

## Supplementary Material

### **Improved laboratory method to test flammability metrics of live plants under dynamic conditions and future implications**

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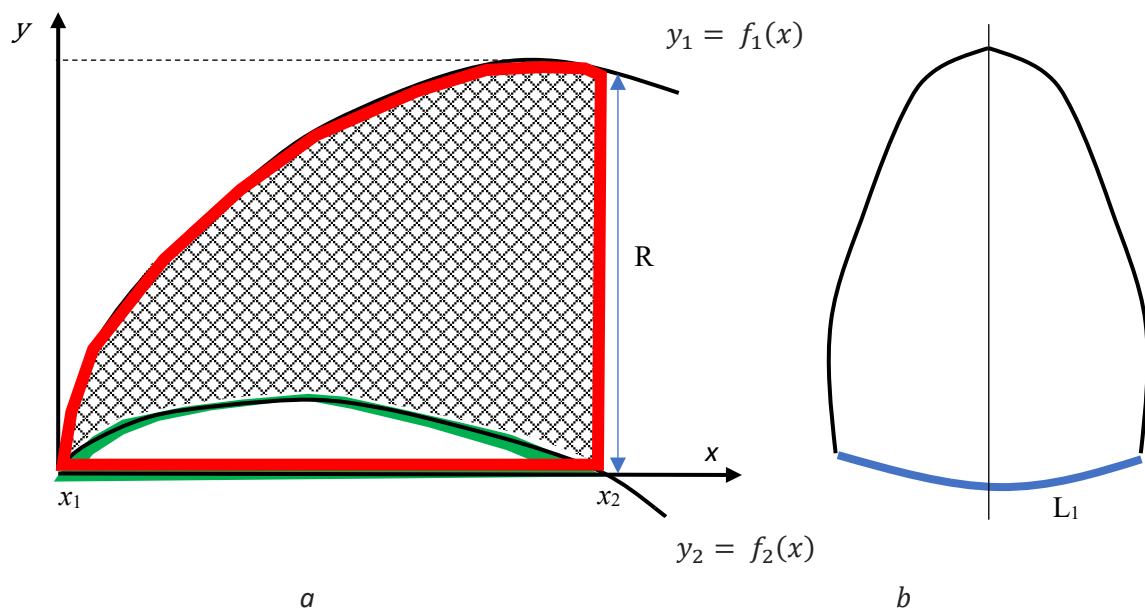
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**Calculation method of bulk volume**

Bulk volume of each sample  $V_{\text{bulk}}$  was obtained by calculating a sector of volume of a solid of revolution. A solid of revolution is a solid 3D figure obtained by rotating a plane curve around the axis of revolution ( $x$  axis in our particular case). To do so we required to characterize the geometry of our samples. Figure S1 shows side and front views for *Acacia*, *Cassinia* and *Pinus* samples. Volume of Bark samples was calculated as the volume of parallelepiped.



**Figure S1.** Geometry of sample: (a) side view and (b) front view. Where  $y_1 = f_1(x)$  and  $y_2 = f_2(x)$  are the rotation curves;  $x_1$  and  $x_2$  are the sample dimensions;  $R$  is radius of the sample base;  $L_1$  is length of the base sector (blue line).

The volume of the solid  $V$  (hatched area) formed by rotating the area between the curves  $y_1 = f_1(x)$  and  $y_2 = f_2(x)$  and the lines  $x=x_1$  and  $x=x_2$  about the  $x$ -axis can be calculated using the following equations:

$$V = V_1 - V_2, \tag{S1}$$

$$V_1 = \pi \int_{x_1}^{x_2} f_1^2(x) dx, \quad V_2 = \pi \int_{x_1}^{x_2} f_2^2(x) dx, \tag{S2}$$

$$V = \pi \int_{x_1}^{x_2} f_1^2(x) dx - \pi \int_{x_1}^{x_2} f_2^2(x) dx \quad (S3)$$

where  $V_1$  and  $V_2$  are the volumes of 3D shapes obtained by rotating  $y_1$  (red outline) and  $y_2$  (green outline) around the axis  $x$ .

To calculate volumes firstly we need to define the two functions  $y_1 = f_1(x)$  and  $y_2 = f_2(x)$  (Figure S1) that best describe the approximate sample shape for each species (except Bark). To do this, the software GetData Graph Digitizer version 2.26.0.20 (Federov 2002-2013) was used. Twenty points along each curve of the sample shape were selected, using an image of the approximated sample shape and the mean sample dimensions for each species as inputs.

