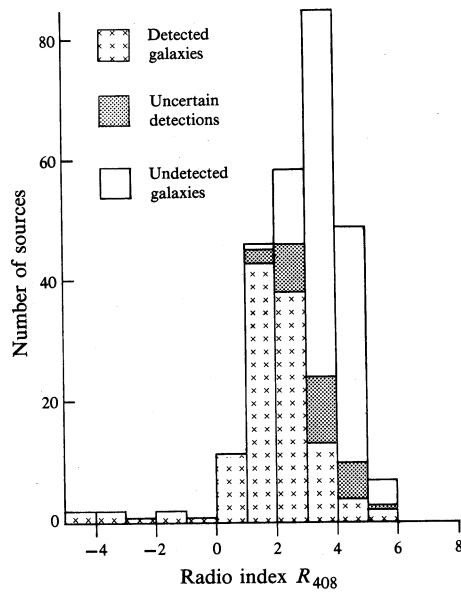


Fig. 6. Distribution of radio index for all galaxies, detected, uncertain and undetected.

the mean index $\langle\alpha\rangle$ is -0.71 with a dispersion of 0.23 . After deconvolution, the dispersion is 0.19 . Analysis of the data for 45 spiral galaxies resulted in $\langle\alpha\rangle = -0.72$ and a dispersion of 0.24 which, after deconvolution, was 0.19 .

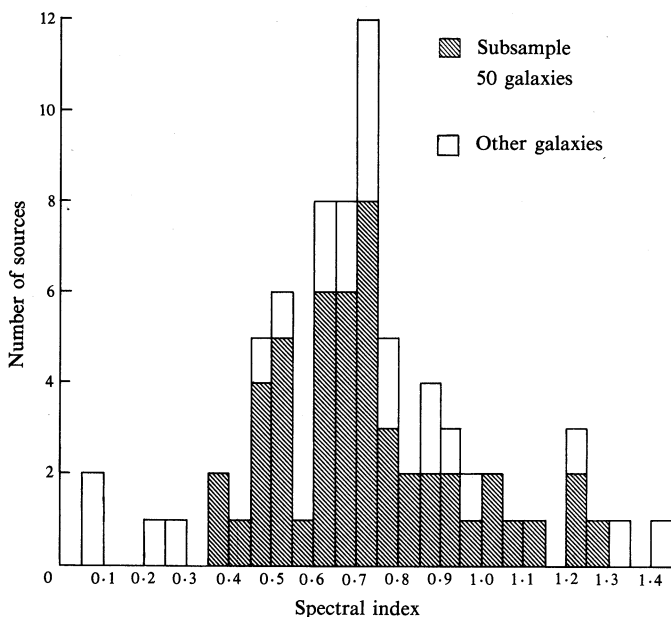


Fig. 7. Distribution of spectral index $|\alpha|$ for detected galaxies. Those with spectral indices less than 0.1 are NGC 1313 and NGC 4594.

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