Using obtained points from GetData Graph Digitizer and R version 3.6.0 (R Core Team 2019) the following function describing the sample shapes was defined:

$$f(x) = A_0 + A_1x + A_2x^2 + A_3x^3 + A_4x^4, \quad (S4)$$

where  $A_0, A_1, A_2, A_3$  and  $A_4$  are constants.

Table S1A shows constants and input parameters to calculate volume using equation (S4).

**Table S1.** Input parameters.

	<i>Acacia</i>		<i>Cassinia</i>		<i>Pinus</i> <sup>1</sup>
	$y_1$	$y_2$	$y_1$	$y_2$	$y_1$
$x_1$ , mm	0	0	0	0	0
$x_2$ , mm	371 (33)	371 (33)	391 (17)	391 (17)	192 (20)
A0	7.17493	0.66667	7.99923	0.28603	-1.27196
A1	2.1538	0.51173	1.82949	0.26486	1.31424
A2	0.01295	0.00331	0.01101	0.00162	-0.0149
A3	3.98E-05	1.06E-05	3.32E-05	5.00E-06	9.86E-05
A4	-4.88E-08	-1.54E-08	-3.94E-08	-7.08E-09	-2.43E-07

<sup>1</sup>*Pinus* has data only for  $y_1$  due to  $y_2=0$  for all samples. Values in round brackets are standard deviation.

Using functions  $y_1 = f_1(x)$  and  $y_2 = f_2(x)$  defined for the sample shape for each species, the dimensions of the samples and the equation (S3), the volume of 3D shape  $V$  for each species (except Bark) can be calculated.

To calculate volume of the sector  $V_{bulk}$  we used the following approach. We calculated circumference  $C$  of the 3D base first and then proportion of it occupied by the sample:

$$L = 2\pi R, \quad (S5)$$

$$S = \frac{L_1}{C}, \quad (S6)$$

$$V_{bulk} = VS, \quad (S7)$$

where  $S$  is the proportion of 3D figure representing sample.

$V_{bulk}$  for Bark was calculated using the equation (S8) below. Length ( $L$ ), width ( $W$ ) and depth ( $D$ ) measurements were taken from the mean dimension calculations.

$$V_{bulk} = LWD \quad (S8)$$

Calculated values are presented in Table S2.

**Table S2.** Calculated parameters.

Species	Mean R (SD), mm	Mean C (SD), mm	Mean $L_1$ (SD), mm	Mean V (SD), m <sup>3</sup>	Mean S (SD)	Mean $V_{bulk}$ (SD), m <sup>3</sup>
<i>Acacia</i>	165 (70)	1039 (441)	249 (56)	0.0222 (0.0022)	0.29 (0.14)	6.49E-03 (3.45E-03)
<i>Cassinia</i>	139 (57)	874 (361)	132 (31)	0.0179 (0.0007)	0.18 (0.08)	3.12E-03 (1.37E-03)
<i>Pinus</i>	-	-	-	0.0023 (0.0001)	1	2.31E-03 (1.17E-04)
Bark	-	-	-	-	-	9.81E-05 (1.75E-05)

$R$  is the radius of the sample base;  $SD$  is the standard deviation;  $C$  is the circumference of the 3D base;  $L_1$  is length of the base sector;  $V$  is the volume of a solid of revolution;  $S$  is the proportion of 3D figure representing sample;  $V_{bulk}$  is the bulk volume of a sample; length ( $L$ ), width ( $W$ ) and depth ( $D$ ) for bark were 192 (20) mm, 53 (6) mm, 10 (2) mm respectively.

**Table S3.** Mean time to false ignition in piloted experiments. Sample size (*n*) is also shown.

Species	Mean Time to False Ignition (sec)	
	Static	Dynamic
<i>Acacia</i>	12.4 ± 9.7 ( <i>n</i> =10)	111 ± 103 ( <i>n</i> =9)
<i>Cassinia</i>	2.8 ± 3.8 ( <i>n</i> =10)	5.9 ± 13.9 ( <i>n</i> =9)
<i>Pinus</i>	1.9 ± 2.9 ( <i>n</i> =10)	3.4 ± 5.2 ( <i>n</i> =10)
Bark	1 ( <i>n</i> =2)	9.6 ± 8.7 ( <i>n</i> =5)

**Table S4.** Comparison of models for the ignition success, time to flammability measure and radiant exposure to flammability measure

Response variable/ Model	Model 1 Spp+Exp+Pilot	Model 2 Spp*Exp+Spp*Pilot+Exp*Pilot	Model 3 Spp*Exp*Pilot
Ignition success, AIC	111	119	123
Time to reach pyrolysis, AIC	527	372	304
Radiant exposure to reach pyrolysis, AIC	547	391	312
Time to reach smouldering, AIC	302	246	234
Radiant exposure to reach smouldering, AIC	317	288	275
Time to ignition, AIC	228	178	182
Radiant exposure to ignition, AIC	246	218	222
Time to reach complete consumption, AIC	85	92	96
Radiant exposure to reach complete consumption, AIC	126	131	135

Spp is the species under the study (*Acacia*, *Cassinia*, *Pinus* and *Bark*), Exp is the type of the heating regime (static or dynamic), Pilot is the ignition method (piloted or unpiloted)

Supplementary Appendix S4

**Table S5.** Summary of results showing median time (sec) required for each species and bark to reach pyrolysis, smouldering, flaming ignition, complete consumption and the median consumption time (sec).

Flammability measure	<i>Acacia</i> , Median (MAD)				<i>Cassinia</i> , Median (MAD)				<i>Pinus</i> , Median (MAD)				Bark, Median (MAD)			
	<i>Unpiloted</i>		<i>Piloted</i>		<i>Unpiloted</i>		<i>Piloted</i>		<i>Unpiloted</i>		<i>Piloted</i>		<i>Unpiloted</i>		<i>Piloted</i>	
	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic
Pyrolysis	16 (2)	347 (12)	3 (2)	308 (69)	6 (2)	271 (20)	1 (NA)	1 (NA)	48 (6)	462 (40)	1 (NA)	1 (NA)	1 (NA)	128 (17)	1 (NA)	130 (31)
Smouldering	25 (3)	480 (22)	22 (6)	319 (81)	13 (3)	443 (32)	11 (4)	150 (94)	57 (6)	515 (9)	48 (10)	378 (83)	4 (2)	184 (12)	2 (1)	171 (27)
Flaming ignition	85 (NA)	589 (NA)	36 (8)	319 (81)	48 (7)	487 (41)	20 (7)	150 (93)	102 (7)	558 (31)	73 (34)	422 (146)	7 (1)	275 (32)	3 (1)	198 (25)
Complete consumption	117 (NA)	600 (NA)	87 (19)	393 (135)	82 (24)	562 (36)	65 (28)	497 (65)	137 (23)	574 (27)	141 (20)	555 (47)	118 (12)	433 (23)	66 (6)	306 (20)
Consumption time	32 (NA)	11 (NA)	59 (55)	48 (23)	16 (7.4)	12 (4.5)	50 (34)	198 (173)	22 (13)	16 (6)	46 (37)	44 (50)	111 (22)	86 (59)	62 (8.2)	97 (21)

NA (not applicable) is for experiments with one successful ignition. MAD is the median standard deviation (sec).

**Table S6.** Summary of results showing median radiant exposure  $H_e$  (kJ/m<sup>2</sup>) required for each species and bark to reach pyrolysis, smouldering, flaming ignition, complete consumption and the median consumption  $H_e$  (kJ/m<sup>2</sup>).

Flammability measure	<i>Acacia</i> , Median (MAD)				<i>Cassinia</i> , Median (MAD)				<i>Pinus</i> , Median (MAD)				Bark, Median (MAD)			
	<i>Unpiloted</i>		<i>Piloted</i>		<i>Unpiloted</i>		<i>Piloted</i>		<i>Unpiloted</i>		<i>Piloted</i>		<i>Unpiloted</i>		<i>Piloted</i>	
	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic
Pyrolysis	1008 (126)	5119 (266)	189 (126)	4266 (1405)	378 (95)	3540 (369)	63 (NA)	9 (NA)	3024 (347)	8517 (1365)	63 (NA)	9 (NA)	63 (NA)	1351 (211)	63 (NA)	1376 (377)
Smouldering	1544 (158)	9187 (841)	1355 (347)	4498 (1725)	788 (158)	7843 (1033)	693 (252)	1648 (1118)	3560 (347)	10650 (397)	2993 (630)	5935 (2500)	221 (95)	2103 (177)	95 (32)	1924 (394)
Flaming ignition	5355 (NA)	14544 (NA)	2268 (504)	4498 (1725)	2993 (410)	9460 (1516)	1260 (410)	1648 (1113)	6426 (441)	12843 (1640)	4568 (2111)	7163 (4720)	410 (32)	3605 (572)	189 (63)	2318 (391)
Complete consumption	7371 (NA)	15232 (NA)	5481 (1197)	6403 (3098)	5166 (1512)	12982 (2122)	4095 (1764)	9870 (3113)	8631 (1449)	13710 (1522)	8883 (1260)	12605 (2755)	7403 (756)	7498 (728)	4127 (378)	4224 (427)
Consumption $H_e$	2016 (NA)	688 (NA)	3717 (3456)	1098 (684)	1008 (467)	419 (76)	3150 (2148)	5883 (4580)	1386 (841)	867 (175)	2898 (2335)	924 (657)	6962 (1354)	2087 (985)	3874 (514)	1867 (521)

NA (not applicable) is for experiments with one successful ignition. MAD is the median standard deviation (kJ/m<sup>2</sup>).

**Table S7.** Median time and radiant exposure required to reach flammability measures and to consume samples for different heating regimes and ignition methods. Differences between medians are displayed through p-value (p). Symbols indicate level of significance: *n* is not significant ( $p > 0.05$ ), \* is suggestive ( $0.05 \geq p > 0.005$ ), \*\* is significant ( $0.005 \geq p > 0.0001$ ), \*\*\* is highly significant ( $p \leq 0.0001$ ).

	Pyrolysis		Smouldering		Flaming ignition		Complete consumption		Consumption time	
	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic	Static	Dynamic
<b>Time, sec (MAD)</b>	2 (1.5)	233 (200)	18 (19)	394 (172)	25 (28)	300 (151)	113 (52)	452 (163)	60 (51)	83 (101)
<b>p-value</b>	<0001 ***		<0001 ***		<0001 ***		<0001 ***		0.02316 *	
<b>Radiant exposure, kJ/m<sup>2</sup> (MAD)</b>	126 (93)	2873 (3470)	1134 (1214)	6339 (5285)	1575 (1775)	4102 (3275)	7088 (3269)	8151 (5534)	3748 (3222)	1682 (1409)
<b>p-value</b>	<0001 ***		<0001 ***		0.00024 **		0.03529 *		0.02587 *	
	Pyrolysis		Smouldering		Flaming ignition		Complete consumption		Consumption time	
	Piloted	Unpiloted	Piloted	Unpiloted	Piloted	Unpiloted	Piloted	Unpiloted	Piloted	Unpiloted
<b>Time, sec (MAD)</b>	1 (0)	72 (104)	55 (73)	75 (108)	68 (87)	103 (145)	231 (229)	166 (154)	73 (56)	56 (64)
<b>p-value</b>	<0001 ***		0.02047 *		0.1756 n		0.5772 n		0.03471 *	
<b>Radiant exposure, kJ/m<sup>2</sup> (MAD)</b>	63 (81)	2043 (2516)	1844 (1872)	2790 (3575)	2268 (2265)	3558 (4289)	5576 (3235)	7775 (2763)	3159 (2953)	1953 (1784)
<b>p-value</b>	<0001 ***		0.002072 **		0.1234 n		0.1278 n		0.166 n	



**Table S8.** Comparison of median time required to reach flammability measures and to consume samples for different heating regimes and ignition methods. Differences between medians are displayed through p-value (p). Symbols indicate level of significance: *n* is not significant ( $p > 0.05$ ), \* is suggestive ( $0.05 \geq p > 0.005$ ), \*\* is significant ( $0.005 \geq p > 0.0001$ ), \*\*\* is highly significant ( $p \leq 0.0001$ ). NA is not applicable.

	<i>Acacia</i>				<i>Cassinia</i>				<i>Pinus</i>				<b>Bark</b>			
	<i>Static vs Dynamic</i>		<i>Unpiloted vs Piloted</i>		<i>Static vs Dynamic</i>		<i>Unpiloted vs Piloted</i>		<i>Static vs Dynamic</i>		<i>Unpiloted vs Piloted</i>		<i>Static vs Dynamic</i>		<i>Unpiloted vs Piloted</i>	
	Unpiloted	Piloted	Static	Dynamic	Unpiloted	Piloted	Static	Dynamic	Unpiloted	Piloted	Static	Dynamic	Unpiloted	Piloted	Static	Dynamic
<b>Pyrolysis</b>	p<0001 ***	p<0001 ***	p=0.00017 **	p=0.18 n	p<0001 ***	p=0.26 n	p=0.00029 **	p<0001 ***	p<0001 ***	p=0.26 n	p<0001 ***	p<0001 ***	p<0001 ***	p=0.0031 **	p=0.051 n	p=0.88 n
<b>Smouldering</b>	p<0001 ***	p<0001 ***	p=0.64 n	p=0.0056 *	p<0001 ***	p=0.005 **	p=0.9 n	p=0.0013 **	p<0001 ***	p=0.00014 **	p=0.2 n	p=0.0034 **	p<0001 ***	p=0.00021 **	p=0.0035 **	p=0.25 n
<b>Flaming ignition</b>	p=N/A	p=0.00019 **	p=N/A	p=N/A	p=0.0054 *	p=0.00014 **	p=0.26 n	p=0.11 n	p=0.0019 **	p=0.014 *	p=0.29 n	p=0.035 *	p<0001 ***	p=0.00037 **	p=0.00034 **	p=0.00097 **
<b>Complete consumption</b>	p=N/A	p=0.0026 **	p=N/A	p=N/A	p<0001 ***	p=0.00036 **	p=0.54 n	p=0.1 n	p=0.0016 **	p=0.00046 **	p=0.42 n	p=0.22 n	p<0001 ***	p<0001 ***	p=0.0015 **	p<0001 ***
<b>Consumption time</b>	p=N/A	p=0.38 n	p=N/A	p=N/A	p=0.28 n	p=0.036 *	p=0.46 n	p=0.99 n	p=0.3 n	p=0.28 n	p=0.81 n	p=0.13 n	p=0.89 n	p=0.092 n	p=0.0037 **	p=0.99 n

**Table S9.** Comparison of median radiant exposure ( $H_e$ ) required to reach flammability measures and to consume samples for different heating regimes and ignition methods. Differences between medians are displayed through p-value (p). Symbols indicate level of significance: *n* is not significant ( $p > 0.05$ ), \* is suggestive ( $0.05 \geq p > 0.005$ ), \*\* is significant ( $0.005 \geq p > 0.0001$ ), \*\*\* is highly significant ( $p \leq 0.0001$ ). NA is not applicable.

	<i>Acacia</i>				<i>Cassinia</i>				<i>Pinus</i>				<i>Bark</i>			
	<i>Static vs Dynamic</i>		<i>Unpiloted vs Piloted</i>		<i>Static vs Dynamic</i>		<i>Unpiloted vs Piloted</i>		<i>Static vs Dynamic</i>		<i>Unpiloted vs Piloted</i>		<i>Static vs Dynamic</i>		<i>Unpiloted vs Piloted</i>	
	Unpiloted	Piloted	Static	Dynamic	Unpiloted	Piloted	Static	Dynamic	Unpiloted	Piloted	Static	Dynamic	Unpiloted	Piloted	Static	Dynamic
<b>Pyrolysis</b>	p<0001 ***	p<0001 ***	p=0.00017 **	p=0.27 n	p<0001 ***	p=0.74 n	p=0.0029 **	p<0001 ***	p<0001 ***	p=0.062 n	p<0001 ***	p<0001 ***	p<0001 ***	p=0.0066 *	p=0.051 n	p=0.84 n
<b>Smouldering</b>	p<0001 ***	p=0.0069 *	p=0.64 n	p=0.0075 *	p<0001 ***	p=0.08 n	p=0.9 n	p=0.0014 **	p<0001 ***	p=0.039 *	p=0.2 n	p=0.00026 **	p<0001 ***	p=0.00052 **	p=0.0035 **	p=0.25 n
<b>Flaming ignition</b>	p=N/A	p=0.033 *	p=N/A	p=N/A	p=0.042 *	p=0.16 n	p=0.0081 *	p=0.021 *	p=0.16 n	p=0.64 n	p=0.29 n	p=0.06 n	p<0001 ***	p=0.0011 **	p=0.00034 **	p=0.0011 **
<b>Complete consumption</b>	p=N/A	p=0.61 n	p=N/A	p=N/A	p=0.0054 *	p=0.67 n	p=0.54 n	p=0.11 n	p=0.2 n	p=0.32 n	p=0.42 n	p=0.27 n	p=0.77 n	p=0.38 n	p=0.0015 **	p=0.0003 **
<b>Consumption <math>H_e</math></b>	p=N/A	p=0.79 n	p=N/A	p=N/A	p=0.63 n	p=0.78 n	p=0.46 n	p=0.86 n	p=0.28 n	p=0.89 n	p=0.81 n	p=0.16 n	p=0.00011 **	p=0.0011 **	p=0.0037 **	p=0.22 n